

**AE 201 - DYNAMICS I**

**TEXT: Fowles: "Analytical Mechanics" 2<sup>nd</sup> Edition**

**READING ASSIGNMENTS**

| <b><u>Assign-<br/>ment No.</u></b> | <b><u>Chapter</u></b> | <b><u>Pages</u></b> | <b><u>Topic</u></b>                    |
|------------------------------------|-----------------------|---------------------|----------------------------------------|
| 1                                  | 1                     | 1-20                | Review of Fundamental Concepts         |
| 2                                  | 2                     | 21-35               | Vector Calculus; Kinematics            |
| 3                                  | 3                     | 41-58               | Rectilinear Motion                     |
| 4                                  | 4                     | 78-86               | Conservative Forces; Potential Energy  |
| 5                                  | 4                     | 86-114              | Projectile; Pendulum Motion            |
| 6                                  | 6                     | 139-160             | Central Forces and Celestial Mechanics |
| 7                                  | 7                     | 171-185             | Systems of Particles                   |
| 8                                  | 8                     | 190-217             | Plane Motion of Rigid Bodies           |
| 9                                  | 5                     | 118-134             | Moving Reference Systems               |
| 10                                 | 9                     | 221-250             | General Motion of a Rigid Body         |

# APPENDIX A

LIST OF ABBREVIATIONS

## ABBREVIATIONS

| Abbreviation                 | Full Name                                  | Page | Page |
|------------------------------|--------------------------------------------|------|------|
| Adm. Serv. Div.              | Administrative Services Division           | 101  | 101  |
| Asst. Dir.                   | Assistant Director                         | 102  | 102  |
| Chief of Div.                | Chief of Division                          | 103  | 103  |
| Comptroller                  | Comptroller                                | 104  | 104  |
| Exec. Dir.                   | Executive Director                         | 105  | 105  |
| Gen. Inv.                    | General Investigation                      | 106  | 106  |
| Ident. Div.                  | Identification Division                    | 107  | 107  |
| Intell. Div.                 | Intelligence Division                      | 108  | 108  |
| Lab.                         | Laboratory                                 | 109  | 109  |
| Legal Coun.                  | Legal Counsel                              | 110  | 110  |
| Plan. & Insp. Div.           | Planning and Inspection Division           | 111  | 111  |
| Rec. Mgmt. Div.              | Records Management Division                | 112  | 112  |
| Spec. Inv.                   | Special Investigation                      | 113  | 113  |
| Training Div.                | Training Division                          | 114  | 114  |
| Off. of Cong. & Public Affs. | Office of Congressional and Public Affairs | 115  | 115  |

AE 211 Dynamics I

TEXT: Fowles : "Analytical Mechanics "

Holt, Rinehart, Winston

OUTLINE OF TOPICS

- I. Review of Kinematics
- II. Review of Equations of Motion for a Particle, Energy Principles, Angular Momentum
- III. Kinetics of Particles
  - Motion of a Projectile in a Resisting Medium
  - Pendulum Problems
  - Harmonic Oscillators
  - Gravitation; Center of Gravity
  - Central Force Motion
- IV. Momentum and Energy Principles for Systems of Particles
- V. Plane Motion of a Rigid Body
- VI. Impulsive Motion
- VII. Moments and Products of Inertia; Kinetic Energy; Angular Momentum
- VIII. Kinematics of Rotation and of Rigid Bodies
- IX. Moving Frames of Reference; Effects of Earth's Rotation
- X. Motion of a Rigid Body

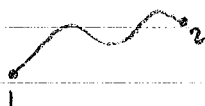
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2000-2001

- I. Review of Literature
- II. Review of Education of Native Americans
- III. Review of Education of Native Americans
- IV. Review of Education of Native Americans
- V. Review of Education of Native Americans
- VI. Review of Education of Native Americans
- VII. Review of Education of Native Americans
- VIII. Review of Education of Native Americans
- IX. Review of Education of Native Americans
- X. Review of Education of Native Americans

# Analytical Mechanics - Fowles Second Edit.

A. Work done moving particle from 1 to 2



$$U_{1-2} = T_2 - T_1 \quad T - \text{kinetic energy}$$

If conservative force field:

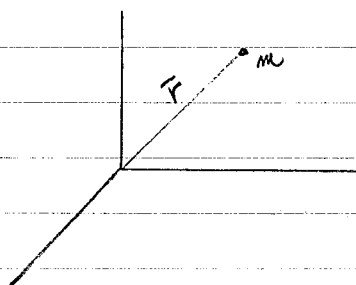
$$T_1 + V_1 = T_2 + V_2 \quad V - \text{potential energy}$$

B. Impulse - Momentum relations

$$m\vec{v}_i + \int \vec{F} dt = m\vec{v}_f$$

C. Review of Kinematics

Definition:

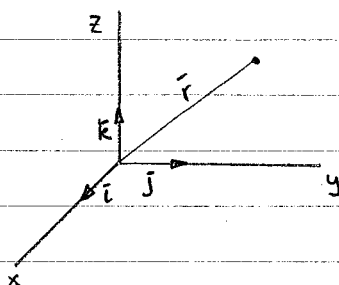


$$\vec{r} = \vec{r}(t), \quad \vec{v} = \frac{d\vec{r}}{dt}, \quad \vec{a} = \frac{d\vec{v}}{dt} = \frac{d^2\vec{r}}{dt^2}$$

## 1. Rectangular Coordinates

$$\vec{r} = x\vec{i} + y\vec{j} + z\vec{k}$$

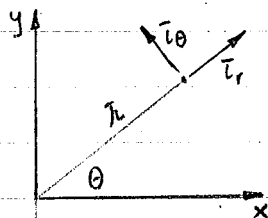
Inertial frame - frame in which  $\vec{F} = m\vec{a}$  holds



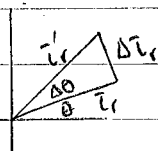
$$\vec{v} = \frac{d\vec{r}}{dt} = \dot{x}\vec{i} + \dot{y}\vec{j} + \dot{z}\vec{k}$$

$$\vec{a} = \frac{d\vec{v}}{dt} = \ddot{x}\vec{i} + \ddot{y}\vec{j} + \ddot{z}\vec{k}$$

## 2. Polar Coordinates (Plane)



$$\begin{aligned}\vec{r} &= r \vec{e}_r \\ \vec{v} &= \frac{d\vec{r}}{dt} = \dot{r} \vec{e}_r + r \frac{d\vec{e}_r}{dt} \\ &= \dot{r} \vec{e}_r + r \dot{\theta} \frac{d\vec{e}_r}{d\theta} \\ &= \dot{r} \vec{e}_r + r \dot{\theta} \vec{e}_\theta\end{aligned}$$

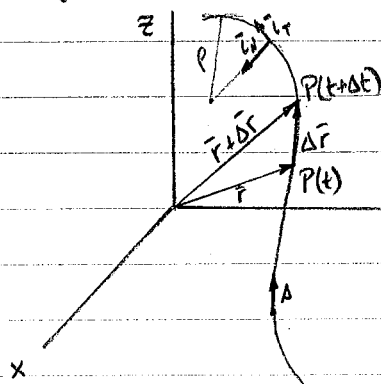


$$\begin{aligned}\lim_{\Delta\theta \rightarrow 0} \frac{\Delta \vec{e}_r}{\Delta\theta} &= \lim_{\Delta\theta \rightarrow 0} \frac{2|\vec{e}_r| \sin \frac{\Delta\theta}{2}}{\Delta\theta} = 1 \\ &= \frac{2(\Delta\theta/2)}{\Delta\theta} = 1\end{aligned}$$

$\frac{d\vec{e}_r}{d\theta}$  is  $\perp$  to  $\vec{e}_r$ :  $\vec{e}_\theta$

$$\begin{aligned}\vec{a} &= \ddot{r} \vec{e}_r + \dot{r} \dot{\theta} \vec{e}_\theta + \dot{r} \dot{\theta} \vec{e}_\theta + r \ddot{\theta} \vec{e}_\theta - r \dot{\theta}^2 \vec{e}_r \\ &= (\ddot{r} - r \dot{\theta}^2) \vec{e}_r + (2\dot{r} \dot{\theta} + r \ddot{\theta}) \vec{e}_\theta\end{aligned}$$

## 3. Tangent-Normal Coordinates (Path)



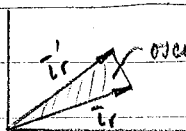
$$\lim_{\Delta t \rightarrow 0} \frac{|\Delta \vec{r}|}{\Delta s} = 1 = |\vec{e}_T|$$

$$\vec{v} = v \vec{e}_T \quad (\text{unit tangent vector})$$

$$\vec{a} = \dot{v} \vec{e}_T + \frac{v^2}{\rho} \vec{e}_N \quad (\text{principal normal})$$

$\vec{e}_T$  &  $\vec{e}_N$  lie in the osculating plane

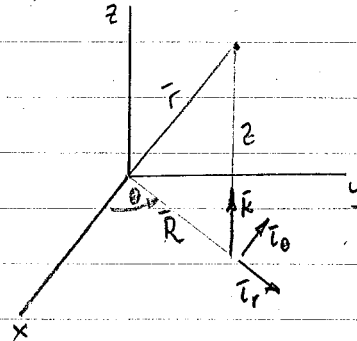
Note: positive  $\vec{e}_N$  points toward center of curvature.



osculating plane

$$\vec{e}_T \times \vec{e}_N = \vec{e}_b \quad \text{binormal.}$$

#### 4. Cylindrical Coordinates



$$\vec{r} = R\vec{e}_r + z\vec{e}_z$$

$$\vec{v} = \dot{R}\vec{e}_r + R\dot{\theta}\vec{e}_\theta + \dot{z}\vec{e}_z$$

$$\vec{a} = (\ddot{R} - R\dot{\theta}^2)\vec{e}_r + (2\dot{R}\dot{\theta} + R\ddot{\theta})\vec{e}_\theta + \ddot{z}\vec{e}_z$$

#### 5. Frenet - Serret Formulas

$$\frac{d\vec{e}_T}{ds} = \frac{1}{\rho} \vec{e}_N ; \quad \frac{d\vec{e}_N}{ds} = -\frac{1}{\rho} \vec{e}_T + \frac{1}{\tau} \vec{e}_b$$

$$\frac{d\vec{e}_b}{ds} = -\frac{1}{\tau} \vec{e}_N$$

$\tau$  - radius of torsion

$$\vec{e}_T \cdot \vec{e}_T = 1 \rightarrow 2 \frac{d\vec{e}_T}{ds} \cdot \vec{e}_T = 0$$

$$\frac{d\vec{e}_N}{ds} = a\vec{e}_T + b\vec{e}_b$$

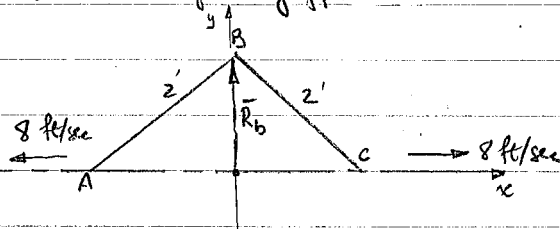
$$\frac{d\vec{e}_b}{ds} = \alpha\vec{e}_T + \beta\vec{e}_N$$

$$\text{and } \vec{e}_T \cdot \vec{e}_N = 0 \quad \vec{e}_T \cdot \vec{e}_b = 0 \quad \vec{e}_N \cdot \vec{e}_b = 0$$

$$\text{gives } a = -\frac{1}{\rho} \quad b = \frac{1}{\tau} \quad \alpha = 0 \quad \beta = -\frac{1}{\tau}$$

Problem 4 Pg 116

Singer & Griffith



Find  $\vec{v}_B$  &  $\vec{a}_B$  when  $\vec{AB}$  is  $\perp$  to  $\vec{BC}$

$$\vec{r}_B = y_B \vec{j}$$

$$\vec{v}_B = \dot{y}_B \vec{j}$$

$$\vec{a}_B = \ddot{y}_B \vec{j}$$

$$y_B = \sqrt{4 - x_C^2}$$

$$\dot{y}_B = \frac{-1}{(4 - x_C^2)^{1/2}} x_C \dot{x}_C = -\frac{8x_C}{(4 - x_C^2)^{1/2}}$$

$$\ddot{y}_B = (4 - x_C^2)^{1/2} - 8\dot{x}_C + 8x_C(4 - x_C^2)^{-3/2}(-\frac{1}{2} - 2x_C\dot{x}_C)$$

$$\ddot{y} = -8x_c^2 (4-x_c^2)^{-3/2} - 64(4-x_c^2)^{-1/2}$$

when  $\vec{AB} \perp \vec{BC}$   $x_c = \sqrt{2}$

$$\therefore \ddot{y}_0 = -8 \text{ ft/sec}^2 \quad \ddot{y}_B = -64\sqrt{2} \text{ ft/sec}^2$$

Problem 2.2 from Fowler

Given  $\vec{r} = (\cos \omega t) \vec{i} + 2 \sin \omega t \vec{j}$

Find  $\vec{v}$  &  $\vec{a}$  when  $t = \pi/4\omega$  sec

$$\vec{v} = -\omega \sin \omega t \vec{i} + 2\omega \cos \omega t \vec{j}$$

$$\vec{a} = -\omega^2 \cos \omega t \vec{i} - 2\omega^2 \sin \omega t \vec{j}$$

$$\vec{v} \cdot \vec{a} = |\vec{v}| |\vec{a}| \cos \phi_a$$

$$\text{@ } t = \pi/4\omega$$

$$\vec{v} = -\frac{\omega\sqrt{2}}{2} \vec{i} + 2\omega \frac{\sqrt{2}}{2} \vec{j}$$

$$\vec{a} = -\omega^2 \frac{\sqrt{2}}{2} \vec{i} - \omega^2 \sqrt{2} \vec{j}$$

$$\frac{\vec{v} \cdot \vec{a}}{|\vec{v}| |\vec{a}|} = \cos \phi$$

$$\cos \phi; \quad \omega^{3/2} - 2\omega^3 = -\frac{3\omega^3}{2}$$

$$|\vec{v}| = \sqrt{\frac{\omega^2}{2} + 2\omega^2} = \omega \sqrt{\frac{5}{2}}; \quad |\vec{a}| = \sqrt{\frac{\omega^4}{2} + 2\omega^4} = \omega^2 \sqrt{\frac{5}{2}}$$

$$\cos \phi = \frac{-\frac{3\omega^2}{2}}{5\omega^{3/2}} = -\frac{3}{5}$$

$$\phi = \cos^{-1}(-\frac{3}{5})$$

## 6. Equations of Motion

Rectangular Coord.

$$\vec{F} = m\vec{a} = m[\ddot{x}\vec{i} + \ddot{y}\vec{j} + \ddot{z}\vec{k}]$$

$$F_x = m\ddot{x}, \quad F_y = m\ddot{y}, \quad F_z = m\ddot{z}$$

Polar Coordinates (Plane)

$$F_r = (\ddot{r} - r\dot{\theta}^2)m$$

$$F_\theta = (2\dot{r}\dot{\theta} + r\ddot{\theta})m$$



2/2/71

Eg of Motion

1. Rect:  $F_x = m\ddot{x}$   $F_y = m\ddot{y}$   $F_z = m\ddot{z}$

2. Path:  $F_r = m\dot{v}$   $F_N = \frac{mv^2}{\rho}$   $F_b = 0$

3. Cylind:  $F_r = m[\ddot{R} - R\dot{\phi}^2]$   $F_\phi = m \frac{1}{R} \frac{d}{dt} [R^2 \dot{\phi}]$   $F_z = m\ddot{z}$

Rectilinear Motion of a particle

I.



$x(0) = x_0$

$\dot{x}(0) = v_0$

$F = F(t) = \alpha t^2$



$F_x = ma_x$

$= m \frac{dv}{dt} = \alpha t^2$

$dv = \frac{\alpha}{m} t^2 dt \rightarrow v + c_1 = \frac{\alpha t^3}{3m}$

at  $t=0$   $v = v_0$   $c_1 = -v_0$

$\therefore v - v_0 = \frac{\alpha t^3}{3m}$

Now  $v = \frac{dx}{dt} = v_0 + \frac{\alpha t^3}{3m} \rightarrow x + c_2 = \frac{\alpha t^4}{12m} + v_0 t$

at  $t=0$   $x = x_0$   $\therefore c_2 = -x_0$

$x - x_0 = v_0 t + \frac{\alpha t^4}{12m}$

II

$F = F(v)$   $F = -kv^2$   $k > 0$

$x(0) = x_0$

$\dot{x}(0) = v_0$



$F_x = ma_x = -kv^2$

$= m v \frac{dv}{dx} = -kv^2$

finally  $-\frac{k}{m} x = \ln v + \ln c_1$   $\ln c_1 = -\frac{k}{m} x_0 - \ln v_0$

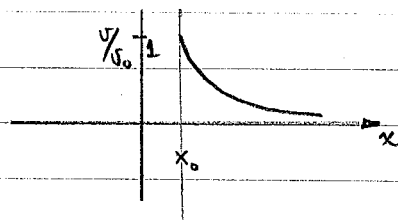
$\therefore -\frac{k}{m} [x - x_0] = \ln \frac{v}{v_0}$  call  $\frac{k}{m} = \lambda$

$$\text{or } e^{\lambda(x_0-x)} = v/v_0$$

$$\frac{dx}{dt} = v_0 e^{\lambda(x_0-x)} ; \quad t = \frac{1}{\lambda v_0} e^{\lambda(x-x_0)} + c_2$$

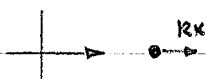
$$\text{at } t=0 \quad x=x_0 \quad \therefore \quad c_2 = -\frac{1}{v_0 \lambda}$$

$$\text{or } \boxed{t = \frac{1}{v_0 \lambda} [e^{\lambda(x-x_0)} - 1]}$$



$$\text{III} \quad F = F(x) \quad F = kx \quad k > 0 \quad x(0) = x_0$$

$$\dot{x}(0) = v_0$$



$$kx = m v \frac{dv}{dx}$$

$$kx dx = m v dv \quad \text{or} \quad \frac{kx^2}{2} = \frac{mv^2}{2} + c_1 \quad c_1 = \frac{k}{2} x_0^2 - \frac{mv_0^2}{2}$$

$$\text{or } \boxed{\frac{k}{m} [x^2 - x_0^2] + v_0^2 = v^2}$$

$$\frac{dx}{dt} = \sqrt{\lambda [x^2 - x_0^2] + v_0^2} \rightarrow dt = \frac{dx}{\sqrt{\lambda x^2 + (v_0^2 - \lambda x_0^2)}}$$

$$\boxed{t = \frac{1}{\sqrt{\lambda}} \ln \left[ x + \sqrt{\frac{v_0^2}{\lambda} - (x_0^2 - x^2)} \right]}$$

$$\text{IV} \quad F = F(x) \quad F = -kx \quad x(0) = x_0$$

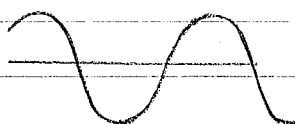
$$\dot{x}(0) = v_0$$



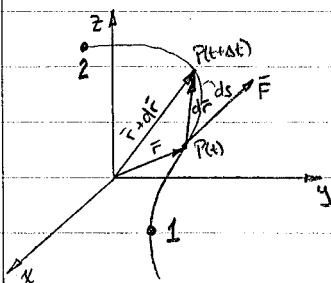
$$-kx = m \ddot{x}$$

$$m \ddot{x} + kx = 0$$

$$x = A \sin \omega t + B \cos \omega t \quad \omega^2 = \frac{k}{m}$$



## Energy Principles



$$dU = \vec{F} \cdot d\vec{r} \quad \text{definition of work.}$$

Principle of work & energy

$$dU = m \frac{d\vec{v}}{dt} \cdot \vec{v} dt$$

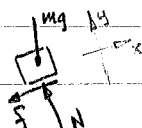
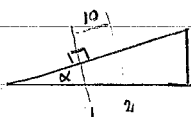
$$= m \vec{v} \cdot d\vec{v} = d\left(\frac{m}{2} \vec{v} \cdot \vec{v}\right) = dT$$

$$\text{Call } T = \frac{m}{2} \vec{v} \cdot \vec{v} = \frac{mv^2}{2} \quad (\text{kinetic energy})$$

$$\int_1^2 dU = T_2 - T_1$$

in kinetic energy

work done on a particle is equal to the change



$$T_2 - T_1 = -[mg \sin \alpha + \mu N] s$$

Consider a scalar point fn.  $V(x, y, z)$

$$\nabla V = \frac{\partial V}{\partial x} \vec{i} + \frac{\partial V}{\partial y} \vec{j} + \frac{\partial V}{\partial z} \vec{k}$$

gradient vector.

$$\frac{dV}{ds} = \nabla V \cdot \frac{d\vec{r}}{ds} = \frac{\partial V}{\partial x} \frac{dx}{ds} + \frac{\partial V}{\partial y} \frac{dy}{ds} + \frac{\partial V}{\partial z} \frac{dz}{ds}$$

directional derivative

$$\text{or } \frac{dV}{ds} = \nabla V \cdot \vec{i}_T$$

Definition of a conservative force field: the work done by a system of forces independent of the path. Work done over a closed path is 0.

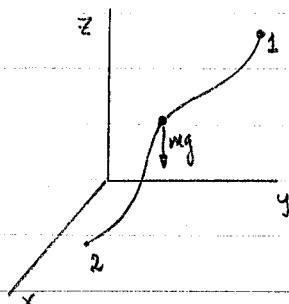
Definition of Potential Energy - for a cons. system of forces define  $V(x, y, z)$

$$dU = \vec{F} \cdot d\vec{r} = -dV$$

$$\text{Recall } dV = \nabla V \cdot d\vec{r} = -\vec{F} \cdot d\vec{r} \rightarrow$$

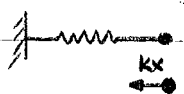
$$\boxed{\vec{F} = -\nabla V}$$

$$F_x = -\frac{\partial V}{\partial x} \quad F_y = -\frac{\partial V}{\partial y} \quad F_z = -\frac{\partial V}{\partial z} \quad \text{if } \vec{F} = F_x \vec{i} + F_y \vec{j} + F_z \vec{k}$$



$x, y$  plane is in plane of earth surface.

$$V = (mg)z$$



$$V = \frac{1}{2} kx^2$$

Inverse square law:

$$V = -\frac{GMm}{r}$$



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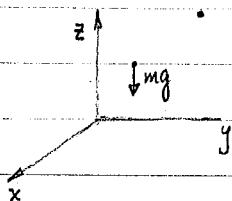
Prob 3,3,5,12,20

Mimeo 9,10

$$\int_1^2 dU = T_2 - T_1$$

In a conservative force field  $\nabla \times \vec{F} = 0$ .

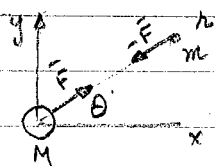
Know derivation of following:



$$V = mgz$$

$$\vec{F}_2 = -mg = -\nabla V = -\frac{\partial V}{\partial z}$$

$$\therefore V_2 - V_1 = mg(z_2 - z_1)$$



$$\vec{F} = -\nabla V = -\frac{\partial V}{\partial r}$$

$$\frac{GMm}{r^2} = -\frac{\partial V}{\partial r}$$

$$\therefore V_2 - V_1 = \left[ \frac{GMm}{r_1} - \frac{GMm}{r_2} \right]$$



$$\vec{F} = -kx = -\frac{\partial V}{\partial x} = -\nabla V$$

$$\therefore V_2 - V_1 = \frac{k}{2} [x_2^2 - x_1^2]$$

Principle of Conservation of Energy - Conservative force field

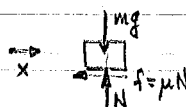
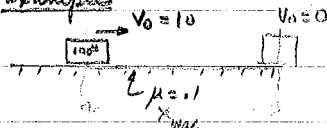
$$dU = \vec{F} \cdot d\vec{r} = -dV \quad \text{Def.}$$

$$dU = \vec{F} \cdot d\vec{r} = dT \quad \text{Principle of work.}$$

$$dT = -dV \rightarrow T_2 - T_1 = V_1 - V_2$$

$$\boxed{T_2 + V_2 = T_1 + V_1}$$

Example



1.

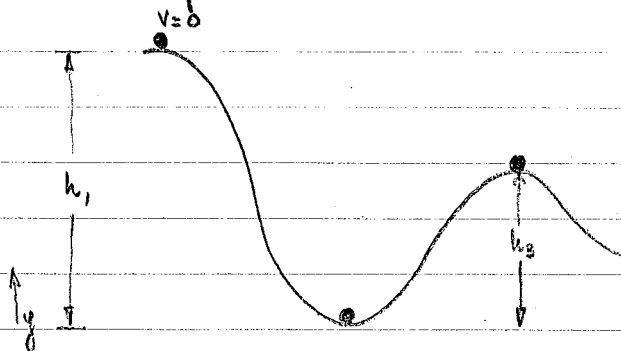
$$\int F_x dx = T_2 - T_1$$

$$\int_1^2 -\mu N dx = -\mu \int_1^2 mg dx = -\mu mg \Delta x = 0 - \frac{1}{2} m v_0^2$$

$$x_m = \frac{v_0^2}{2\mu g} = \frac{100}{2(0.1)(32.2)} \approx 15 \text{ ft}$$

2.  $F_x = \max = -\mu N = m v \frac{dv}{dx}$ ;  $-\mu g (x_2 - x_1) = \frac{v_2^2}{2} - \frac{v_1^2}{2}$ ;  $\frac{v_1^2}{2\mu g} = x_2 - x_1 \approx 15 \text{ ft.}$

Example

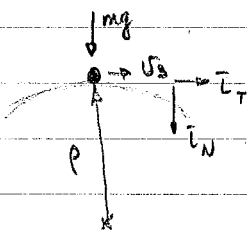


$$T_1 + V_1 = T_3 + V_3$$

$$0 + mgh_1 = \frac{mv_3^2}{2} + mgh_3$$

$$v_3 = \sqrt{2g(h_1 - h_3)}$$

$$v_2 = \sqrt{2gh_1}$$

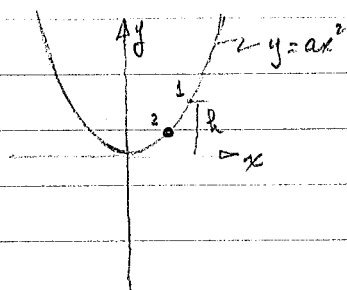


$$F = \frac{mv_3^2}{r_{\min}} = mg \quad r_{\min} = 2(h_1 - h_3)$$

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3-1 hr. Quizzes.

Example in Constrained Motion.



$$T + V = \text{constant.}$$

$$T_1 + V_1 = T_2 + V_2$$

$$0 + mgh = \frac{1}{2}mv^2 + mgy$$

$$\frac{1}{2}mv^2 = m(gh - gy)$$

$$v^2 = 2g(h - y) \quad (1)$$

$$\dot{x}^2 + \dot{y}^2 = v^2 \quad (2) \quad \text{also} \quad \dot{y} = 2ax\dot{x}$$

$$\dot{x}^2 + \dot{y}^2 = 2g(h - y)$$

$$\dot{x}^2 [1 + 4a^2x^2] = 2g(h - ax^2) \quad (3)$$

$$\frac{dx}{dt} = \sqrt{\frac{2g(h - ax^2)}{1 + 4a^2x^2}} \quad ; \quad dt = dx \sqrt{\frac{1 + 4a^2x^2}{2g(h - ax^2)}} \quad (4)$$

If  $h \ll 1$   $y \ll 1$  go back to (3)

$$\dot{x}^2 [1 + 4ay] = 2g(h - y) \quad \text{neglect } 4ay$$

$$\therefore \dot{x}^2 = 2g(h - ax^2)$$

$$2\dot{x}\ddot{x} = -4gax\dot{x} \rightarrow \ddot{x} + 2gax = 0$$

$$x = C_1 \sin \omega t + C_2 \cos \omega t$$

$$\omega^2 = 2ga$$

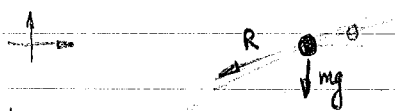
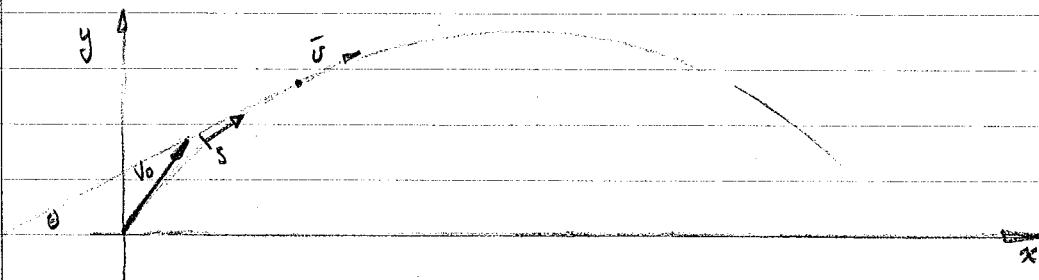
$$\dot{x} = C_1 \omega \cos \omega t - C_2 \omega \sin \omega t$$

$$\text{if } \dot{x} = 0 \quad C_1 = 0 \quad \text{if } v = 0 \text{ at } y = h.$$

$$\therefore x = C_2 \cos \omega t$$

Projectile Motion (with resistance)

Planar Motion - assume uniform grav. field.



1 Cartesian

$$(1) F_x = ma_x = m\ddot{x} = -R \cos \theta$$

$$v \cos \theta = \dot{x} ; v \sin \theta = \dot{y} \rightarrow \dot{x}^2 + \dot{y}^2 = v^2$$

$$(2) F_y = ma_y = m\ddot{y} = -R \sin \theta - mg$$

$$\text{from (1)} \quad -R \frac{\dot{x}}{v} = m\ddot{x} \quad (1a)$$

$$\text{let } \phi(x, y) = \frac{R}{mv}$$

$$\text{" (2)} \quad -R \frac{\dot{y}}{v} - mg = m\ddot{y} \quad (2a)$$

$$\text{then } \ddot{x} + \phi \dot{x} = 0 \quad \ddot{y} + \phi \dot{y} = -g$$

2 Tangent-Normal Coordinate.



$$(1) F_T = ma_T = m\dot{v} = -R - mg \sin \theta$$

$$(2) F_N = ma_N = mg \cos \theta = \frac{mv^2}{\rho} \quad \rho d\theta = -ds$$

$$(1) \text{ can be written as } -\frac{R}{mv} - g \frac{\sin \theta}{v} = -\frac{dv}{\rho d\theta} \quad (3a)$$

$$(2) \text{ can be written as } mg \cos \theta = -\frac{mv^2 d\theta}{ds} \quad (4)$$

$$\text{using (3)} \quad \frac{R}{mv} + g \frac{\sin \theta}{v} = -\frac{dv}{ds} \quad \text{we can get}$$

$$\frac{dv}{d\theta} = \left[ \frac{R}{mg} + \sin \theta \right] \frac{v}{\cos \theta}$$

3 Equation of the hodograph:

$$4a \quad \frac{1}{v} \frac{dv}{d\theta} = \Phi \sec\theta + \tan\theta \quad \text{if } R/mg = \Phi \quad \& \quad \Phi = cv^2$$

$$\text{substitute } \tanh \psi = \sin\theta$$

$$\operatorname{sech}^2 \psi d\psi = \cos\theta d\theta$$

$$1 - \tanh^2 \psi = \cos^2 \theta$$

$$\operatorname{sech}^2 \psi = \cos^2 \theta$$

$$\frac{d}{d\psi} \left( \frac{1}{v^2} \right) = -2c - 2 \left( \frac{1}{v^2} \right) \tanh \psi$$

$$\text{when } \frac{1}{v^2} = \frac{1}{v^2}(\psi)$$

$$\frac{1}{v^2} = \cos^2 \theta \left[ A - c \tanh^{-1}(\sin\theta) \right] - c \sin\theta$$

$$\frac{dx}{d\theta} = \frac{dx}{ds} \frac{ds}{d\theta} = -p \cos\theta$$

$$x = \int -p \cos\theta d\theta + c_1 = \int -\frac{v^2}{g} d\theta + c_1$$

$$\frac{dy}{d\theta} = -p \tan\theta \cos\theta$$

$$y = \int -p \cos\theta \tan\theta d\theta + c_2 = \int -\frac{v^2}{g} \tan\theta d\theta + c_2$$

$$4b \quad \text{if } R = mgc \quad \Phi = cg$$

use rectangular coord.

$$\ddot{x} + gc\dot{x} = 0$$

$$\text{let } \varphi = \dot{x} \quad \dot{\varphi} = \ddot{x}$$

$$\dot{\varphi} + gc\varphi = -g$$

$$\varphi + gc\varphi = 0$$

$$\text{let } \varphi = Ae^{\lambda t} + A\lambda e^{\lambda t} + gcAe^{\lambda t} = 0$$

$$\lambda = -gc$$

$$\therefore \varphi = Ae^{-gct}$$

$$\dot{x}(0) = \dot{x}_0 = A$$

$$x = \frac{A}{-gc} e^{-gct} = \frac{\dot{x}_0}{-gc} e^{-gct} + B$$

$$B = \frac{\dot{x}_0}{gc} + x_0$$

$$x = \frac{\dot{x}_0}{gc} [1 - e^{-gct}] + x_0$$

y turns out to be

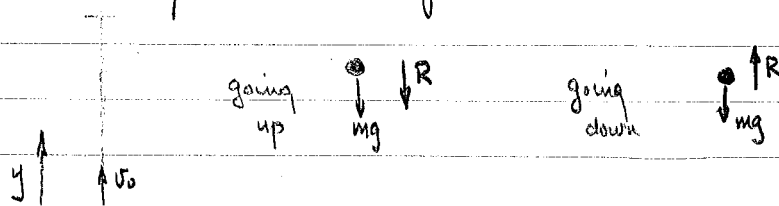
$$y = y_0 - \frac{t}{c} + \frac{1}{gc} \left[ \dot{y}_0 + \frac{1}{c} \right] [1 - e^{-gct}]$$



# Vertical Motion of Projectile in $R = kv^2$ Medium.

Eq of Hodograph is no good.

Initially  $v(0) = v_0, y = 0$



$$-R - mg = m v \frac{dv}{dy} \quad \text{if } R = mgcv^2$$

$$-g[1 + cv^2] = v \frac{dv}{dy} \quad ; \quad -g dy = \frac{v dv}{1 + cv^2}$$

$$-g \int dy = \frac{1}{2c} \ln(1 + cv^2) \rightarrow -2gc y = \ln(1 + cv^2) + A$$

$$A = -\ln(1 + cv_0^2) \quad \therefore +2gc y = \ln\left(\frac{1 + cv_0^2}{1 + cv^2}\right)$$

$$y \downarrow \quad mg = mgcv^2 = m v \frac{dv}{dy}$$

$$g(1 - cv^2) = v \frac{dv}{dy}$$

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$$\text{UP} \quad y = -\frac{1}{2gc} \ln(1 + cv^2) + C_1$$

$$\text{DOWN} \quad y = \frac{1}{2gc} \ln(1 - cv^2) + C_2$$

$$\Delta KE = \Delta \text{Work} \quad -\int_0^H (mg + R) dy = -\frac{1}{2} m v_0^2$$

H.W. Chapter 4.

4.1 abc

4.3

4.5

$$\vec{F} = y\vec{i} + x\vec{j}$$

$$\vec{F} = y\vec{i} - x\vec{j}$$

both conserve

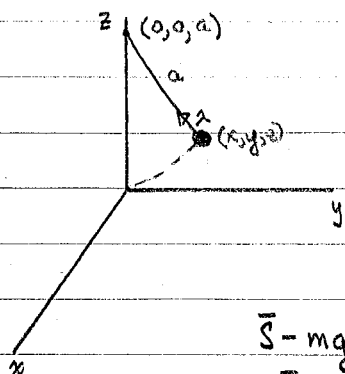
Energy principle needed

Quiz #1

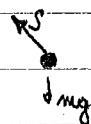
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Kinematics, Kinetics (Rectilinear), Work & Energy.

# Pendulum Motion.



## Small Oscillations of a Spherical Pendulum.



$$\vec{F} = m\vec{a}$$

$$\vec{F} = F_x \vec{i} + F_y \vec{j} + F_z \vec{k} = m(\ddot{x}\vec{i} + \ddot{y}\vec{j} + \ddot{z}\vec{k})$$

$$\vec{S} - mg\vec{k} = m(\ddot{x}\vec{i} + \ddot{y}\vec{j} + \ddot{z}\vec{k})$$

$$S\vec{\lambda} - mg\vec{k} = m\ddot{x}\vec{i} + m\ddot{y}\vec{j} + m\ddot{z}\vec{k}$$

$$\vec{\lambda} = \frac{-x\vec{i} - y\vec{j} + (a-z)\vec{k}}{\sqrt{x^2 + y^2 + (a-z)^2}}$$

$$S \left[ \frac{-x\vec{i} - y\vec{j} + (a-z)\vec{k}}{a} \right] - mg\vec{k} = m\ddot{x}\vec{i} + m\ddot{y}\vec{j} + m\ddot{z}\vec{k}$$

$$(1) \quad -S\frac{x}{a} = m\ddot{x} ; \quad -S\frac{y}{a} = m\ddot{y} ; \quad S\frac{(a-z)}{a} - mg = m\ddot{z}$$

for small excursions  $a^2 = x^2 + y^2 + (a-z)^2$

$$a^2 = x^2 + y^2 + a^2 - 2az + z^2$$

$$z = \frac{1}{2a} [x^2 + y^2 + z^2] \quad \text{if } x, y \ll 1 \quad z \text{ is second order small}$$

$\therefore z$  " very small,

$$\therefore \frac{S(a)}{a} - mg = 0 \quad \boxed{S \approx mg}$$

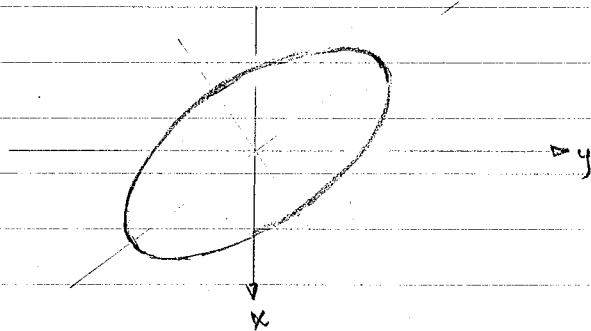
$$-\frac{mgx}{a} = m\ddot{x} ; \quad -\frac{mgy}{a} = m\ddot{y}$$

$$\ddot{x} + \frac{g}{a}x = 0 ; \quad \ddot{y} + \frac{g}{a}y = 0$$

$$x = c_1 \cos \omega t + c_2 \sin \omega t ; \quad y = c_3 \cos \omega t + c_4 \sin \omega t$$

$$\omega^2 = g/a$$

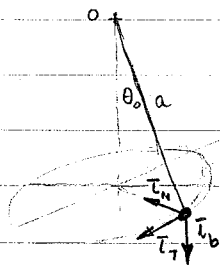
$$\omega^2 = g/a$$



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### Conical Pendulum.

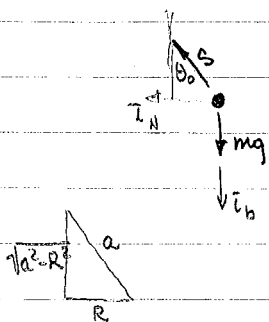
Is motion at constant  $\theta_0$  possible



$$\vec{F} = m\vec{a}$$

$$F_T \vec{e}_T + F_N \vec{e}_N + F_b \vec{e}_b = m \left[ \ddot{r} \vec{e}_T + \frac{v^2}{\rho} \vec{e}_N \right]$$

$$F_T = m \frac{dv}{dt} \quad F_N = \frac{mv^2}{\rho} \quad F_b = 0 \quad (1,2,3)$$



$$\vec{F}_T = 0 \quad \vec{F}_N = S \sin \theta_0 \quad F_b = mg - S \cos \theta_0 \quad (4)$$

$$0 = m \frac{dv}{dt} \rightarrow v = c \quad F_T \quad (5)$$

$$S \sin \theta_0 = \frac{mv^2}{R} \quad F_N \quad (6)$$

$$mg - S \cos \theta_0 = 0 \quad F_b \quad (7)$$

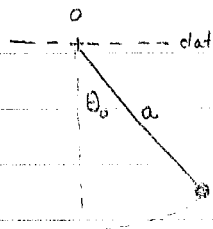
$$mg \tan \theta_0 = \frac{mv^2}{R}$$

$$\boxed{\frac{g R^2}{\sqrt{a^2 - R^2}} = v^2} \quad (8)$$

$$S \cdot \frac{R}{a} = \frac{mg R^2}{R \sqrt{a^2 - R^2}}$$

$$\boxed{S = \frac{mga}{\sqrt{a^2 - R^2}}} \quad (9)$$

Simple Pendulum. (Motion is in a plane)



Linear approximation.

$$T + V = E \quad ; \quad v = a\dot{\theta}$$

$$\frac{1}{2}ma^2\dot{\theta}^2 - mga\cos\theta = E$$

diff the exprs.

$$\frac{1}{2}ma^2 2\dot{\theta}\ddot{\theta} + mga\sin\theta\dot{\theta} = 0$$

$$\dot{\theta} [\ddot{\theta} + \frac{g}{a}\sin\theta] = 0$$

either  $\dot{\theta} = 0$

trivial

$$\ddot{\theta} + \frac{g}{a}\sin\theta = 0$$

$$\ddot{\theta} + \frac{g}{a}\theta = 0$$

if  $\theta < 10^\circ$   $\sin\theta \sim \theta$

$$\text{let } \theta = A\sin\omega t + B\cos\omega t$$

$$\omega = \sqrt{g/a}$$

$$\text{period } T = \frac{2\pi}{\omega} = 2\pi\sqrt{\frac{a}{g}}$$

Exact Solution

$$T + V = \text{const.}$$

$$\theta(0) = \alpha \quad \dot{\theta}(0) = 0$$

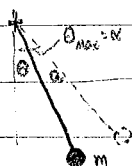
$$\frac{1}{2}ma^2\dot{\theta}^2 - mga\cos\theta = -mga\cos\alpha$$

$$\dot{\theta}^2 = \frac{2g}{a}(\cos\theta - \cos\alpha) = 2\omega^2(\cos\theta - \cos\alpha)$$

$$\dot{\theta}^2 = 4\omega^2\left(\sin^2\frac{\alpha}{2} - \sin^2\frac{\theta}{2}\right)$$

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H.W. #4.9, 4.10



$$\dot{\theta}^2 = 2\omega^2[\cos\theta - \cos\alpha]$$

$$\omega^2 = g/a$$

$$\dot{\theta}^2 = 4\omega^2\left[\sin^2\frac{\alpha}{2} - \sin^2\frac{\theta}{2}\right]$$

$$\text{let } \sin\frac{\theta}{2} = \sin\frac{\alpha}{2}\sin\phi$$

$$\text{let } k = \sin\frac{\alpha}{2}$$

$$\frac{\dot{\theta}}{2}\cos\frac{\theta}{2} = k\cos\phi\dot{\phi}$$

$$\dot{\theta}^2 = 4k^2\frac{\cos^2\phi\dot{\phi}^2}{\cos^2\frac{\theta}{2}} = 4\omega^2k^2[1 - \sin^2\phi]$$

$$\dot{\varphi}^2 = \omega^2 [1 - \sin^2 \frac{\theta}{2}] = \omega^2 [1 - k^2 \sin^2 \varphi]$$

$$\dot{\varphi} = \omega \sqrt{1 - k^2 \sin^2 \varphi}$$

$$dt = \frac{1}{\omega} \frac{d\varphi}{\sqrt{1 - k^2 \sin^2 \varphi}}$$

$$t = \int \frac{1}{\omega} \frac{d\varphi}{\sqrt{1 - k^2 \sin^2 \varphi}} + C \quad \text{period.}$$

$$\text{Period} = P = 4 \frac{1}{\omega} \int_0^{\pi/2} \frac{d\varphi}{\sqrt{1 - k^2 \sin^2 \varphi}}$$

$$\begin{array}{l} \theta = \alpha \\ \varphi = 0 \end{array} \quad \begin{array}{l} \theta = 0 \\ \varphi = \pi/2 \end{array}$$

$$T = 4 \frac{1}{\omega} \int_0^{\pi/2} \frac{d\varphi}{\sqrt{1 - k^2 \sin^2 \varphi}}$$

$$\int_0^{\pi/2} \frac{d\varphi}{\sqrt{1 - k^2 \sin^2 \varphi}} = \frac{2\pi}{\omega} \left[ 1 + \left(\frac{1}{2}\right)^2 k^2 + \left(\frac{1 \cdot 3}{2 \cdot 4}\right)^2 k^4 + \left(\frac{1 \cdot 3 \cdot 5}{2 \cdot 4 \cdot 6}\right)^2 k^6 + \dots \right]$$

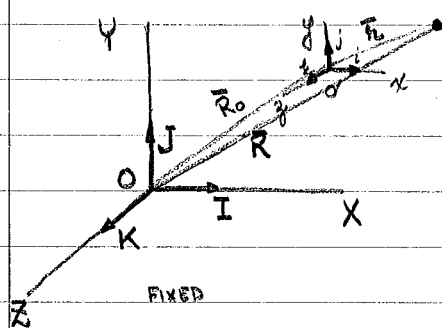
$$k \sim \alpha/2$$

$$T \approx \frac{2\pi}{\omega} \left[ 1 + \frac{\alpha^2}{16} \right] \approx 2\pi \sqrt{\frac{a}{g}} \left[ 1 + \frac{\alpha^2}{16} \right] \quad \text{soft spring.}$$

as  $\alpha \uparrow$   $T \uparrow$  causing the pendulum to slow down.

### Moving Frames of Reference

#### A. Frames in Translation Only



OXYZ - fixed

O'xyz - translating frame.

$$\bar{R} = \bar{R}_0 + \bar{r}$$

$$\bar{R} = X\bar{I} + Y\bar{J} + Z\bar{K} + x\bar{i} + y\bar{j} + z\bar{k}$$

$$\bar{V}_{abs} = \frac{d\bar{R}}{dt} = \dot{X}\bar{I} + \dot{Y}\bar{J} + \dot{Z}\bar{K} + \dot{x}\bar{i} + \dot{y}\bar{j} + \dot{z}\bar{k}$$

$$\bar{V}_{abs} = \frac{d\bar{R}_0}{dt} + \frac{d\bar{r}}{dt} = \bar{V}_0 + \bar{v}$$

$$\bar{a}_{abs} = \bar{A}_0 + \bar{a}$$

In translating frame  $I, \bar{i}; J, \bar{j}; K, \bar{k}$  are the same we can then write

$$\bar{R} = (X+x, Y+y, Z+z)$$

$$\bar{F} = m\bar{a} = m[\ddot{\bar{R}}_0 + \ddot{\bar{r}}]$$

$$[\bar{F} - m\ddot{\bar{R}}_0] = m\ddot{\bar{r}}$$

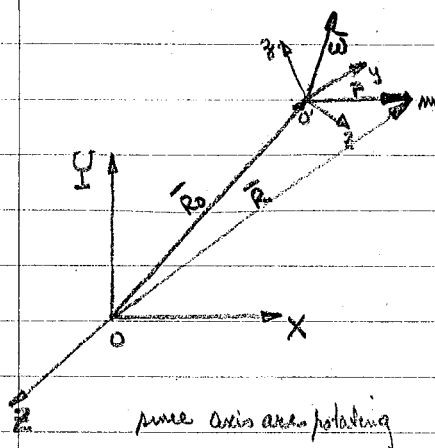
inertia force

### A. General Frame of Motion

$OXYZ$  - fixed

$O'xyz$  - moving

$\bar{\omega}$  - axis of rotation



$$\bar{R} = \bar{R}_0 + \bar{r}$$

$$\bar{V}_{abs} = \frac{d\bar{R}}{dt} = \underbrace{\frac{d\bar{R}_0}{dt}}_{\text{vel of } O'} + \underbrace{\frac{d\bar{r}}{dt}}_{\text{vel of } m \text{ w.r.t } O'}$$

$$\frac{d\bar{R}_0}{dt} = \dot{X}\bar{I} + \dot{Y}\bar{J} + \dot{Z}\bar{K}$$

$$\frac{d\bar{r}}{dt} = \dot{x}\bar{i} + x\frac{d\bar{i}}{dt} + \dot{y}\bar{j} + y\frac{d\bar{j}}{dt} + \dot{z}\bar{k} + z\frac{d\bar{k}}{dt}$$

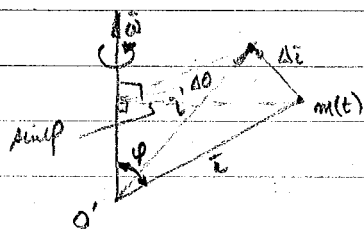
$$= (\dot{x}\bar{i} + \dot{y}\bar{j} + \dot{z}\bar{k}) + (x\frac{d\bar{i}}{dt} + y\frac{d\bar{j}}{dt} + z\frac{d\bar{k}}{dt})$$

$\downarrow$   
v of translation  
relative velocity

$\downarrow$   
v of rotation of axes.

$$= \left( \frac{\delta \bar{r}}{\delta t} \right) + (\bar{\omega} \times \bar{r})$$

$$\bar{V}_{abs} = \frac{d\bar{R}}{dt} = \bar{V}_0 + \frac{\delta \bar{r}}{\delta t} + (\bar{\omega} \times \bar{r})$$



$$\left| \frac{d\bar{i}}{dt} \right| = \lim_{\Delta t \rightarrow 0} \left| \frac{\Delta \bar{i}}{\Delta t} \right|$$

$$= \lim_{\Delta t \rightarrow 0} \left| \frac{\sin \phi \Delta \theta}{\Delta t} \right| = \sin \phi \omega = \bar{\omega} \times \bar{i}$$

$$x\frac{d\bar{i}}{dt} + y\frac{d\bar{j}}{dt} + z\frac{d\bar{k}}{dt} = x(\bar{\omega} \times \bar{i}) + y(\bar{\omega} \times \bar{j}) + z(\bar{\omega} \times \bar{k})$$

$$= \bar{\omega} \times (x\bar{i} + y\bar{j} + z\bar{k}) = \bar{\omega} \times \bar{r}$$

$\bar{A}$  - moving frame of reference

$$\frac{d}{dt} [\bar{A}] = \frac{\delta [\bar{A}]}{\delta t} + \bar{\omega} \times [\bar{A}]$$

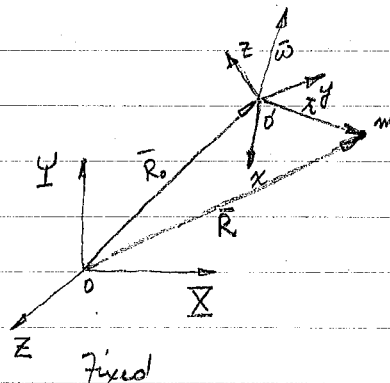
In Summary

$$\bar{R} = \bar{R}_0 + \bar{r}$$

$$\bar{V}_{abs} = \bar{V}_0 + \frac{\delta \bar{r}}{\delta t} + \bar{\omega} \times \bar{r}$$

$$\begin{aligned} \bar{a}_{abs} &= \bar{R}_0'' + \frac{\delta}{\delta t} \left[ \frac{\delta \bar{r}}{\delta t} + \bar{\omega} \times \bar{r} \right] + \bar{\omega} \times \left\{ \frac{\delta \bar{r}}{\delta t} + \bar{\omega} \times \bar{r} \right\} \\ &= \bar{R}_0'' + \underbrace{\frac{\delta^2 \bar{r}}{\delta t^2}}_{\text{relative acc.}} + \underbrace{\frac{\delta \bar{\omega}}{\delta t} \times \bar{r}}_{\text{transverse}} + \underbrace{2\bar{\omega} \times \frac{\delta \bar{r}}{\delta t}}_{\text{Coriolis}} + \underbrace{\bar{\omega} \times (\bar{\omega} \times \bar{r})}_{\text{Centrifugal accel.}} \end{aligned}$$

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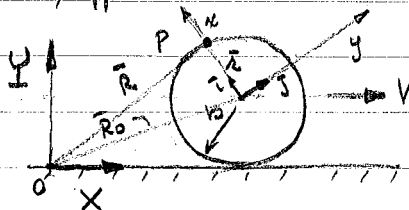
$$\bar{R} = \bar{R}_0 + \bar{r}$$

$$\bar{V}_{abs} = \frac{d\bar{R}}{dt} = \frac{d\bar{R}_0}{dt} + \frac{\delta \bar{r}}{\delta t} + \bar{\omega} \times \bar{r}$$

$$\bar{a}_{abs} = \frac{d^2 \bar{R}}{dt^2} = \underbrace{\bar{R}_0''}_{\text{accel of } o} + \underbrace{\frac{\delta^2 \bar{r}}{\delta t^2}}_{\text{relative acc.}} + \underbrace{\frac{\delta \bar{\omega}}{\delta t} \times \bar{r}}_{\text{transverse}} + \underbrace{2\bar{\omega} \times \frac{\delta \bar{r}}{\delta t}}_{\text{Coriolis}} + \underbrace{\bar{\omega} \times (\bar{\omega} \times \bar{r})}_{\text{Centrifugal}}$$

Example:

Suppose I have a wheel (rad.  $b$ ) rolling in a straight line at  $V$  (const).



$$\bar{r} = b\bar{i}$$

$$\frac{\delta \bar{r}}{\delta t} = 0 = \frac{\delta^2 \bar{r}}{\delta t^2}$$

$$\bar{\omega} = \frac{V}{b} \bar{k}$$

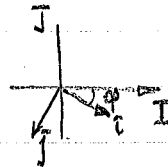
$$\frac{\delta \bar{\omega}}{\delta t} = 0$$

$$\frac{d\bar{R}_0}{dt} = V$$

$$\bar{a}_{abs} = 0 + 0 + 0 + 0 + \frac{V}{b} \bar{k} \times \left( \frac{V}{b} \bar{k} \times b\bar{i} \right) = \frac{V}{b} \bar{k} \times (V\bar{j}) = -\frac{V^2}{b} \bar{i}$$

What is  $\vec{v}_{abs}$  of point P?

$$\begin{aligned}\vec{v}_{abs} &= \frac{d\vec{R}_0}{dt} + \frac{\delta \vec{r}}{\delta t} + \vec{\omega} \times \vec{r} \\ &= V\vec{i} + 0 + V\vec{j}\end{aligned}$$

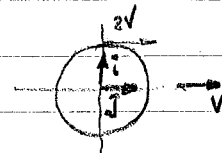


$$\vec{i} = \vec{r} \cos \varphi - \vec{j} \sin \varphi$$

$$\vec{v}_{abs} = V \cos \varphi \vec{i} + V(1 - \sin \varphi) \vec{j}$$

$$\text{for } \varphi = 270^\circ \quad \vec{v} = V(0 + (1+1)\vec{j}) = 2V\vec{j}$$

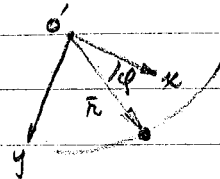
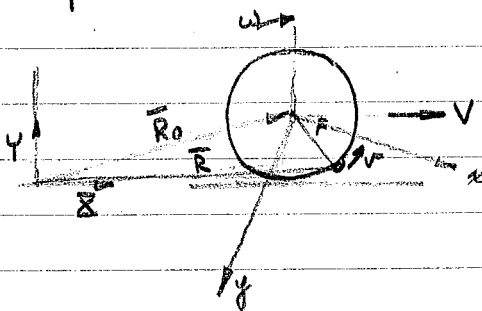
$$\text{for } \varphi = 90^\circ \quad \vec{v} = V(0 + (1-1)\vec{j}) = 0$$



Example:

wheel, rad.  $b$ , uniform speed  $V$ .

calculate acceleration on bug  
bug moving at unif speed  $u$



$$\vec{r} = r \cos \varphi \vec{i} + r \sin \varphi \vec{j}$$

$$\frac{\delta \vec{r}}{\delta t} = -r \dot{\varphi} \sin \varphi \vec{i} + r \dot{\varphi} \cos \varphi \vec{j} \quad \text{but } -r \dot{\varphi} = u$$

$$\frac{\delta^2 \vec{r}}{\delta t^2} = -r \dot{\varphi}^2 \cos \varphi \vec{i} - r \dot{\varphi}^2 \sin \varphi \vec{j} = -\frac{u^2}{r} (\cos \varphi \vec{i} + \sin \varphi \vec{j})$$

$$\vec{\omega} = \frac{V}{b} \vec{k}$$

$$\vec{\omega} \times \vec{r} = \frac{V}{b} \vec{k} \times (r \cos \varphi \vec{i} + r \sin \varphi \vec{j})$$

$$\vec{\omega} \times \vec{r} = \frac{Vr}{b} \cos \varphi \vec{j} - \frac{Vr}{b} \sin \varphi \vec{i}$$

$$\vec{\omega} \times (\vec{\omega} \times \vec{r}) = \frac{V}{b} \vec{k} \times (\vec{\omega} \times \vec{r}) = -\frac{V^2 r}{b^2} \cos \varphi \vec{i} - \frac{V^2 r}{b^2} \sin \varphi \vec{j}$$

$$\text{but } b=r \quad \therefore \vec{\omega} \times (\vec{\omega} \times \vec{r}) = -\frac{V^2}{b} \cos \varphi \vec{i} - \frac{V^2}{b} \sin \varphi \vec{j}$$



$$\vec{a}_{abs} = \frac{d\vec{R}_0}{dt^2} + \frac{\delta^2 \vec{r}}{\delta t^2} + \frac{\delta \vec{\omega}}{\delta t} \times \vec{r} + 2\vec{\omega} \times \frac{\delta \vec{r}}{\delta t} + \vec{\omega} \times (\vec{\omega} \times \vec{r})$$

$$= 0 - \frac{v^2}{b} (\cos \phi \vec{i} + \sin \phi \vec{j}) + 0 + 2\frac{V}{b} \vec{k} \times (v \sin \phi \vec{i} - v \cos \phi \vec{j})$$

$$- \frac{v^2}{b} (\cos \phi \vec{i} + \sin \phi \vec{j})$$

$$= -\frac{v^2}{b} (\cos \phi \vec{i} + \sin \phi \vec{j}) + \frac{2Vv}{b} (\sin \phi \vec{j} + \cos \phi \vec{i}) - \frac{v^2}{b} (\cos \phi \vec{i} + \sin \phi \vec{j})$$

$$= -\frac{\cos \phi \vec{i}}{b} [(v-V)^2] - \frac{\sin \phi \vec{j}}{b} [(v-V)^2]$$

$$= -\frac{1}{b} [(v-V)^2] \{ \cos \phi \vec{i} + \sin \phi \vec{j} \}$$

$$\text{If } \phi = 0 \quad \vec{a}_{abs} = -\frac{1}{b} [(v-V)^2] \vec{i}$$

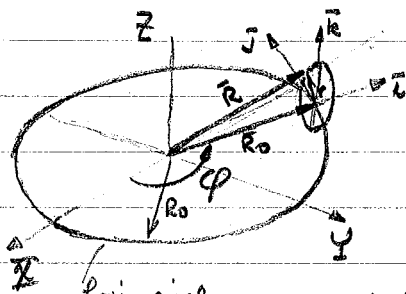
Force on Bug.

$$\vec{F} = m\vec{a}_{abs}$$

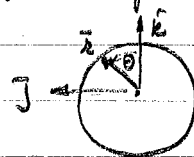
$$\therefore \vec{F} = -\frac{m}{b} (v-V)^2 \vec{i}$$

$$\vec{F} = \frac{m(v-V)^2}{b}$$

Example: wheel moves in a circle at uniform speed  $V$  (rad/s) circle rad  $R_0$



$\vec{k}$  is always vertical  $\vec{j}$  is tangent to traj of axis of wheel.  $\vec{i}$  in  $\vec{R}_0$  direct  $\vec{j}$  is horiz.



$$\vec{v} = \frac{d\vec{R}_0}{dt} + \frac{\delta \vec{r}}{\delta t} + \vec{\omega} \times \vec{r}$$

$$\frac{d\vec{R}_0}{dt} = V\vec{j}$$

$$\text{note } V = b\dot{\theta} = R_0\dot{\phi}$$

$$\vec{r} = b \cos \theta \vec{k} + b \sin \theta \vec{j}$$

$$\frac{\delta \vec{r}}{\delta t} = -V \sin \theta \vec{k} + V \cos \theta \vec{j}$$

$$\vec{\omega} = \frac{V}{R_0} \vec{k}$$

$$\begin{aligned}\vec{\omega} \times \vec{r} &= \frac{V}{R_0} \vec{k} \times b (\cos \theta \vec{k} + \sin \theta \vec{j}) \\ &= \frac{Vb}{R_0} (-\sin \theta \vec{i})\end{aligned}$$

$$\begin{aligned}\vec{v} &= V \vec{j} + V (-\sin \theta \vec{k} + \cos \theta \vec{j}) - \frac{Vb}{R_0} (\sin \theta \vec{i}) \\ &= V \left[ (1 + \cos \theta) \vec{j} - \frac{b}{R_0} \sin \theta \vec{i} - \sin \theta \vec{k} \right]\end{aligned}$$

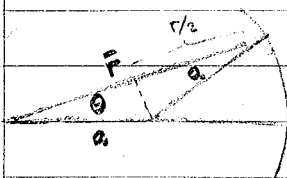
$$\text{when } \theta = 0 \quad \vec{v} = V [2\vec{j}]$$

$$\text{when } \theta = 90^\circ \quad \vec{v} = V \left[ \vec{j} - \frac{b}{R_0} \vec{i} - \vec{k} \right]$$

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Ch. 5-1-5-7

Test.



$$\cos \theta = \frac{r}{2a}$$

$$r = 2a \cos \theta$$

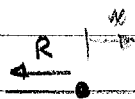
$$\dot{r} = -2a \dot{\theta} \sin \theta$$

$$\ddot{r} = -2a \ddot{\theta} \cos \theta$$

$$a_r = -2a \dot{\theta}^2 \cos \theta - 2a \cos \theta \ddot{\theta} = -4a \dot{\theta}^2 \cos \theta$$

$$a_\theta = 2(-2a \dot{\theta} \sin \theta) \dot{\theta} = -4a \dot{\theta}^2 \sin \theta$$

$$|a| = \sqrt{a_r^2 + a_\theta^2} = \sqrt{16a^2 \dot{\theta}^4} = 4a \dot{\theta}^2$$



$$-mcv = m \frac{dv}{ds}$$

$$-cds = dv$$

$$-cs = v + B$$

$$-cx = v - v_0$$

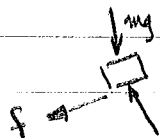
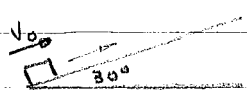
$$x_{\max} = \frac{v_0}{c}$$

$$-mcv = m \frac{dv}{dt}$$

$$-cdt = \frac{dv}{v}$$

$$-ct = \ln \left( \frac{v}{v_0} \right)$$

$$\text{when } v=0 \quad \ln 0 = -ct \quad t = \infty$$

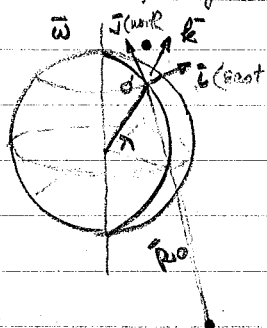


$$-f - mg \sin \theta = \bar{F}$$

$$(-\mu mg \cos \theta - mg \sin \theta) dx = -\frac{m v_0^2}{2}$$

$$x_{\max} = \frac{v_0^2}{2g(\mu \cos \theta + \sin \theta)} = 16.5 \text{ ft.}$$

Motion of Projectile near surface of Earth.



$$x_0 = y_0 = z_0 = 0$$

$$\dot{x}(0) = \dot{x}_0; \dot{y}(0) = \dot{y}_0; \dot{z}(0) = \dot{z}_0$$

$$\bar{F} = m\bar{a}$$

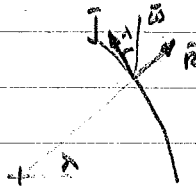
$$-mg\bar{k} = m \left\{ \frac{d^2 \bar{r}_0}{dt^2} + \frac{\delta^2 \bar{r}}{\delta t^2} + \frac{\delta \bar{\omega}}{\delta t} \times \bar{r}_0 + 2\bar{\omega} \times \frac{\delta \bar{r}}{\delta t} + \bar{\omega} \times (\bar{\omega} \times \bar{r}) \right\}$$

$\frac{\delta \bar{\omega}}{\delta t} \times \bar{r}_0$ ;  $\frac{d^2 \bar{r}_0}{dt^2}$  is small & can be neglected. so can  $\bar{\omega}(\bar{\omega} \times \bar{r})$

$$m \frac{\delta^2 \bar{r}}{\delta t^2} = -mg\bar{k} - m 2\bar{\omega} \times \frac{\delta \bar{r}}{\delta t}$$

$$\frac{\delta^2 \bar{r}}{\delta t^2} = -g\bar{k} - 2\bar{\omega} \times \frac{\delta \bar{r}}{\delta t} \quad (1)$$

$$\ddot{x}\bar{i} + \ddot{y}\bar{j} + \ddot{z}\bar{k} = -g\bar{k}$$



$$\bar{\omega} = \omega \cos \lambda \bar{j} + \omega \sin \lambda \bar{k}$$

$$\bar{r} = x\bar{i} + y\bar{j} + z\bar{k}$$

$$\frac{\delta \bar{r}}{\delta t} = \dot{x}\bar{i} + \dot{y}\bar{j} + \dot{z}\bar{k} \quad (2)$$

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Exam on 3/25 Start reading chapter 6.

└ Pendulum, Moving Frames, Central Forces.

$$\frac{\delta^2 \bar{h}}{\delta t^2} = \ddot{x} \bar{i} + \ddot{y} \bar{j} + \ddot{z} \bar{k}$$

$$-2\omega \times \frac{\delta \bar{h}}{\delta t} = -2\omega \begin{vmatrix} \bar{i} & \bar{j} & \bar{k} \\ 0 & \cos \lambda & \sin \lambda \\ \dot{x} & \dot{y} & \dot{z} \end{vmatrix}$$

$$-2\omega \left[ (\dot{z} \cos \lambda - \dot{y} \sin \lambda) \bar{i} - (0 - \dot{x} \sin \lambda) \bar{j} + (0 - \dot{x} \cos \lambda) \bar{k} \right] \quad (3)$$

$$\ddot{x} \bar{i} + \ddot{y} \bar{j} + \ddot{z} \bar{k} = -g \bar{k} - 2\omega \left[ (\dot{z} \cos \lambda - \dot{y} \sin \lambda) \bar{i} + (\dot{x} \sin \lambda) \bar{j} - (\dot{x} \cos \lambda) \bar{k} \right]$$

$$\ddot{x} = -2\omega (\dot{z} \cos \lambda - \sin \lambda \dot{y}) \quad (4)$$

$$\ddot{y} = -2\omega (\dot{x} \sin \lambda) \quad (5)$$

$$\ddot{z} = -g + 2\omega \dot{x} \cos \lambda \quad (6)$$

Integrate 5 & 6.

$$\dot{y} = -2\omega \sin \lambda x + \dot{y}_0 \quad (7)$$

$$\dot{z} = -gt + 2\omega \cos \lambda x + \dot{z}_0 \quad (8)$$

$$\ddot{x} = -2\omega \left( -gt \cos \lambda + 2\omega \cos^2 \lambda x + \dot{z}_0 \cos \lambda + 2\omega \sin^2 \lambda x - \dot{y}_0 \sin \lambda \right)$$

but  $2\omega$  terms is small so we can neglect it

$$\ddot{x} = -2\omega \left[ \cos \lambda (-gt + \dot{z}_0) - \sin \lambda (\dot{y}_0) \right]$$

$$\dot{x} = -2\omega \left[ \cos \lambda \left( -gt \frac{t^2}{2} + \dot{z}_0 t \right) - \sin \lambda (\dot{y}_0 t) \right] + \dot{x}_0$$

$$x = -2\omega \left[ \cos \lambda \left( -gt \frac{t^3}{6} + \dot{z}_0 \frac{t^2}{2} \right) - \sin \lambda \left( \dot{y}_0 \frac{t^2}{2} \right) \right] + \dot{x}_0 t + x_0 \quad (10)$$

10 into 7 and 8

$$y = \dot{y}_0 t - \omega \sin \lambda \dot{x}_0 t$$

$$z = -\frac{1}{2}gt^2 + \dot{z}_0 t + \omega \cos \lambda \dot{x}_0 t^2 \quad \left. \begin{array}{l} \\ \end{array} \right\} \text{neglecting } \omega^2 \text{ terms.}$$

fire from origin at  $V_0$  vertically.

$$x_0 = y_0 = z_0 = 0$$

$$\dot{x}_0 = \dot{y}_0 = \dot{z}_0 = v_0$$

$$x = -2\omega \left[ \cos \lambda \left( -\frac{gt^3}{6} + \frac{v_0 t^2}{2} \right) \right] \quad (1) \quad y = 0 \quad z = -\frac{1}{2}gt^2 + v_0 t \quad (3)$$

$$\dot{z} = -gt + v_0 = 0 \quad ; \quad t_1 = \frac{v_0}{g} \quad (4) \quad ; \quad x_1 = \frac{\omega \cos \lambda}{3} \left[ g \frac{v_0^3}{g^3} \right] - \omega v_0 \frac{v_0^2}{g^2} \cos \lambda$$

$$y_1 = 0 \quad ; \quad z_1 = -\frac{1}{2} \frac{v_0^2}{g} + \frac{v_0^2}{g} = \frac{1}{2} \frac{v_0^2}{g} \quad (7) \quad = -\frac{2}{3} \omega \cos \lambda \frac{v_0^3}{g^2} \quad (5)$$

Down assume start at origin  $\dot{x}_0 = \dot{y}_0 = \dot{z}_0 = 0$

$$x = \frac{1}{3} \omega g t^3 \cos \lambda \quad y = 0 \quad z = -\frac{1}{2} g t^2$$

when  $z = -\frac{1}{2} \frac{v_0^2}{g}$   $t_2$  is time of fall.

$t_2$  turns out to be  $\frac{v_0}{g}$

$$x_2 = \frac{1}{3} \omega g \frac{v_0^3}{g^3} \cos \lambda = \frac{1}{3} \omega \frac{v_0^3}{g^2} \cos \lambda$$

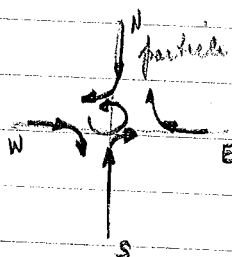
$$x = x_1 + x_2 = -\frac{1}{3} \omega \cos \lambda \frac{v_0^3}{g^2}$$

$$v_2 = 0$$

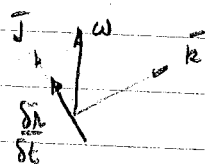
$$z_2 = -\frac{1}{2} \frac{v_0^2}{g}$$

$$\boxed{\begin{aligned} x &= -\frac{1}{3} \omega \cos \lambda \frac{v_0^3}{g^2} \\ z_{TOT} &= 0 \quad y_{TOT} = 0 \end{aligned}}$$

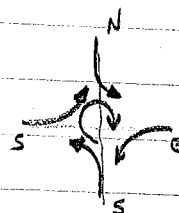
Suppose a particle moves north.

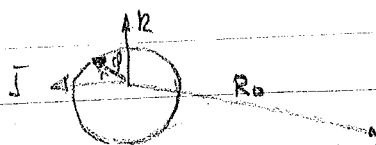


in southern hemisphere

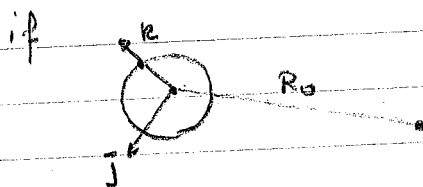


tends to curve around to east in northern hemisphere.



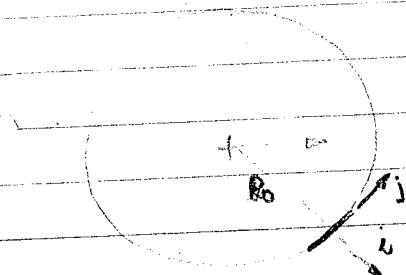


$2\bar{\omega} \times \frac{\delta \bar{r}}{\delta t}$  exists due to rotation



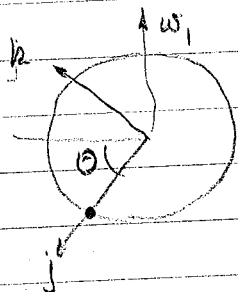
$\bar{r} = b\bar{k}$   $\bar{\omega} \times \frac{\delta \bar{r}}{\delta t}$  does not exist here due

in case 1



$$\bar{\omega} = \frac{v}{R_0} \bar{k}$$

in case 2



$$\bar{\omega} = \omega_1 (-\sin\theta \bar{j} + \cos\theta \bar{i}) + \omega_2 \bar{k}$$

$b = \text{rad of wheel}$

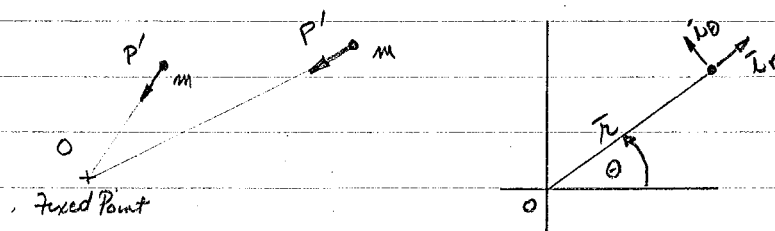
$$\bar{r} = b\bar{j}$$

$$\frac{\delta \bar{r}}{\delta t} = \frac{\delta \bar{r}'}{\delta t'} = 0$$

$$\frac{\delta \bar{\omega}}{\delta t} \times \bar{r} = 0$$

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# Central Force Systems.



Angular Momentum  $\vec{h}_O = \vec{r} \times m\vec{v}$

$$\frac{d\vec{h}_O}{dt} = \underbrace{\vec{v} \times m\vec{v}}_0 + \vec{r} \times m \frac{d\vec{v}}{dt} = \vec{r} \times \vec{F} = 0 \text{ in a central force system.}$$

Therefore  $\vec{h}_O = \text{constant}$ .

Motion is planar since  $\vec{h}_O \perp \vec{r}$  &  $\perp m\vec{v}$

from this  $m r_1 v_1 \sin \phi_1 = m r_2 v_2 \sin \phi_2$

$v_1 \sin \phi_1 = v_0$   $v_2 \sin \phi_2 = v_0$

$\vec{F} = m\vec{a} = \frac{d}{dt}(m\vec{v})$  also  $\vec{M} = \frac{d}{dt}(\vec{h})$

$\vec{F} = m\vec{a}$

$$F_r \hat{r}_r + F_\theta \hat{r}_\theta = m [\ddot{r} - r\dot{\theta}^2] \hat{r}_r + m \left[ \frac{1}{r} \frac{d}{dt} (r^2 \dot{\theta}) \right] \hat{r}_\theta$$

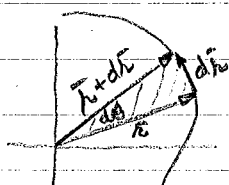
$F_r = m(\ddot{r} - r\dot{\theta}^2)$  ①

$F_\theta = m \left( \frac{1}{r} \frac{d}{dt} [r^2 \dot{\theta}] \right)$  ②

$F_\theta = 0 \Rightarrow \frac{d}{dt} (r^2 \dot{\theta}) = 0$   $r^2 \dot{\theta} = h = \text{constant}$  ③

but  $r^2 \dot{\theta} = r v_\theta$

note:



$dA = \frac{1}{2} r^2 d\theta$

$\frac{dA}{dt} = \frac{1}{2} r^2 \frac{d\theta}{dt} = \frac{1}{2} r^2 \dot{\theta} = \text{const.}$

$F_r = -mP$   
 $= (\ddot{r} - r\dot{\theta}^2) m$

$P' = mP$

$$P = \dot{r} - r\dot{\theta}^2$$

$$\text{let } r = \frac{1}{u} \quad \dot{\theta} = \frac{h}{r^2} = hu^2$$

$$\frac{dr}{dt} = \frac{d}{d\theta} \left( \frac{1}{u} \right) \frac{d\theta}{dt} = hu^2 \left( -\frac{du}{d\theta} \right) \frac{1}{u^2} = -h \frac{du}{d\theta}$$

$$\frac{d\dot{r}}{dt} = \frac{d}{d\theta} \left( -h \frac{du}{d\theta} \right) \frac{d\theta}{dt} = \dot{\theta} \left( -h \frac{d^2u}{d\theta^2} \right) = -hu^2 \frac{d^2u}{d\theta^2}$$

$$-P = -h^2 u^2 \frac{d^2u}{d\theta^2} - \frac{1}{u} h^2 u^4 ; \quad \boxed{\frac{P}{h^2 u^2} = \frac{d^2u}{d\theta^2} + u} \quad (4)$$

Energy form of equation of motion

$$T + V = E$$

$$\frac{1}{2} u^2 + V = E$$

for unit mass

$$\frac{1}{2} [\dot{r}^2 + (r\dot{\theta})^2] = E - V$$

$$h^2 \left( \frac{du}{d\theta} \right)^2 + \left( \frac{1}{u} h u^4 \right)^2 = \frac{2(E - V)}{1}$$

$$\left( \frac{du}{d\theta} \right)^2 + u^2 = \frac{2(E - V)}{h^2} \quad (5)$$

$$\frac{d}{dt} \text{ of eq 5} = \text{eq 4}$$

Try Problems 4-17, 19, 21



3/16/71

$$\frac{d^2 u}{d\theta^2} + u = \frac{P(u)}{h^2 u^2}$$

or

$$\left(\frac{du}{d\theta}\right)^2 + u^2 = \frac{2(E-V)}{h^2}$$

Orbits in Inverse Square Force Fields

$$P = \frac{\mu}{r^2} = \mu u^2$$

$$\frac{d^2 u}{d\theta^2} + u = \frac{\mu}{h^2}$$

$$u_h = A \cos \theta + B \sin \theta \quad u_p = \mu/h^2$$

$$u = A \cos \theta + B \sin \theta + \mu/h^2$$

or

$$u = C \cos(\theta - \theta_0) + \frac{\mu}{h^2}$$

Arbitrary constants from initial conditions

$$E(t=0); \vec{v}(t=0) \rightarrow r_0, \theta_0, v_r, v_\theta$$

set up coordinate system so that  $\theta_0 = 0$

Rotate axes to make  $\theta_0 = 0$

$$u = C \cos \theta + \mu/h^2$$

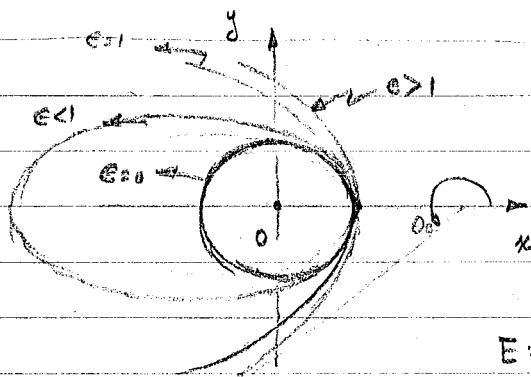
$$u = \mu/h^2 [1 + e \cos \theta] \quad e = \frac{Ch^2}{\mu}$$

$$u = \frac{1}{l} [1 + e \cos \theta] \quad l = \mu/h^2$$

$1 + e \cos \theta$  equation of conic section with one of foci at origin in terms of  $E$  &  $h$

$$e = \sqrt{1 + \frac{2Eh^2}{\mu^2}}$$

for earth orbits  $P = \mu/h^2 = \frac{GM}{h^2} = \frac{gR^2}{h^2}$  where  $\mu = 1.41 \times 10^{16} \frac{\text{ft}^3}{\text{sec}^2}$



|         |           |         |
|---------|-----------|---------|
| $e > 1$ | hyperbola | $E > 0$ |
| $e = 1$ | parabola  | $E = 0$ |
| $e < 1$ | ellipse   | $E < 0$ |
| $e = 0$ | circle    | "       |

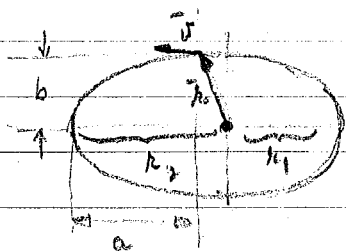
$$\frac{du}{d\theta} = 0$$

$$E = T + V = \frac{v^2}{2} - \frac{\mu}{r} \quad \text{grav. potential}$$

as  $r \rightarrow \infty \quad E \rightarrow \frac{v^2}{2} > 0; \quad v = \sqrt{2E}$

Escape velocity as  $r \rightarrow \infty \quad v \rightarrow 0 \quad E \rightarrow 0$

### Elliptic Orbits



$$a = \frac{1}{2}(r_1 + r_2) = \frac{1}{2}\left(\frac{l}{1+e} + \frac{l}{1-e}\right)$$

$$\rightarrow a = \frac{l}{1-e^2} = \frac{h^2}{\mu \left[1 - \left(1 + \frac{2Eh^2}{\mu^2}\right)\right]} = -\frac{\mu}{2E}$$

$$b = a\sqrt{1-e^2} \quad \text{further} \quad a = \frac{l}{1-e^2} \quad b = \sqrt{\frac{l^2}{1-e^2}} = \sqrt{-\frac{h^2}{2E}}$$

$$v^2 = 2\left(E + \frac{\mu}{r}\right) = -\frac{\mu}{a} + \frac{2\mu}{r}$$

$$\boxed{v^2 = \mu \left[ \frac{2}{r} - \frac{1}{a} \right]}$$

$$\frac{dA}{dt} = \frac{h}{2} \quad \int_0^T dt = \int \frac{2}{h} dA$$

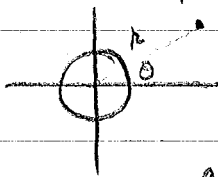
$$T = \frac{2}{h} \pi ab$$

$$T^2 = \frac{4}{h^2} \pi^2 a^2 b^2 = \frac{4\pi^2}{h^2} a^2 \left(-\frac{h^2}{2E}\right) = \frac{4\pi^2 a^2}{-\mu/a} = \frac{4\pi^2}{\mu} a^3$$

$$T = 2\pi \sqrt{\frac{a^3}{\mu}}$$

# Elementary Problems in Space Mechanics (Use Conservation of Energy & Momentum Theorems)

## Escape Velocity



Def:  $v_e$   $r \rightarrow \infty$   $v \rightarrow 0$

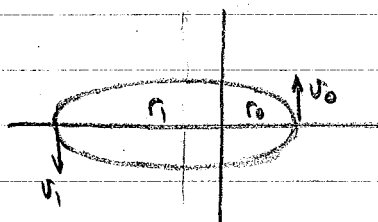
$$E=0 = \frac{v_e^2}{2} - \frac{gR^2}{r}$$

$$\text{at } r=r_0 \quad v_{e_0}^2 = \frac{2gR^2}{r_0} \quad v_{e_0} = \sqrt{\frac{2gR^2}{r_0}}$$

$$\text{at } r_0=R \quad v_e = \sqrt{2gR} \quad \text{at earth's surface, } \approx 25000 \text{ mph.}$$

$$1.467 \text{ mph} = 1 \text{ ft/sec}$$

$$v_{e_0} = v_e \sqrt{\frac{R}{r_0}} \quad R = 3960 \text{ miles}$$



$$\frac{v_1^2}{2} - \frac{gR^2}{r_1} = \frac{v_0^2}{2} - \frac{gR^2}{r_0}$$

$$r_0 v_0 = r_1 v_1$$

$$\frac{v_0^2}{2} - \frac{gR^2}{r_0} = \frac{1}{2} \left( \frac{r_0}{r_1} v_0 \right)^2 - \frac{gR^2}{r_1}$$

$$v_0^2 \left( 1 - \frac{r_0^2}{r_1^2} \right) = \frac{2gR^2}{r_0} \left( 1 - \frac{r_0}{r_1} \right)$$

$$v_0^2 \left( 1 + \frac{r_0}{r_1} \right) = \frac{2gR^2}{r_0}$$

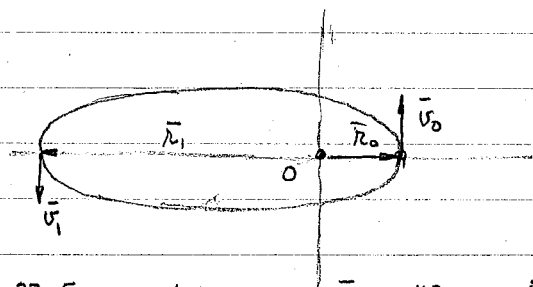
$$\boxed{\frac{r_0}{r_1} = \frac{2gR^2}{r_0 v_0^2} - 1}$$

$$\frac{v_1}{v_0} = \frac{r_0}{r_1}$$

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Do problems 1, 2, 3

Example:



$$v_0 = 22,500 \text{ mph}$$

$$r_0 = 4300 \text{ miles}$$

$$\textcircled{1} \quad \frac{v_0^2}{2} - \frac{\mu}{r_0} = \frac{v_1^2}{2} - \frac{\mu}{r_1}$$

$$\textcircled{2} \quad v_0 r_0 = v_1 r_1 \quad (h = r^2 \dot{\theta} = r v_{\theta})$$

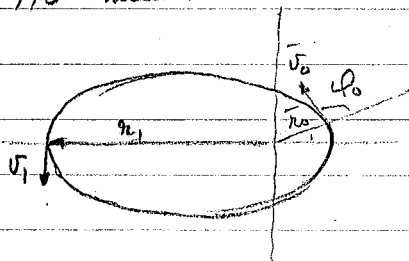
$$\frac{r_0}{r_1} = \frac{2(qR^2)}{r_0 v_0^2} - 1 = \frac{v_0^2 R}{r_0 v_0^2} - 1 = \left(\frac{25000}{22500}\right)^2 \frac{3960}{4300} - 1$$

$$\frac{r_0}{r_1} = 1.139 - 1 = .139$$

$$r_1 = \frac{4300}{.139} = 30,950 \quad h_1 = 26,990 \text{ miles}$$

$$v_1 = \frac{r_0}{r_1} v_0 = .139 (22500) =$$

How much error in  $\phi_0$  of satellite is not to come closer than 140 miles



$$\frac{v_1^2}{2} - \frac{\mu}{r_1} = \frac{v_0^2}{2} - \frac{\mu}{r_0}$$

$$r_1 v_1 = r_0 v_0 \sin \phi_0$$

$$r_1 = 4100 \quad r_0 = 4300$$

$$\frac{1}{2} \left( \frac{r_0 v_0 \sin \phi_0}{r_1} \right)^2 - \frac{gR^2}{r_1} = \frac{v_0^2}{2} - \frac{gR^2}{r_0}$$

$$\left( \frac{r_0}{r_1} \right)^2 v_0^2 \sin^2 \phi_0 = v_0^2 + \frac{2gR^2}{r_1} \left( 1 - \frac{r_1}{r_0} \right)$$

$$\frac{r_0}{r_1} = 1.0488$$

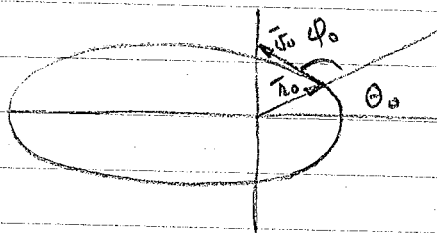
$$v_0 = 33,000 \text{ ft/sec}$$

$$(33 \times 10^3)^2 \left[ (1.0488)^2 \sin^2 \phi_0 - 1 \right] = \frac{2(1.408) \times 10^{16}}{4100(5280)} \left[ 1 - \frac{1}{1.0488} \right]$$

$$\sin \phi_0 = 0.9796$$

$$\phi_0 = 78.4^\circ$$

$$\text{true } \phi_0 = 90^\circ \pm 11.6^\circ$$



Given  $r_0$  &  $v_0$  what is equation of trajectory

$$u = \frac{\mu}{h^2} [1 + e \cos(\theta - \theta_0)]$$

$$h = r_0 v_0 \sin \phi_0 \quad \mu = gR^2$$

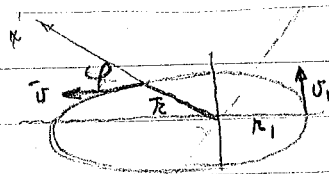
$$E = \frac{v_0^2}{2} - \frac{\mu}{r_0}$$

$$e = \sqrt{1 + \frac{2Eh^2}{\mu^2}} = \sqrt{1 + \frac{2 \left( \frac{v_0^2}{2} - \frac{\mu}{r_0} \right) r_0^2 v_0^2 \sin^2 \phi_0}{(1.408 \times 10^{16})^2}}$$

$$\text{at } \theta = 0 \quad u_0 = \frac{\mu}{h^2} (1 + e \cos \theta_0)$$

$$\cos \theta_0 = \frac{1}{e} \left[ \frac{h^2}{r_0 \mu} - 1 \right]$$

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Given  $\vec{r}(t)$   $\vec{v}(t)$

$$u = \mu/h^2 [1 + \epsilon \cos \theta]$$

$$\begin{aligned} \text{or } u &= C \cos(\theta - \theta_0) + \frac{\mu}{h^2} \\ &= \frac{\mu}{h^2} (1 + \epsilon \cos(\theta - \theta_0)) \end{aligned}$$

$$h = r^2 \dot{\theta} = r v_{\theta} = |\vec{r}| |\vec{v}| \sin \phi$$

apical angle lies between 2 pts where  $\frac{du}{d\theta} = 0$ .

$$h = r(t) v(t) \sin \phi = r_1 v_1$$

$$\epsilon = \sqrt{1 + \frac{2 E h^2}{\mu^2}}$$

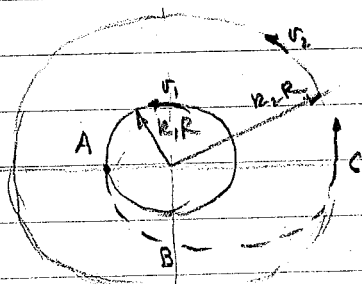
$$E = \frac{v(t)^2}{2} - \frac{\mu}{r(t)}$$

$$\vec{F} = -\frac{\partial V}{\partial \vec{r}}$$

$$\text{at } t=0 \quad \frac{1}{r(t)} = \frac{\mu}{h^2} [1 + \epsilon \cos(-\theta_0)]$$

after  $\theta_0$  is obtained

$$u = \frac{\mu}{h^2} [1 + \epsilon \cos(\theta - \theta_0)]$$



Instantaneous veloc. changes  $K_1 R \rightarrow K_2 R$

$$v_1 c + \Delta V = v_2$$

$$v^2 = \mu \left[ \frac{2}{r} - \frac{1}{a} \right]$$

$$v_1^2 = gR^2 \left[ \frac{2}{k_1 R} - \frac{1}{k_1 R} \right] = \frac{gR}{k_1} \quad (1)$$

$$v_A^2 = gR^2 \left[ \frac{2}{R/R} - \frac{2}{(k_1 + k_2)R} \right] = 2gR \left[ \frac{k_2}{k_1(k_1 + k_2)} \right] \quad (2)$$

$$v_c^2 = 2gR \left[ \frac{k_1}{k_2(k_1 + k_2)} \right] \quad (3)$$

$$v_2^2 = \frac{gR}{k_2} \quad (4)$$

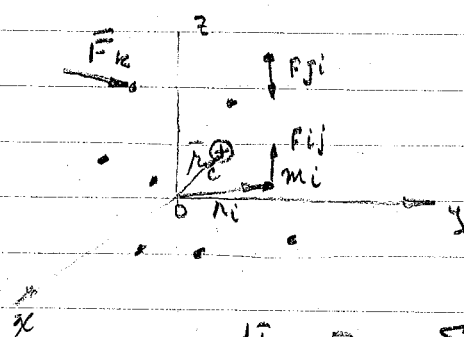
$$\Delta V_A = V_A - V_1 = \sqrt{2gR \left[ \frac{k_2}{k_1(k_1+k_2)} \right]} - \sqrt{\frac{gR}{k_1}}$$

$$\Delta V_C = V_2 - V_C = \sqrt{\frac{gR}{k_2}} - \sqrt{2gR \left[ \frac{k_1}{k_2(k_1+k_2)} \right]}$$

$$\text{total Energy} = \frac{1}{2} m (v_A^2 - v_1^2) + \frac{1}{2} m (v_2^2 - v_C^2)$$

$$= \frac{m g R}{2} \left[ \frac{k_2 - k_1}{k_1 k_2} \right]$$

### System of Particles



### Linear Momentum

#### Theorem

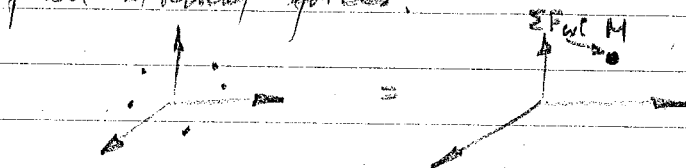
$$M \bar{v}_C = \sum_i m_i \bar{v}_i ; M = \sum_i m_i$$

$$\text{Define } \bar{r}_C = \frac{\sum_i m_i \bar{r}_i}{\sum_i m_i}$$

$$\frac{d\bar{r}_C}{dt} = \bar{v}_C = \frac{\sum_i m_i \bar{v}_i}{M}$$

$$\sum_i m_i \bar{v}_i = M \bar{v}_C \quad \text{QED}$$

The center of mass of system of particles moves as if it were a single particle of mass  $M$  acted upon by the resultant of all external forces.



Theorem:

$$\bar{F}_i = m_i \frac{d}{dt} \bar{v}_i$$

$$\vec{F}_i^{(e)} + \sum_j \vec{F}_{ij} = m_i \frac{d}{dt} \vec{v}_i \quad \text{for } i^{\text{th}} \text{ particle}$$

the total sum: 
$$\sum_i \vec{F}_i^{(e)} + \sum_i \sum_j \vec{F}_{ij} = \sum_i m_i \frac{d}{dt} \vec{v}_i$$

according to Newton's third law  $F_{ji} = -F_{ij} \Rightarrow \sum_i \sum_j \vec{F}_{ij} = 0$   
the forces do not have to be colinear.

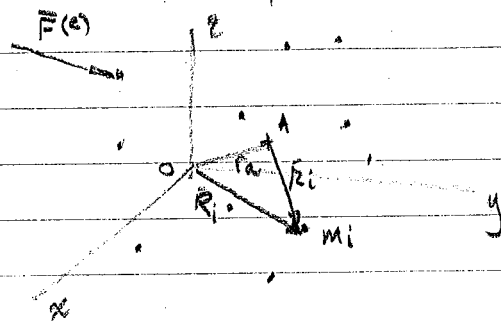
$$\sum_i \vec{F}_i^{(e)} = \sum_i m_i \frac{d}{dt} \vec{v}_i = M \frac{d}{dt} \vec{v}_c$$

If  $\sum_i \vec{F}_i^{(e)} = 0$  then  $M \frac{d}{dt} \vec{v}_c = \frac{d}{dt} (M \vec{v}_c) = 0$

$\therefore M \vec{v}_c$  is a constant and is the principle of Constant Linear Momentum.

### Angular Momentum: total

The time rate of change of angular momentum of a system of particles about a pt a is equal to the total external moment about pt A if a is a fixed pt or if a is the center of mass.



$$\vec{h}_A = \sum_i \vec{r}_i \times m_i \vec{v}_i$$

where  $\vec{v}_i = \frac{d\vec{r}_i}{dt} = \frac{d(\vec{r}_a + \vec{r}_i)}{dt}$

$$\frac{d\vec{h}_A}{dt} = \sum_i \vec{r}_i \times m_i (\vec{\dot{r}}_a + \vec{\dot{r}}_i) + \sum_i \vec{r}_i \times m_i \frac{d\vec{v}_i}{dt}$$

$$= \sum_i \vec{r}_i \times m_i \vec{\dot{r}}_a + \sum_i \vec{r}_i \times \vec{F}_i$$

if pt A is fixed  $\vec{\dot{r}}_a = 0 \therefore \frac{d\vec{h}_A}{dt} = \sum_i \vec{r}_i \times \vec{F}_i$

if pt A is at center of mass  $\sum_i m_i \vec{r}_i \times \vec{\dot{r}}_a = 0$



$$\bar{r}_c = \frac{\sum m_i \bar{r}_i}{\sum m_i} = 0$$

$$\sum m_i \bar{r}_i = 0 \rightarrow \sum m_i \frac{d\bar{r}_i}{dt} = 0$$

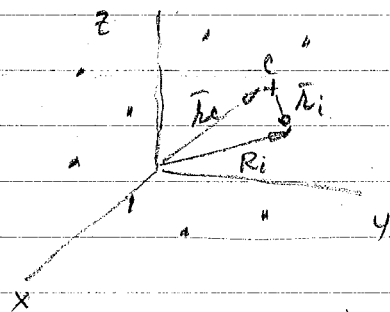
$$\therefore (m_1 \bar{r}_1 + \dots + m_i \bar{r}_i + \dots) \times \bar{r}_c = 0$$

$$\therefore \bar{h}_A = \sum \bar{G}_i$$

$$\text{if forces are colinear } \sum \bar{G}_i^{(e)} + \sum \bar{G}_i^{(int)} = \sum \bar{G}_i$$

$$\text{and } \sum \bar{G}_i^{(int)} = 0 \quad \therefore \sum \bar{G}_i^{(e)} = \sum \bar{G}_i = \bar{h}_A$$

Theorem: The total angular momentum of a system of particles about the mass center may be calculated from the absolute velocities or the velocities relative to mass center.



$$\bar{h}_c = \sum \bar{r}_i \times m_i \bar{v}_i = \sum \bar{r}_i \times m_i (\bar{v}_c + \bar{v}_i')$$

$$\text{if pt is a center of mass } \sum \bar{r}_i \times m_i \bar{v}_c = 0$$

$$\therefore \bar{h}_c = \sum \bar{r}_i \times m_i \bar{v}_i'$$

$$\text{find: } \bar{h}_c = \sum \bar{r}_i \times m_i \bar{v}_i' + \sum \bar{r}_i \times m_i \frac{d\bar{v}_c}{dt} = \sum \bar{r}_i \times \bar{F}_i$$

$$\text{since } \bar{r}_i \times \bar{v}_i' = 0; \text{ since } \bar{r}_i = \bar{R}_i - \bar{r}_c \text{ then}$$

$$\sum \bar{r}_i \times \bar{F}_i = \sum \bar{r}_i \times m_i [\bar{R}_i - \bar{r}_c] = \sum \bar{r}_i \times m_i \bar{R}_i$$

$$\text{but } \bar{F}_i = m_i \bar{R}_i \text{ then } \sum \bar{r}_i \times \bar{F}_i$$

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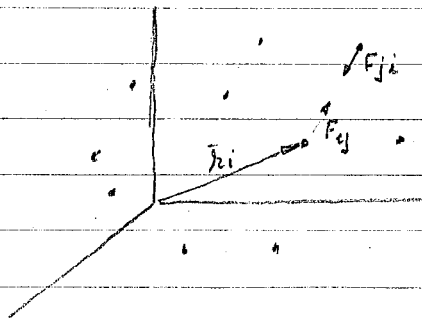
## Work & Energy Principle

$$\vec{F}_i = m_i \frac{d^2 \vec{r}_i}{dt^2}$$

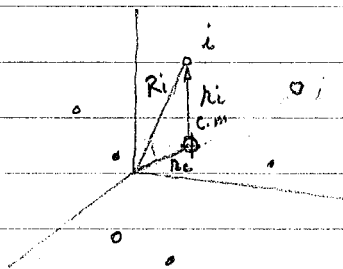
$$\begin{aligned} dW &= \vec{F}_i \cdot d\vec{r}_i \\ &= \sum m_i \frac{d\vec{v}_i}{dt} \cdot \vec{v}_i dt \\ &= d \sum \frac{m_i}{2} \vec{v}_i \cdot \vec{v}_i = d \sum \frac{m_i}{2} v_i^2 \end{aligned}$$

$$dW = dT$$

Exception: you cannot exclude the internal forces which produce work



## Kinetic Energy



$$\begin{aligned} T &= \sum_i \frac{1}{2} m_i \vec{v}_i \cdot \vec{v}_i \\ &= \sum_i \frac{1}{2} m_i (\vec{v}_c + \vec{v}_i') \cdot (\vec{v}_c + \vec{v}_i') \\ &= \sum_i \frac{1}{2} m_i \vec{v}_c^2 + \sum_i m_i \vec{v}_i' \cdot \vec{v}_c + \sum_i \frac{1}{2} m_i \vec{v}_i'^2 \end{aligned}$$

$$T = \frac{1}{2} M v_c^2 + \sum_i \frac{1}{2} m_i v_i'^2 \quad v_i' - \text{relative velocity.}$$

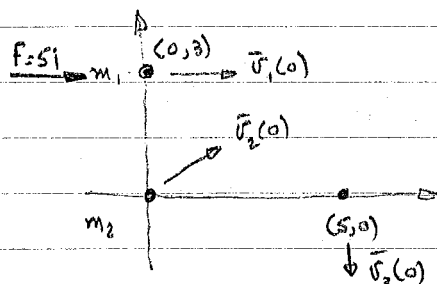
K.E. of C.M.

D'Alembert Forces

$$\sum_i \vec{F}_i(t) = M \frac{d\vec{v}_c}{dt}$$

$$\sum_i \vec{F}_i(t) - M \frac{d\vec{v}_c}{dt} = 0$$

Example



$$\begin{aligned} \text{at } t=0 \quad \vec{r}_1 &= 3\vec{j} & \vec{v}_1 &= 10\vec{i} \\ \vec{r}_2 &= 0 & \vec{v}_2 &= 5\vec{i} + 5\vec{j} \\ \vec{r}_3 &= 5\vec{i} & \vec{v}_3 &= -10\vec{j} \end{aligned}$$

$$\begin{aligned} m_1 &= 1 \\ m_2 &= 3 \\ m_3 &= 6 \end{aligned}$$

$$\text{at } t=0 \quad \text{what is } \vec{r}_c = \frac{\sum m_i \vec{r}_i}{\sum m_i} = \frac{3\vec{j} + 6(5\vec{i})}{10} = .3\vec{j} + 3\vec{i}$$

$$\text{at } t=0 \quad \vec{p} = \sum m_i \vec{v}_i = 10\vec{i} + 15\vec{i} + 15\vec{j} - 60\vec{j} = 25\vec{i} - 45\vec{j}$$

$$\text{at } t=0 \quad \vec{v}_c = \frac{\vec{p}}{\sum m_i} = 2.5\vec{i} - 4.5\vec{j}$$

$$\begin{aligned} \vec{h}_c(0) &= \sum \vec{r}_i \times m_i \vec{v}_i = 3\vec{j} \times (10\vec{i}) + 0 + 5\vec{i} \times (-60\vec{j}) \\ &= -30\vec{k} - 300\vec{k} = -330\vec{k} \end{aligned}$$

$$\sum_i \vec{F}_i(t) = M \frac{d\vec{v}_c}{dt} = 5\vec{i} = M [\ddot{x}_c \vec{i} + \ddot{y}_c \vec{j}]$$

$$5 = M \ddot{x}_c \quad 0 = M \ddot{y}_c$$

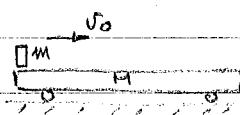
$$\boxed{\frac{5t}{M} = x_c - 2.5}$$

$$\boxed{\dot{y}_c = -4.5}$$

$$\boxed{x_c = \frac{5t^2}{2M} - 2.5t + 3}$$

$$\boxed{y_c = -4.5t + .3}$$

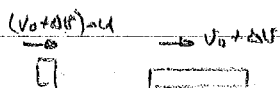
Example



$$\sum \vec{F}_i = M \frac{d\vec{v}_c}{dt} = 0 \rightarrow M\vec{v}_c = \text{constant.}$$

initial momentum = final momentum.

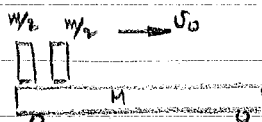
$$(M+m)v_0 = M(v_0 + \Delta v) + m(v_0 + \Delta v - u)$$



$u$  is relative of man

$$0 = \Delta v (M+m) - mu$$

$$\Delta v = \frac{m}{M+m} u$$



1 jumps off first relative speed  $u$

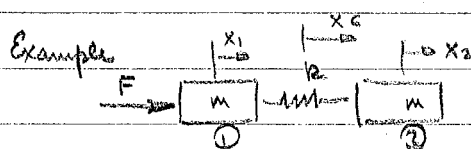
$$(M+m)v_0 = (M+m/2)(v_0 + \Delta v) + m/2(v_0 + \Delta v - u)$$

$$0 = \Delta v (M+m) - m/2 u \quad \Delta v_1 = \frac{m}{2(M+m)} u$$

$$(M+m/2)(v_0 + \Delta v_1) = M(v_0 + \Delta v_1 + \Delta v_2) + m/2(v_0 + \Delta v_1 + \Delta v_2 - u)$$

$$0 = M\Delta v_2 + m/2\Delta v_2 - u m/2 \quad \Delta v_2 = \frac{u m}{2(M+m/2)}$$

$$\Delta v_T = \Delta v_1 + \Delta v_2$$



$$m_1 = m_2 = m$$

$$x(0) = 0 \quad \dot{x}(0) = 0$$

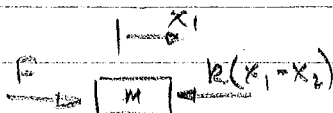
$$x_1 = x_1(t)$$

$$x_2 = x_2(t)$$

$$\frac{x_1 + x_2}{2} = x_c$$

$$F = 2m \frac{dv_c}{dt} \quad \left| v_c = \frac{F}{2m} t \right|$$

$$\left| x_c = \frac{F}{4m} t^2 \right|$$



$$F - k(x_1 - x_c) = m\ddot{x}_1$$

$$F - k(x_1 - 2x_c + x_1) = m\ddot{x}_1$$

$$F - 2k(x_1 - x_c) = m\ddot{x}_1$$

$$F/2 = m\ddot{x}_c$$

$$F/2 - 2k(x_1 - x_c) = m(\ddot{x}_1 - \ddot{x}_c)$$

$$(\ddot{x}_1 - \ddot{x}_c) + \frac{2k}{m}(x_1 - x_c) = \frac{F}{2m}$$

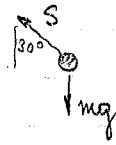
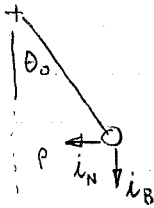
$$(x_1 - x_c) = A \sin \sqrt{\frac{2k}{m}} t + B \cos \sqrt{\frac{2k}{m}} t + \frac{F}{4k}$$

$$x_1 = \frac{Ft^2}{4m} + \frac{F}{4k} \left( 1 - \cos \sqrt{\frac{2k}{m}} t \right)$$

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# Test Review

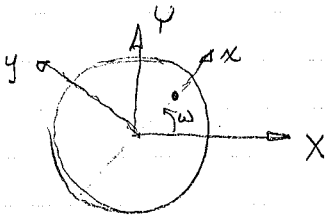
1.



$$\begin{aligned} S \cos \theta_0 &= mg \\ S \sin \theta_0 &= \frac{mv^2}{\rho} \end{aligned}$$

$$v \approx 6.1 \text{ ft/sec}$$

2.



$$\bar{a}_{abs} = \frac{d^2 \bar{R}_0}{dt^2} + \frac{\delta^2 \bar{r}}{\delta t^2} + \frac{\delta \bar{\omega}}{\delta t} \times \bar{r} + 2\bar{\omega} \times \frac{\delta \bar{r}}{\delta t} + \bar{\omega} \times (\bar{\omega} \times \bar{r})$$

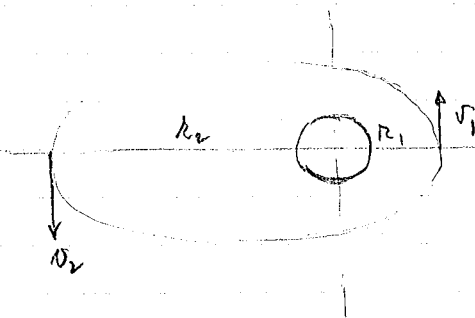
$$\bar{r} = x\bar{i}$$

$$\frac{\delta \bar{r}}{\delta t} = v\bar{i}$$

$$\bar{\omega} = \omega\bar{k}$$

$$\bar{a}_{abs} = 2\omega\bar{k} \times v\bar{i} + (\omega\bar{k}) \times (\omega\bar{k} \times x\bar{i})$$

3.



$$r_1 v_1 = r_2 v_2$$

## Impulsive Forces.

Particle

$$\bar{F} = \frac{d}{dt}(m\bar{v})$$

$$\int_{t_0}^{t_1} \bar{F} dt = \int_{t_0}^{t_1} \frac{d}{dt}(m\bar{v}) dt = d(m\bar{v})$$

$$(m\bar{v})_i + \int_{t_0}^{t_1} \bar{F} dt = (m\bar{v})_f$$

Impulse

$$\bar{G} = \frac{d}{dt} \bar{h}$$

when

$$\bar{h} = \bar{r} \times m\bar{v}$$

$$\int_{t_0}^{t_1} \bar{G} dt = d\bar{h} \rightarrow$$

$$\bar{h}_i + \int_{t_0}^{t_1} \bar{G} dt = \bar{h}_f$$

angular impulse.

## Collision

$$\lim_{t_1 \rightarrow t_0} \int_{t_0}^{t_1} \bar{F} dt = \hat{F} \text{ impulsive force}$$

∴ we get  $\hat{F} = \Delta m \bar{v}$

$$(m\bar{v})_{\text{int}} + \hat{F} = (m\bar{v})_{\text{final}}$$

$$\lim_{t_1 \rightarrow t_0} \int_{t_0}^{t_1} \hat{G} dt = \hat{G} - \text{impulsive moment} = \lim_{t_1 \rightarrow t_0} \int (\bar{r} \times \bar{F}) dt \quad \text{if } \bar{r} \text{ is a constant}$$

$$\hat{G} = \bar{r} \times \lim_{t_1 \rightarrow t_0} \int_{t_0}^{t_1} \bar{F} dt = \bar{r} \times \hat{F}$$

$$\hat{G} = \bar{r} \times \hat{F}$$

$$\bar{h}_{\text{init}} + \hat{G} = \bar{h}_f$$

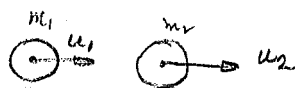
Summary

$$\hat{F} = \Delta m \bar{v}; \quad \hat{G} = \Delta \bar{h}$$

$$\hat{F} = \Delta m \bar{v}_c; \quad \hat{G} = \Delta \bar{h}_c$$

particle  
system.

### Collision of two particles



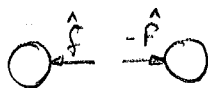
line of motion.

$u_1, u_2$  are speeds before collision

$u'_1, u'_2$  after collision

$$(m\bar{v})_i + \hat{F} = (m\bar{v})_f$$

consider whole system.



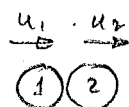
$$m_1 u_1 + m_2 u_2 + 0 = m_1 u'_1 + m_2 u'_2 \quad (1)$$

$$m_1 u_1 + \hat{F} = m_1 u'_1$$

coefficient of restitution  $\epsilon = \frac{v_{\text{separat}}}{v_{\text{approach}}} = \frac{u'_2 - u'_1}{u_1 - u_2}$

giving

$$(2)$$



$u'_1, u'_2$

$$m_1 u_1 + m_2 u_2 = m_1 u'_1 + m_2 u'_2 \quad (1)$$

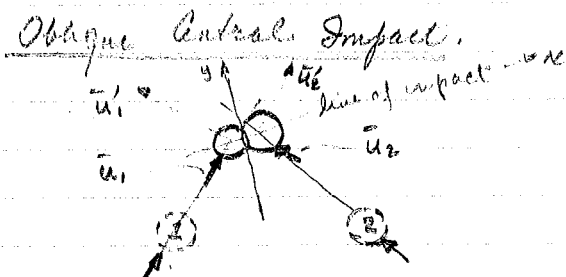
$$\epsilon = \frac{u'_1 - u'_2}{u_2 - u_1} \quad (2)$$

$$u'_1 = \frac{[(m_1 - m_2\epsilon)u_1 + m_2(1+\epsilon)u_2]}{m_1 + m_2}$$

$$u'_2 = \frac{[m_1(1+\epsilon)u_1 + (m_2 - m_1\epsilon)u_2]}{(m_1 + m_2)}$$

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if  $\epsilon = 0$   $u_2' = u_1'$  (plastic collision)if  $\epsilon = 1$  also  $m_1 = m_2$   $u_1 = u_2'$   
 $u_2 = u_1'$  (elastic collision)known  $\bar{u}_1, \bar{u}_2$  line of impact  
find  $\bar{u}_1', \bar{u}_2'$ 

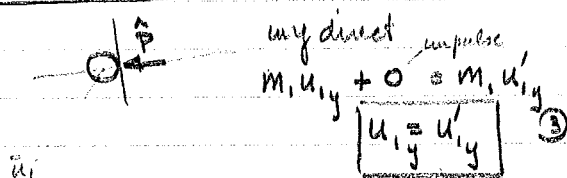
Consider Entire System.

$$m_1 \bar{u}_1 + m_2 \bar{u}_2 = m_1 \bar{u}_1' + m_2 \bar{u}_2' \quad (1)$$

$$m_1 u_{1x} + m_2 u_{2x} = m_1 u_{1x}' + m_2 u_{2x}' \quad (2)$$

$$m_1 u_{1y} + m_2 u_{2y} = m_1 u_{1y}' + m_2 u_{2y}' \quad (3) \quad \text{not indep. of 2 \& 4}$$

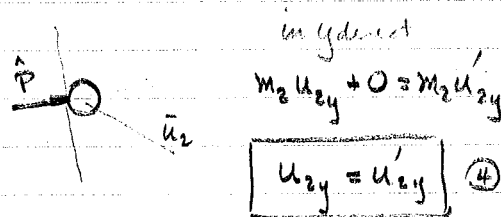
Particle 1 alone.



in x direct.

$$m_1 u_{1x} - \hat{P} = m_1 u_{1x}' \quad (6)$$

Particle 2 alone



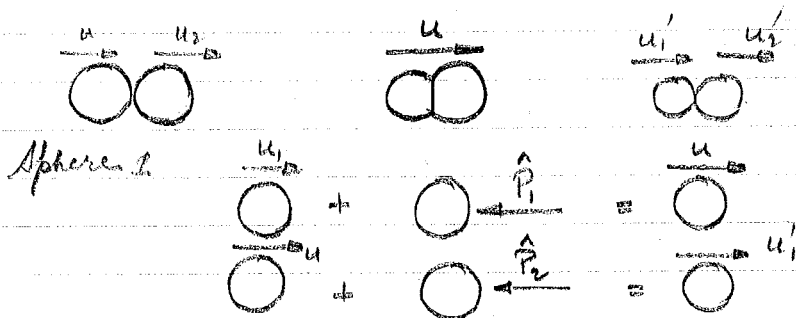
$$m_2 u_{2x} + \hat{P} = m_2 u_{2x}' \quad (7)$$

$$\epsilon = \frac{(u_2')_x - (u_1')_x}{(u_1)_x - (u_2)_x} \quad (5)$$

adding 6 &amp; 7 gives eqn. 1.

Coefficient of Restitution may be defined also as

$$\epsilon = \frac{\hat{P}_2}{\hat{P}_1} \quad \begin{array}{l} \text{impulsive force of restitution} \\ \text{" " " compression} \end{array}$$



$$m_1 u_1 - \hat{P}_1 = m_1 u_1'$$

$$m_1 u_1 - \hat{P}_2 = m_1 u_1'$$

Sphere 2

$$\begin{array}{c} \frac{u_2}{\text{---}} \\ \text{---} \end{array} + \frac{\hat{P}_1}{\text{---}} = \frac{u}{\text{---}}$$

$$\begin{array}{c} \text{---} \\ \text{---} \end{array} + \frac{\hat{P}_2}{\text{---}} = \frac{u_2'}{\text{---}}$$

$$m_1 u_2 + \hat{P}_1 = m_2 u$$

$$m_2 u + \hat{P}_2 = m_2 u_2'$$

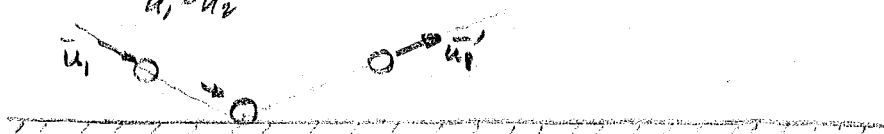
Consider

$$e = \frac{\hat{P}_2}{\hat{P}_1} = \frac{u - u_1'}{u_1 - u}$$

$$e = \frac{\hat{P}_2}{\hat{P}_1} = \frac{u_1' - u}{u - u_2}$$

$$\frac{u - u_1'}{u_1 - u} = \frac{u_2' - u}{u - u_2} \rightarrow \text{find } u \text{ and put into } e$$

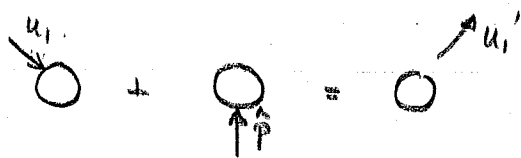
$$e = \frac{u_1' - u_1}{u_1 - u_2}$$



$$m_1 \bar{u}_1 = m_1 \bar{u}_1'$$

$$m_1 \bar{u}_{1x} = m_1 \bar{u}_{1x}'$$

$$m_1 \bar{u}_{1x} = m_1 \bar{u}_{1x}'$$



$$m_1 u_{1x} = m_1 u_{1x}'$$

$$e = \frac{(u_1')_y - (u_2')_y}{(u_2)_y - (u_1)_y} = \frac{(u_1')_y - 0}{0 - (u_1)_y}$$

$$-e(u_1)_y = (u_1')_y$$



①

②

$$\bar{u}_1 = 10 \text{ ft/sec}$$

$$\bar{u}_2 = -20 \text{ ft/sec}$$

$$m_1 = 1 \text{ unit} \quad m_2 = 10 \text{ units}$$

$$m_1 \bar{u}_1 + m_2 \bar{u}_2 = m_1 \bar{u}_1' + m_2 \bar{u}_2'$$

$$1 \cdot 10 + 10(-20) = 1 \cdot \bar{u}_1' + 10 \bar{u}_2'$$

$$-190 = \bar{u}_1' + 10 \bar{u}_2' \rightarrow \text{①}$$

$$e = \frac{u_2' - u_1'}{u_1 - u_2}$$

$$\text{let } e = .5$$

$$.5 = \frac{u_2' - u_1'}{30}$$

$$u_2' - u_1' = 15$$

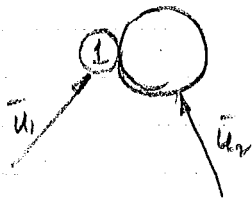
$$u_1' + 10(15 + u_1') = -190$$

$$11u_1' = -340$$

$$u_1' = \frac{-340}{11} = -30.9$$

$$u_2' = 15 + u_1' = 15 - 30.9 = -15.9$$





H.W.

$$e = 0.5 \quad m_1 = 1 \quad m_2 = 10$$

$$\vec{u}_1 = 10\hat{i} + 10\hat{j} \quad \vec{u}_2 = -20\hat{i} + 15\hat{j}$$

find  $\vec{u}_1'$  &  $\vec{u}_2'$

$$T - T' = (1 - e^2) \frac{1}{2} [m_1 u_1^2 + m_2 u_2^2]$$

$$u_1 = v_c + v_1$$

$$u_1' = v_c + v_1'$$

$v_c$  = center of mass

$v_i$  speeds relative to center of mass

$$u_2 = v_c + v_2$$

$$u_2' = v_c + v_2'$$

$$T = \frac{1}{2} m_1 (v_c + v_1)^2 + \frac{1}{2} m_2 (v_c + v_2)^2$$

$$T' = \frac{1}{2} m_1 (v_c + v_1')^2 + \frac{1}{2} m_2 (v_c + v_2')^2$$

H.W. Problem 7.13

before impact

$$m_1 (v_c + v_1) + m_2 (v_c + v_2) = (m_1 + m_2) v_c$$

after impact

$$m_1 (v_c + v_1') + m_2 (v_c + v_2') = (m_1 + m_2) v_c$$

and  $e =$

$$e = \frac{u_2' - u_1'}{u_1 - u_2} = \frac{v_c + v_2' - v_c - v_1'}{v_c + v_1 - v_c - v_2} = \frac{v_2' - v_1'}{v_1 - v_2}$$

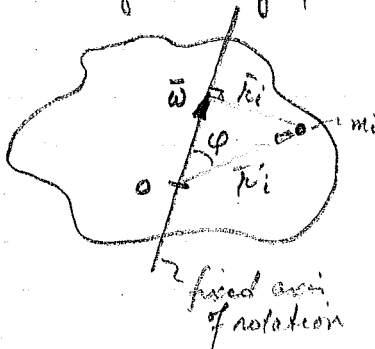
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### Rigid Bodies

Collections of particles whose relative position of particles remains unchanged.  $\epsilon h!$

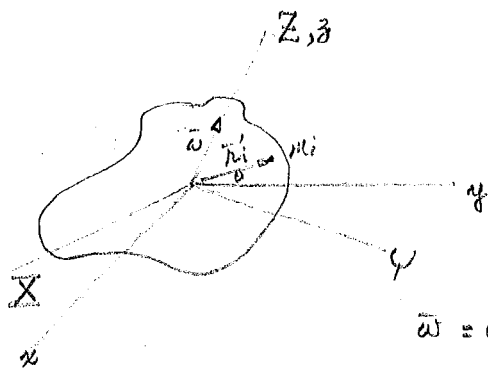
### Plane Motion of Rigid Bodies

Rigid Body rotating about a fixed axis.



$$\vec{v}_i = \vec{\omega} \times \vec{r}_i'$$

$$|\vec{v}_i| = \omega r_i \sin \phi = \omega r_i$$



Rotation with  $z$  fixed  
 $\vec{r}_i' = r \cos \theta \vec{j} + r \sin \theta \vec{k}$

$$\vec{v}_i = \frac{d\vec{r}_i'}{dt} + \vec{\omega} \times \vec{r}_i' = \vec{\omega} \times \vec{r}_i'$$

$$\vec{\omega} = \omega \vec{k} \quad \omega \times \vec{r}_i' = -i\omega r \cos \theta$$

Kinetic Energy

$$T = \sum_i \frac{1}{2} m_i v_i^2 = \sum_i \frac{1}{2} m_i \omega^2 r_i^2 = \boxed{\frac{1}{2} I \omega^2} \quad \text{since } \sum m_i r_i^2 = I$$

Angular Momentum

$$\vec{L}_0 = \sum_i \vec{r}_i \times m_i \vec{v}_i$$

$$|\vec{L}_0| = \sum_i m_i \vec{r}_i' \times \vec{v}_i = \sum_i m_i r_i' \omega r_i' \sin \varphi$$

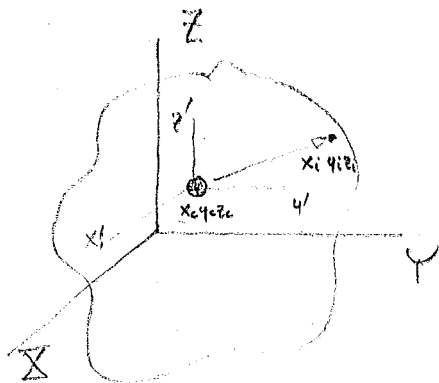
$$L_0 \text{ along } \omega \text{ axis} = \left\{ \sum_i m_i r_i'^2 \omega \sin \varphi \right\} \sin \varphi = \sum_i \omega [m_i] (r_i' \sin \varphi)^2$$

$$(L_0)_\omega = I \omega$$

If rigid body rotates and translates.

$$T = \frac{1}{2} M v_c^2 + \frac{1}{2} I \omega^2$$

Translation rotation.  $I$  is through center of mass



$$x_i = x_c + x_i'$$

$$y_i = y_c + y_i'$$

$$z_i = z_c + z_i'$$

$$T = \sum_i \frac{1}{2} m_i v_i^2$$

$$= \sum_i \frac{1}{2} m_i [\dot{x}_i^2 + \dot{y}_i^2 + \dot{z}_i^2]$$

$$= \sum_i \frac{1}{2} m_i [(\dot{x}_c + \dot{x}_i')^2 + (\dot{y}_c + \dot{y}_i')^2 + (\dot{z}_c + \dot{z}_i')^2]$$

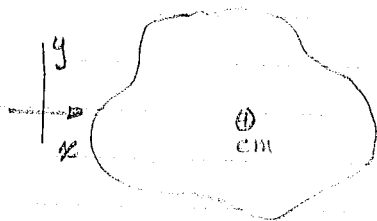
$$\text{since } \sum m_i x_c \dot{x}_i' = \sum m_i y_c \dot{y}_i' = \sum m_i z_c \dot{z}_i' = 0$$

$$\sum \frac{1}{2} m_i (\dot{x}_i'^2 + \dot{y}_i'^2 + \dot{z}_i'^2) = \sum \frac{1}{2} m_i \dot{r}_i'^2 = \frac{1}{2} M v_c^2 + \frac{1}{2} I \omega^2$$

$$\text{but } v_i' = \omega r_i'$$

$$\text{also } \sum \frac{1}{2} m_i (\dot{x}_i'^2 + \dot{y}_i'^2 + \dot{z}_i'^2) = \frac{1}{2} I \omega^2$$

# Eqs of Motion for Rigid Body Plane Motion



$$\begin{aligned} \vec{F} &= M \ddot{\vec{r}}_c \\ F_x &= M \ddot{x}_c \\ F_y &= M \ddot{y}_c \end{aligned}$$

with respect to fixed system.

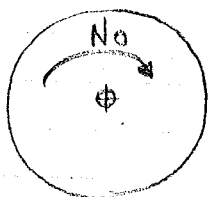
$$\sum \vec{r}_i \times \vec{F}_i = \frac{d\vec{h}}{dt}$$

$\vec{r}_i \times \vec{F}_i \rightarrow N$

$$N = I_{f, cm} \dot{\omega}$$

$I$  is about a fixed pt or the center of mass.

Example:



$$N = N_0 = \text{constant.}$$

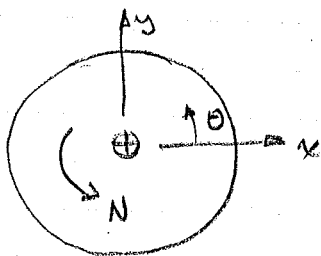
$$N = I_0 \dot{\omega}$$

$$\omega = \frac{N}{I_0} t + C_1 \quad \text{at } t=0 \quad \omega = \omega_0$$

$$\theta = \frac{N}{2I_0} t^2 + \omega_0 t + C_2 \quad \text{at } t=0 \quad \theta = \theta_0$$

$$\theta = \frac{N}{2I_0} t^2 + \omega_0 t + \theta_0$$

Example:



$$\omega = \omega(t) \quad [\dot{\theta}(t) = ?]$$

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$$N = N_0 + N_1 \cos ct - L \dot{\omega}$$

$$N = I_0 \ddot{\theta} = I_0 \dot{\omega}$$

$$I_0 = m k_0^2 \quad m k_0^2 \dot{\omega} = N_0 + N_1 \cos ct - L \dot{\omega}$$

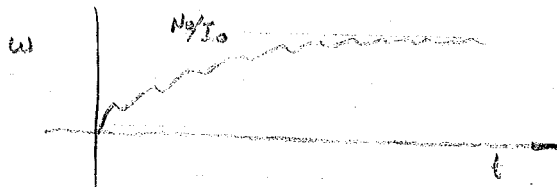
$$\dot{\omega} = \frac{N_0}{I_0} + \frac{N_1}{I_0} \cos ct - \frac{L}{I_0} \dot{\omega}$$

$$\dot{\omega} + \frac{L}{I_0} \dot{\omega} = \frac{N_0 + N_1 \cos ct}{I_0}$$

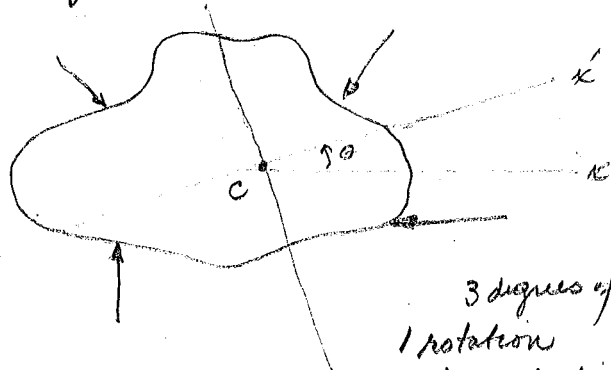
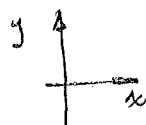
homogeneous sol.

particular solution

$$\omega = A e^{-\frac{L}{I_0} t} + \frac{N_0}{I_0} + \frac{N_1}{I_0 \sqrt{(\frac{L}{I_0})^2 + c^2}} \cos(ct + \epsilon)$$



# Equations of Motion - Rigid Body in Plane Motion



3 degrees of freedom.  
1 rotation  
2 translation.

$$\Sigma X = \Sigma F_x = m \ddot{x}_c \quad (1)$$

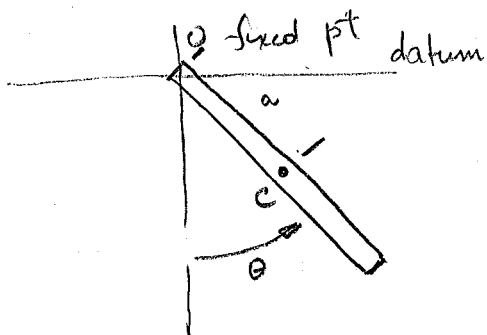
$$\Sigma Y = \Sigma F_y = m \ddot{y}_c \quad (2)$$

$$\Sigma M = I_c \ddot{\theta} \quad (3)$$

If conservative forcefield  
 $T + V = E$

$$\frac{1}{2} m v_c^2 + \frac{1}{2} I_c \dot{\theta}^2 + V = E \quad (4)$$

## Compound Pendulum.



$$|\theta - 10| \leq 0$$

$$T + V = E$$

$$\frac{1}{2} I_o \dot{\theta}^2 - m g a \cos \theta = E$$

$$\frac{1}{2} I_o \cdot 2 \dot{\theta} \ddot{\theta} + m g a \sin \theta \dot{\theta} = 0$$

$$\dot{\theta} (I_o \ddot{\theta} + m g a \sin \theta) = 0$$

$$I_o = m k_o^2$$

$$m k_o^2 \ddot{\theta} + m g a \sin \theta = 0$$

$$k_o^2 \ddot{\theta} + g a \sin \theta = 0 \quad \text{for } 10^\circ \leq \theta \leq 10^\circ \quad \sin \theta \sim \theta$$

$$\ddot{\theta} + \frac{g a / k_o^2}{\omega_1^2} \theta = 0$$

$$\text{for simple pendulum } \ddot{\theta} + \frac{g L}{\omega_2^2} \theta = 0$$

$$L_{\text{eff}} = \frac{k_o^2}{a}$$

$$k_o^2 = k_c^2 + a^2$$

$$\omega_1 = \sqrt{g a / k_o^2} = \sqrt{\frac{g a}{k_c^2 + a^2}} ;$$

$$T = \frac{2\pi}{\omega_2} = \frac{2\pi}{\sqrt{\frac{g a}{k_c^2 + a^2}}}$$

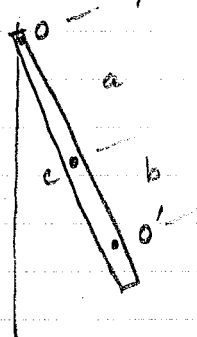
$$\tau^2 = \frac{4\pi^2}{g} \left[ \frac{k_c^2}{a} + a \right] \quad \text{as } a \rightarrow 0 \quad \tau \rightarrow \infty, \\ a \rightarrow \infty \quad \tau \rightarrow \infty,$$

$$\text{find } \frac{d\tau}{da} = 0 \quad 2\tau \frac{d\tau}{da} = c \left[ -\frac{k_c^2}{a^2} + 1 \right] = 0$$

$$k_c = a \quad \therefore \tau \text{ is min at this pt.}$$

$$\therefore \tau_{\min}^2 = \frac{4\pi^2}{g} [2k_c] = \frac{8k_c\pi^2}{g}$$

Is there another pt  $O'$  such that  $\tau_{\min} = \tau_{O'}$   $O'$  is center of oscillation



$$\frac{k_c^2}{a} + a = \frac{k_c^2}{b} + b$$

$$\frac{k_c^2 b}{a} + ab = k_c^2 + b^2$$

$$b^2 - b\left(\frac{k_c^2}{a} + a\right) + k_c^2 = 0$$

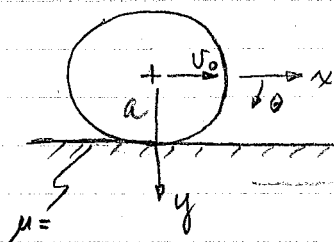
$$\left(b - \frac{k_c^2}{a}\right)(b - a) = 0 \quad b = \frac{k_c^2}{a}$$

$$k_c = \frac{\int x dm}{\int dm}$$

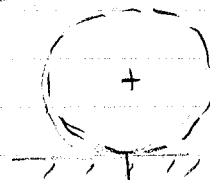
from  $x = x_c$  axis

$$I_c = \int (x - x_c)^2 dm$$

Example:

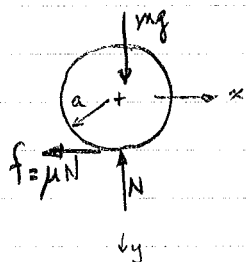


$$v(0) = v_0 \quad x_c(0) = 0 \\ \dot{\theta}(0) = 0 \quad \theta(0) = 0$$



pure roll  $\rightarrow$

roll and slip



$$\begin{aligned} Y &= mg - N = m\ddot{y}_c = 0 & N &= mg & (1) \\ X &= m\ddot{x}_c = -\mu N & & & (2) \\ N &= \mu Na = I_c \ddot{\theta} & & & (3) \end{aligned}$$

integrate two  $-\mu mg = m\ddot{x}_c$

$$\dot{x}_c = -\mu g t + C_1, \quad C_1 = v_0 \quad (4)$$

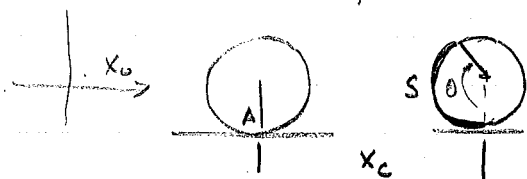
$$x_c = -\mu g \frac{t^2}{2} + v_0 t + C_2 \quad (5)$$

integrate three  $\mu m g a = m k_c^2 \ddot{\theta}$

$$\dot{\theta} = \frac{\mu g a}{k_c^2} t + C_3 \quad (6)$$

$$\theta = \frac{\mu g a}{2 k_c^2} t^2 + C_4 \quad (7)$$

check speed of bottom most pt if equal to 0 pure roll if  $\neq 0$  slip



$$s = r\theta = x_c = a\theta + x_0$$

$$v_c = \dot{x}_c = a\dot{\theta} \quad \text{pure roll.} \quad (8)$$

$$\ddot{x}_c = a\ddot{\theta}$$

To calculate  $x_c^*$ ,  $t^*$ ,  $\dot{x}_c = a\dot{\theta}$

$$\dot{x}_c = -\mu g t^* + v_0 = a \left[ \frac{\mu g a}{k_c^2} t^* \right]$$

$$t^* = \frac{v_0}{\mu g \left[ \frac{a^2}{k_c^2} + 1 \right]} \quad (9) \quad \text{put (9) into (5)}$$

$$x_c^* = -\frac{v_0^2}{2\mu g \left[ \frac{a^2}{k_c^2} + 1 \right]} + \frac{2v_0^2 \left[ \frac{a^2}{k_c^2} + 1 \right]}{2\mu g \left[ \frac{a^2}{k_c^2} + 1 \right]^2} = \frac{v_0^2 (1 + 2\frac{a^2}{k_c^2})}{2\mu g \left[ \frac{a^2}{k_c^2} + 1 \right]^2}$$

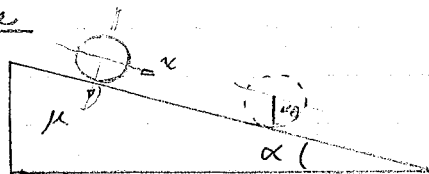
$$\vec{r} = a\vec{j} \quad \vec{\omega} = \dot{\theta}\vec{k} \quad \vec{v}_A = \vec{\omega} \times \vec{r} + \vec{v}_C$$

8.1 abc

4/22/71

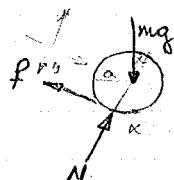
3<sup>rd</sup> quiz - May 6 2 questions  
HW. Problems 8.13, 15a, 17, 19

Example



Ball starts from rest on rough plane.

What is  $\mu_{\min}$  for pure roll of ball - sphere.



$$f \leq \mu N$$

$$-N + mg \cos \alpha = m \ddot{y}_c = 0$$

$$N = mg \cos \alpha \quad (1)$$

$$-f + mg \sin \alpha = m \ddot{x}_c \quad (2)$$

$$T = f a = I_c \ddot{\theta} \quad (3)$$

Kinematic condition pure roll

$$\left. \begin{aligned} x_c &= a \theta \\ \dot{x}_c &= a \dot{\theta} \\ \ddot{x}_c &= a \ddot{\theta} \end{aligned} \right\} (4)$$

$$f = \frac{m k_c^2}{a^2} \ddot{x}_c \quad (5)$$

$$-f + mg \sin \alpha = \frac{f a^2}{k_c^2}$$

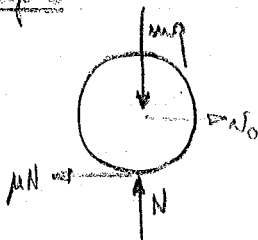
$$f = \frac{mg \sin \alpha}{(1 + a^2/k_c^2)} \leq \mu mg \cos \alpha$$

$$\mu \geq \frac{\tan \alpha}{(1 + a^2/k_c^2)} = \frac{\tan \alpha (k_c^2)}{k_c^2 + a^2}$$

$$\mu_{\min} = \tan \alpha \frac{k_c^2}{k_c^2 + a^2} = \frac{I_c \tan \alpha}{I_0}$$

$$I_0 = m k_c^2 + m a^2$$

Example



$$V + T = \frac{1}{2} m v_c^2 + \frac{1}{2} I_c \dot{\theta}^2 + \text{potential}$$

$$\dot{x}_c = a \dot{\theta}$$

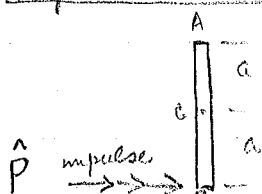
previous example.

Impulse: Momentum  
Angular

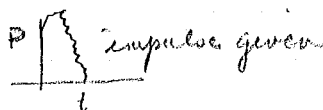
$$\begin{aligned} m v_{c0} - \mu N \Delta t &= m v_c^{\text{sp}} \\ 0 + \mu N a \Delta t &= I_c \dot{\theta}^{\text{sp}} \end{aligned}$$

$$\Delta t = t^*$$

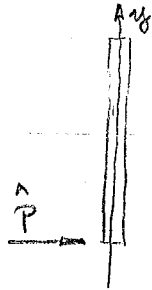
Impulsive forces on Rigid Bodies



$$m, 2a$$



Bar initially at rest, free. Calculate the velocity at A.



$$0 + \hat{P} = m v_c \quad (1)$$

$$0 + \hat{P}a = I_c \omega \quad (2)$$

$$v_{c,x} = \frac{\hat{P}}{m}$$

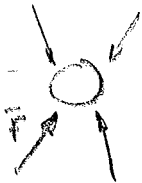
$$\omega = \frac{\hat{P}a}{m k_c^2}$$

$$v_A = v_c - a\omega$$

$$v_A = \frac{\hat{P}}{m} - \frac{\hat{P}a^2}{m k_c^2}$$

Review

4/27/71



$$\sum \vec{F}_i = \vec{F}$$

$$\vec{F} = \frac{d}{dt}(m\vec{v})$$

$$\int_0^t \vec{F} dt = \int_{m\vec{v}_1}^{m\vec{v}_2} d(m\vec{v})$$

$$\text{linear impulse} = \Delta(m\vec{v})$$

$$m\vec{v}_1 + \int_0^t \vec{F} dt = (m\vec{v})_2$$

$$\vec{h}_1 + \int_0^t \vec{N} dt = \vec{h}_2 \quad \text{— angular momentum} \quad \vec{N} = \frac{d\vec{h}}{dt}$$

$$\text{Impulsive Force} - \hat{F} = \lim_{\Delta t \rightarrow 0} \int_0^{\Delta t} \vec{F} dt$$

$$\text{Impulsive Moment} - \hat{N} = \lim_{\Delta t \rightarrow 0} \int_0^{\Delta t} \vec{N} dt = \lim_{\Delta t \rightarrow 0} \int_0^{\Delta t} \vec{r} \times \vec{F} dt$$

$$= \vec{r} \times \lim_{\Delta t \rightarrow 0} \int_0^{\Delta t} \vec{F} dt = \vec{r} \times \hat{F}$$

$\vec{r}$  doesn't change instantly, however  $\vec{v}$  does.

Particle

$$(m\vec{v})_1 + \hat{F} = (m\vec{v})_2$$

$$\vec{h}_1 + \hat{N} = \vec{h}_2$$

System of Particles

$$(m\vec{v}_c)_1 + \hat{F} = (m\vec{v}_c)_2$$

$$\vec{h}_1 + \hat{N} = \vec{h}_2$$

about cm or fixed pt.

$$\text{Rigid Body (Plane Motion)}$$

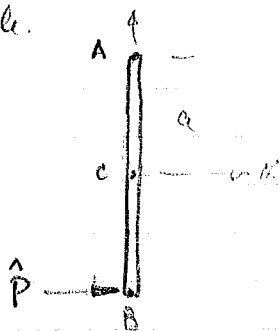
$$(m\vec{v}_c)_1 + \hat{F} = (m\vec{v}_c)_2$$

relative point of part in rigid bodies remain unchanged

$$(I\omega)_1 + \hat{N} = (I\omega)_2$$



Example.



$\hat{P}$  given. Initially at rest.  
 $v_A = ?$

$$v_{Ax} = v_{Cx} - a\omega$$

$$(m\vec{v})_1 + \hat{F} = (m\vec{v})_2$$

$$0 + |\hat{P}| = m v_C$$

$$v_C = \frac{|\hat{P}|}{m} \quad (1)$$

$$\vec{h}_1 + \hat{N} = \vec{h}_2$$

$$0 + a|\hat{P}| = I_C \omega$$

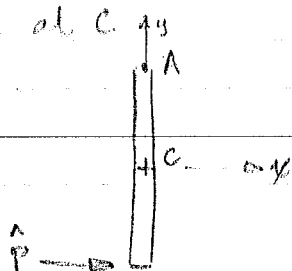
$$\omega = \frac{a|\hat{P}|}{I_C}$$

$$\omega = \frac{3|\hat{P}|}{ma} \quad (2)$$

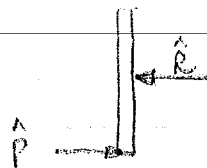
$$v_A = \frac{|\hat{P}|}{m} [1 - 3] = -\frac{2|\hat{P}|}{m}$$

$$I_C = \frac{ma^2}{3}$$

pt fixed at C



no translation



$$\sum m\vec{v}_i \quad 0 + |\hat{P}| - |\hat{R}| = (m\vec{v}_C)_2 = 0$$

$$|\hat{P}| = |\hat{R}| \quad (1)$$

$$\sum \vec{h}_i \quad 0 + |\hat{P}|a = I_C \omega$$

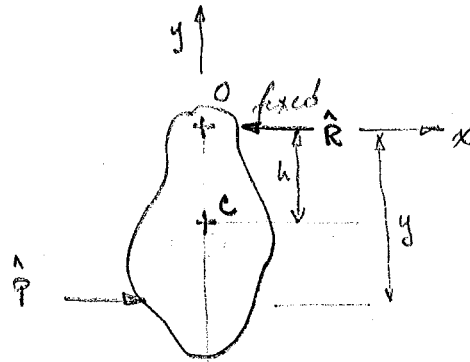
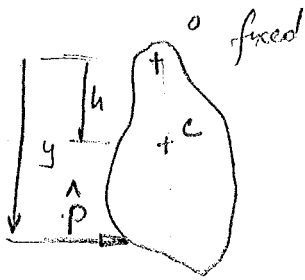
$$\hat{P}a = \frac{ma^2}{3} \omega$$

$$\omega = \frac{3\hat{P}}{ma}$$

$$v_{Ax} = v_{Cx} - a\omega$$

$$= 0 - \frac{3\hat{P}}{m}$$

Center of Percussion - pt along axis of pt fixed & cm.  $\therefore$   
 $\hat{P}$  gives 0 motion at ft. pt.



lin mom.

$$0 + |\hat{P}| \cdot |\hat{R}| = m v_c$$

ang mom

$$0 + |\hat{P}| y = I_o \omega$$

C.P.  $y$  for  $|\hat{R}| = 0$

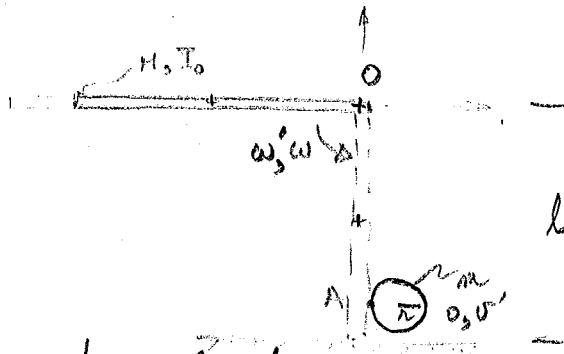
$$\hat{P} = m \bar{v}_c = m h \omega \quad (1a)$$

$$|\hat{P}| y = m k_o^2 \omega \quad (2a)$$

$$m h \omega y = m k_o^2 \omega$$

$$y = k_o^2 / h$$

Problems:



To calc.  $\omega$  use principle of energy

$$T + V = E$$

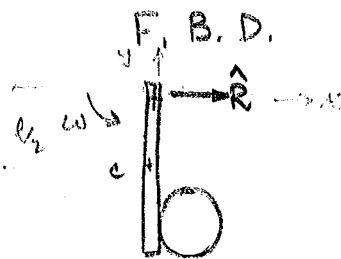
$$0 + 0 = \frac{1}{2} I_o \omega^2 - M g l / 2$$

$$\frac{M l^2}{3} = I_o$$

$$0 = \frac{1}{2} \frac{M l^2}{3} \omega^2 - M g l / 2$$

$$\omega = \sqrt{\frac{3g}{l}}$$

$\omega', v', \hat{R}$



$$v_c = l/2 \omega$$

$$M l/2 \omega + \hat{R} = M l/2 \omega' + m v'$$

$$I_o \omega + 0 = I_o \omega' + m v' (l/2)$$

$$e = \frac{v_{\text{sep}}}{v_{\text{app}}} = \frac{\omega'(l-r) - v'}{\omega(l-r)}$$

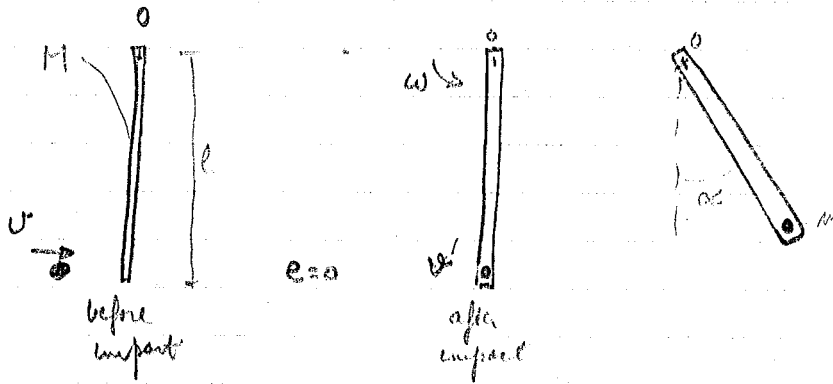
$$v' = \frac{(1+e)(l-r) \sqrt{\frac{3g}{l}}}{\left[1 + 3\frac{m}{M}\left(1 - \frac{r}{l}\right)^2\right]}$$

$$|\hat{R}| = \left[1 - \frac{3}{2}\left(1 - \frac{r}{l}\right)\right] m v'$$

$$\omega' = \omega \left[ \frac{1 - 3e\frac{m}{M}\left(1 - \frac{r}{l}\right)^2}{1 + 3\frac{m}{M}\left(1 - \frac{r}{l}\right)^2} \right]$$

Ballistic Pendulum.

$$m \ll M$$



$$mvl + 0 = mv'l + I_0 \omega$$

$$v', \omega, v$$

$$e = \frac{v_{\text{sep}}}{v_{\text{app}}} = \frac{\omega l - v'}{v - 0} = 0$$

$$|v' - \omega l|$$

$$\omega = \frac{mvl}{ml^2 + I_0}$$

measure alpha & apply conservation of energy

$$\frac{1}{2} I_0 \omega^2 + \frac{1}{2} m v'^2 - mgl - Mgl/2 = 0 - Mgl/2 \cos \alpha - mgl \cos \alpha$$

$$\left[ \frac{1}{2} I_0 + \frac{1}{2} ml^2 \right] \omega^2 = [mgl + Mgl/2] (1 - \cos \alpha)$$

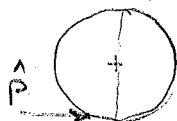
Assume  $m \ll \frac{M}{2}$   $ml^2 \ll I_0$

$$v = \sqrt{\frac{I_0 M l (1 - \cos \alpha)}{ml}}$$

8.21



8.23



8.27

8.25 - not needed

4/29/71

# General Motion of a Rigid Body

## Kinematics

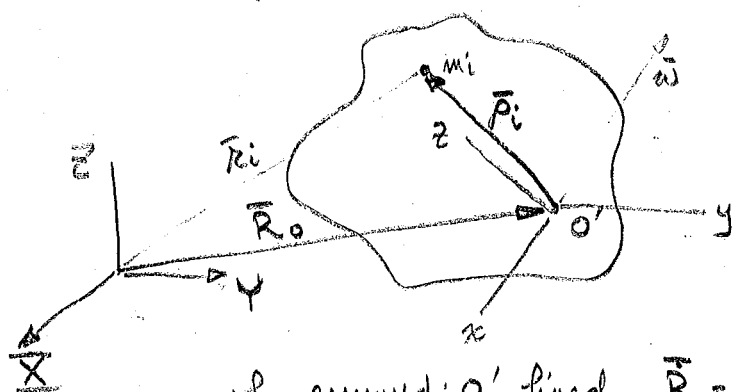
### Axiom:

The displ. of rigid body is completely descr. by displ. of 3 non-collinear pts.

### Euler's Theorem:

The most gen. displ. of rigid body about fixed pt is equiv to a rotation about a line through pt.

### Velocity of a Pt in a Rigid Body

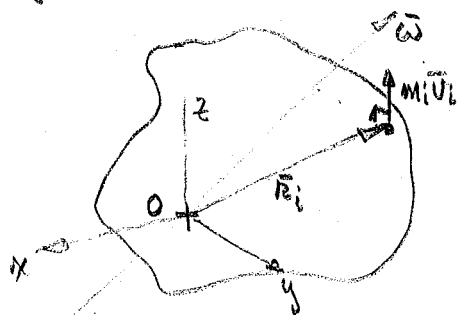


$$\bar{r}_i = \bar{R}_0 + \bar{\rho}_i$$

$$\bar{v}_i = \bar{v}_{ab} = \frac{d\bar{R}_0}{dt} + \frac{\delta \bar{\rho}_i}{\delta t} + \bar{\omega} \times \bar{\rho}_i$$

if assumed:  $O'$  fixed  $\bar{R}_0 = 0$  + if  $x, y, z$  axis fixed in body  
then  $\frac{\delta \bar{\rho}_i}{\delta t} = 0$   
 $\therefore \bar{v}_{ab} = \bar{\omega} \times \bar{\rho}_i$

### Angular Momentum of a Rigid Body Rotating About fixed pt.



$$\begin{aligned} \bar{h}_0 &= \sum_i \bar{r}_i \times m_i \bar{v}_i \\ &= \sum_i m_i \bar{r}_i \times (\bar{\omega} \times \bar{r}_i) \end{aligned}$$

$$\begin{aligned} \bar{r}_i \times (\bar{\omega} \times \bar{r}_i) &= \begin{vmatrix} \bar{i} & \bar{j} & \bar{k} \\ x_i & y_i & z_i \\ \lambda_1 & \lambda_2 & \lambda_3 \end{vmatrix} \\ &= \bar{i} (y_i \lambda_3 - z_i \lambda_2) + \bar{j} (z_i \lambda_1 - x_i \lambda_3) \\ &\quad + \bar{k} (x_i \lambda_2 - y_i \lambda_1) \end{aligned}$$

$$\bar{\omega} \times \bar{r}_i = \begin{vmatrix} \bar{i} & \bar{j} & \bar{k} \\ \omega_x & \omega_y & \omega_z \\ x_i & y_i & z_i \end{vmatrix}$$

$$\begin{aligned} &= \bar{i} (\omega_y z_i - \omega_z y_i) + \bar{j} (\omega_z x_i - \omega_x z_i) \\ &\quad + \bar{k} (\omega_x y_i - \omega_y x_i) \end{aligned}$$

$$\bar{h}_0 = \bar{i} \sum m_i [\omega_x (y_i^2 + z_i^2) - \omega_y (x_i y_i) - \omega_z (x_i z_i)] + \bar{j} \sum m_i [\omega_y (x_i^2 + z_i^2) - \omega_x (x_i y_i) - \omega_z (y_i z_i)] + \bar{k} \sum m_i [\omega_z (x_i^2 + y_i^2) - \omega_x (y_i z_i) - \omega_y (x_i z_i)]$$

$$\begin{aligned} \text{let } I_{xx} &= \sum_i m_i (y_i^2 + z_i^2) = \int (y^2 + z^2) dm \\ I_{yy} &= \sum_i m_i (z_i^2 + x_i^2) = \int (z^2 + x^2) dm \\ I_{zz} &= \sum_i m_i (x_i^2 + y_i^2) = \int (x^2 + y^2) dm \end{aligned} \quad \left. \vphantom{\begin{aligned} I_{xx} \\ I_{yy} \\ I_{zz} \end{aligned}} \right\} \begin{array}{l} \text{Mass Moments} \\ \text{of inertia.} \end{array}$$

$$\text{define } I_{xy} = - \sum_i m_i x_i y_i = - \int xy dm$$

$$\begin{aligned} \vec{h}_o &= (I_{xx} \omega_x + I_{xy} \omega_y + I_{xz} \omega_z) \vec{i} + (I_{yx} \omega_x + I_{yy} \omega_y + I_{yz} \omega_z) \vec{j} \\ &\quad + (I_{zx} \omega_x + I_{zy} \omega_y + I_{zz} \omega_z) \vec{k} \end{aligned}$$

If at O we find principle axes  $I_{12} \rightarrow 0$   
if  $x, y, z$  principal axes then

$$\vec{h}_o = I_{xx} \omega_x \vec{i} + I_{yy} \omega_y \vec{j} + I_{zz} \omega_z \vec{k}$$

ang momentum vector doesn't lie on  $\vec{\omega}$  vector.

if  $x_p, y_p, z_p$  and  $\vec{\omega}$  lies on one of the axes then  $h_o = I_{ii} \omega_i$

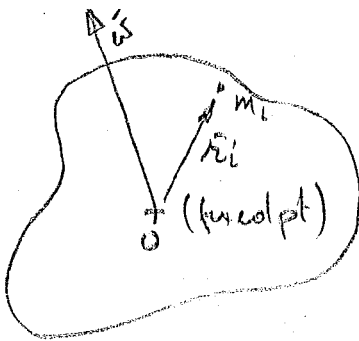
$$\vec{N} = \frac{d}{dt} \vec{h}$$

5/4/71

Exam Motion of Rigid Bodies in Plane, Collisions - 2 quest.

2:00 PM Exam  
5th HR 215

$\vec{h} = I_{xx} \omega_x \vec{i} + I_{yy} \omega_y \vec{j} + I_{zz} \omega_z \vec{k}$  principal axes only  
Kinetic Energy for Rigid Body Rotating about Fixed Point



$$\begin{aligned}
 T &= \sum_i \frac{1}{2} m_i \vec{v}_i \cdot \vec{v}_i \\
 &= \sum_i \frac{1}{2} (\vec{\omega} \times \vec{r}_i) \cdot (m_i \vec{v}_i) \\
 &= \sum_i \frac{1}{2} \vec{\omega} \cdot (\underbrace{\vec{r}_i \times m_i \vec{v}_i}_{\vec{h}_i})
 \end{aligned}$$

$$T = \sum_i \frac{1}{2} \vec{\omega} \cdot \vec{h}_i = \frac{1}{2} \vec{\omega} \cdot \vec{h}$$

$$\vec{\omega} = \omega_x \vec{i} + \omega_y \vec{j} + \omega_z \vec{k}$$

$$\vec{h} = I_{xx} \omega_x \vec{i} + I_{yy} \omega_y \vec{j} + I_{zz} \omega_z \vec{k}$$

$$T = \frac{1}{2} [I_{xx} \omega_x^2 + I_{yy} \omega_y^2 + I_{zz} \omega_z^2]$$

for general motion

$$T = \frac{1}{2} [I_{xx} \omega_x^2 + \dots] + \frac{1}{2} M [v_{cx}^2 + v_{cy}^2 + v_{cz}^2]$$

Mass Moment of Inertia -  $I_{xx} = \int_M (y^2 + z^2) dm$

Principal Axes -  $I_{xy} = I_{yz} = I_{zx} = 0$

Euler's Equation of Motion

$$\vec{N} = \frac{d\vec{h}}{dt} \quad \vec{h} \text{ for cm or fixed pt.}$$

$$\vec{h} = I_{xx} \omega_x \vec{i} + I_{yy} \omega_y \vec{j} + I_{zz} \omega_z \vec{k} \quad \text{principal axes only}$$

$\frac{d\vec{h}}{dt} = \frac{\delta \vec{h}}{\delta t} + \vec{\omega} \times \vec{h}$  for axes fixed in body Euler's Equation will be developed.

$$\frac{d\vec{h}}{dt} = \vec{N} = I_{xx} \dot{\omega}_x \vec{i} + I_{yy} \dot{\omega}_y \vec{j} + I_{zz} \dot{\omega}_z \vec{k} + \begin{vmatrix} \vec{i} & \vec{j} & \vec{k} \\ \omega_x & \omega_y & \omega_z \\ I_{xx}\omega_x & I_{yy}\omega_y & I_{zz}\omega_z \end{vmatrix}$$

$$\vec{N} = \vec{i} [I_{xx} \dot{\omega}_x + I_{zz} \omega_z \omega_y - I_{yy} \omega_y \omega_z] + \vec{j} [I_{yy} \dot{\omega}_y + I_{xx} \omega_x \omega_z - I_{zz} \omega_z \omega_x] + \vec{k} [I_{zz} \dot{\omega}_z + I_{yy} \omega_y \omega_x - I_{xx} \omega_x \omega_y]$$

$$\begin{aligned} N_x &= I_{xx} \dot{\omega}_x + (I_{zz} - I_{yy}) \omega_y \omega_z \\ N_y &= I_{yy} \dot{\omega}_y + (I_{xx} - I_{zz}) \omega_z \omega_x \\ N_z &= I_{zz} \dot{\omega}_z + (I_{yy} - I_{xx}) \omega_x \omega_y \end{aligned}$$

Example Rigid Body - Constrained to move about fixed axis  $\vec{\omega}$  const.

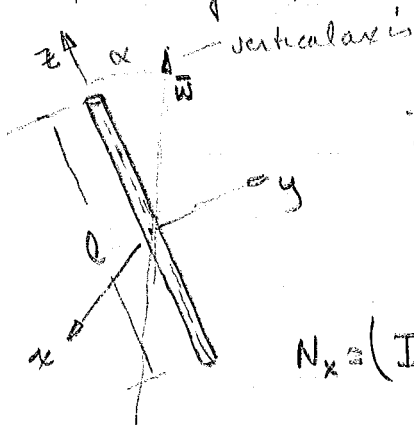
$$\dot{\omega}_x = \dot{\omega}_y = \dot{\omega}_z = 0$$

$$N_x = (I_{zz} - I_{yy}) \omega_y \omega_z$$

$$N_y = (I_{xx} - I_{zz}) \omega_z \omega_x$$

$$N_z = (I_{yy} - I_{xx}) \omega_x \omega_y$$

For a thin uniform rod.



$x, y, z$  are principal axes fixed to body

$$I_{zz} = 0$$

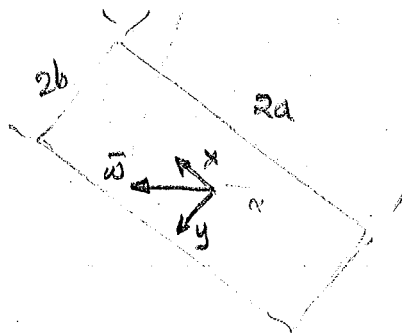
$$I_{xx} = I_{yy} = \frac{ml^2}{12}$$

$$N_z = 0 \quad I_{xx} = I_{yy}$$

$$N_y = 0 \quad \omega_x = 0$$

$$\begin{aligned} N_x &= (I_{zz} - I_{yy}) \omega_y \omega_z = -\frac{ml^2}{12} (\omega \sin \alpha)(\omega \cos \alpha) \\ &= -\frac{ml^2}{12} \omega^2 \sin \alpha \cos \alpha \end{aligned}$$

Rectangular Plate rotates with constant speed about diagonal  $\vec{N} = ??$



$$N_x = (I_{zz} - I_{yy}) \omega_y \omega_z$$

$$N_y = (I_{xx} - I_{zz}) \omega_z \omega_x$$

$$N_z = (I_{yy} - I_{xx}) \omega_x \omega_y$$

$$\vec{\omega} = \omega \cos \alpha \hat{z} + \omega \sin \alpha \hat{y}$$

$$I_{xx} = \frac{1}{3} m b^2, \quad I_{yy} = \frac{1}{3} m a^2$$

$$I_{zz} = \frac{1}{3} m (b^2 + a^2)$$

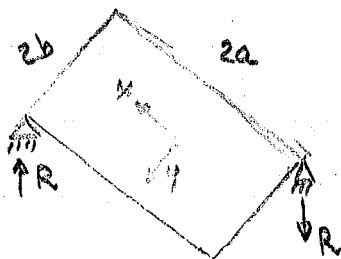
$$N_x, N_y = 0$$

$$N_z = \left( \frac{1}{3} m a^2 - \frac{1}{3} m b^2 \right) \omega^2 \cos \alpha \sin \alpha$$



$$= \frac{1}{3} m \frac{(a^2 - b^2)}{a^2 + b^2} a b \omega^2$$

Calculate Reaction



if  $a > b$  ↷

$$R \left[ \sqrt{(2b)^2 + (2a)^2} \right] - N_z = 0$$

$$R = \frac{N_z}{2\sqrt{a^2 + b^2}} = \frac{N_z}{2\sqrt{a^2 + b^2}} = \frac{1}{6} \frac{(a^2 - b^2)}{\sqrt{a^2 + b^2}} a b \omega^2$$



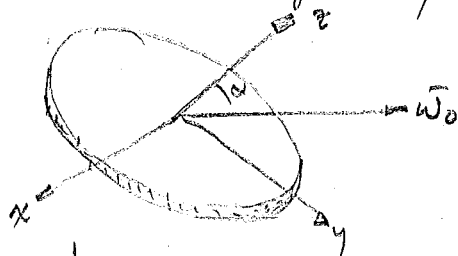
5/10/71

$$N_x = I_{xx} \dot{\omega}_x + \omega_y \omega_z (I_{zz} - I_{yy})$$

$$N_y = I_{yy} \dot{\omega}_y + \omega_z \omega_x (I_{xx} - I_{zz})$$

$$N_z = I_{zz} \dot{\omega}_z + \omega_x \omega_y (I_{yy} - I_{xx})$$

Free Rotation, Rigid Body Axis of Symmetry.



Disk mass  $m$ , Rad a

Set spinning  $\bar{\omega}_0$  in  $yz$  plane.

$$\bar{\omega} = \omega_x \bar{i} + \omega_y \bar{j} + \omega_z \bar{k}$$

$$\bar{\omega}_0 = 0 + \omega_0 \sin \alpha \bar{j} + \omega_0 \cos \alpha \bar{k}$$

$\bar{N} = 0$  no torque

let  $I = I_{xx} = I_{yy}$   $I_{ss} = I_{zz}$

$$0 = I \dot{\omega}_x + \omega_y \omega_z (I_{ss} - I)$$

$$0 = I \dot{\omega}_y + \omega_z \omega_x (I - I_{ss})$$

$$0 = I_{ss} \dot{\omega}_z + \omega_x \omega_y (I - I) \rightarrow \dot{\omega}_z = 0 \quad \omega_z = \text{const}$$

$$\boxed{\omega_z = \omega_0 \cos \alpha}$$

Call  $\Omega = \left( \frac{I_{ss}}{I} - 1 \right) \omega_0 \cos \alpha$

$$\dot{\omega}_x + \omega_y \Omega = 0$$

$$\dot{\omega}_y - \omega_x \Omega = 0$$

$$\ddot{\omega}_y - \dot{\omega}_x \Omega = 0$$

$$\dot{\omega}_x = \frac{\ddot{\omega}_y}{\Omega} \rightarrow \ddot{\omega}_y + \omega_y \Omega^2 = 0$$

$$\omega_y = A \cos \Omega t + B \sin \Omega t = \omega_1 \cos \Omega t$$

$$\omega_y(0) = \omega_1 = \omega_0 \sin \alpha \quad \boxed{\omega_y = \omega_0 \sin \alpha \cos \Omega t}$$

$$\dot{\omega}_y = -\omega_0 \sin \alpha (\Omega \sin \Omega t) \quad \therefore \boxed{\omega_x = -\omega_0 \sin \alpha (\sin \Omega t)}$$

$$\omega_x^2 + \omega_y^2 = \omega_1^2 = \text{const.} = \omega_0^2 \sin^2 \alpha$$

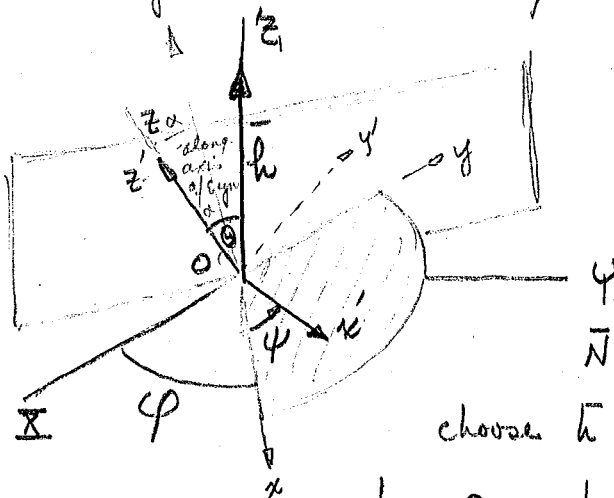
the precession of  $\bar{\omega} = \Omega$  as seen from the moving frame of reference

$$\frac{1}{2} (I_{xx} \omega_x^2 + I_{yy} \omega_y^2 + I_{zz} \omega_z^2) = T = \text{const.} \quad \text{C}_1$$

$$\bar{N} = \frac{dh}{dt} = \text{const in space}$$

$$\vec{h} \cdot \vec{h} = h^2 = I_{xx} \omega_x^2 + I_{yy} \omega_y^2 + I_{zz} \omega_z^2 = C_2$$

Eulerian Angles  $\rightarrow$  Orientation of Rotation Relative to a fixed Coord. System.



Eulerian Angles  $\varphi, \psi, \theta$

$$\vec{N} = 0 \quad \vec{h} = \text{const.}$$

choose  $\vec{h}$  to coincide with  $\vec{Z}$

$$h_x = 0 \quad h_y = h \sin \theta \quad h_z = h \cos \theta$$

$$h_x = I_{xx} \omega_x = 0 \quad \omega_x = 0$$

$$h_y = I_{yy} \omega_y = h \sin \theta = \omega \sin \alpha I$$

$$h_z = I_{zz} \omega_z = I_s \omega \cos \alpha = h \cos \theta$$

$$\frac{h_y}{h_z} = \tan \theta = \frac{I}{I_s} \tan \alpha$$

In terms of Eulerian Angles

$$\omega_x = 0$$

$$\omega_y = \dot{\varphi} \sin \theta \quad \omega_z = \dot{\varphi} \cos \theta + \dot{\psi}$$

$$\omega_y = \omega \sin \alpha = \dot{\varphi} \sin \theta$$

$$\dot{\varphi} = \frac{\omega \sin \alpha}{\sin \theta}$$

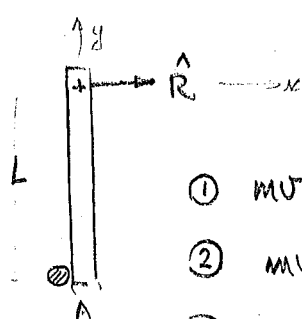
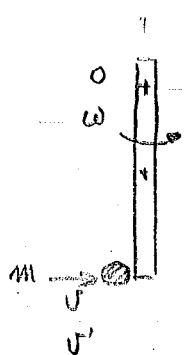
$$\dot{\varphi} = \omega \sqrt{1 + \left( \frac{I_s}{I} - 1 \right) \cos^2 \alpha}$$

for a disk  $\frac{I_s}{I} = 2 \quad \Omega = \omega \cos \alpha$

if  $\alpha$  is small  $\Omega \approx \omega$

$$\dot{\varphi} \approx 2\omega$$

$$\dot{\varphi} \approx \omega \sqrt{1 + 3 \cos^2 \alpha}$$



$$\textcircled{1} \quad m\vec{v} + \hat{R} = m\vec{v}' + M\vec{v}_c \quad v_c = \omega \frac{L}{2}$$

$$\textcircled{2} \quad m\vec{v}L = m\vec{v}'L + I_0 \omega$$

$$\textcircled{3} \quad e = \frac{\omega L - v'}{v - 0} \quad \frac{ML^2}{3}$$

find  $v', \omega, \hat{R}$

$$(0.01)(100) + \hat{R} = (0.01)v' + 1.5\omega \frac{3}{2} \quad \textcircled{1A}$$

$$(0.01)(100)3 = (0.01)(3)v' + \frac{(1.5)(9)}{3}\omega \quad \textcircled{2A}$$

$$.5 = \frac{3\omega - v'}{100} \quad \textcircled{3A}$$

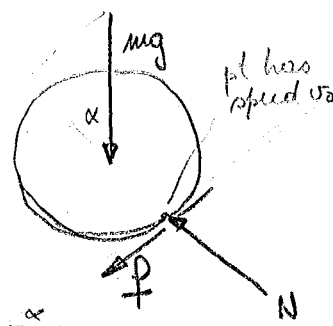
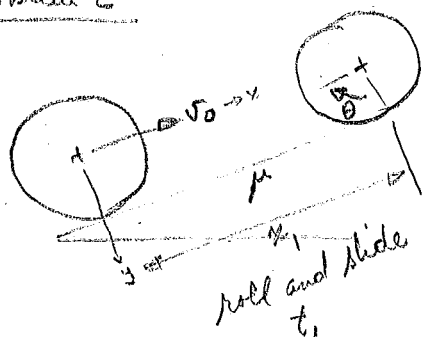
$$v' = -41.5 \text{ ft/sec}$$

$$\omega = 2.83 \text{ rad/sec}$$

$$\hat{R} = +1.705 \text{ lbsec}$$

$$\begin{aligned} 0 &\leftarrow m\vec{v} - \hat{P} = m\vec{v}' \\ \hat{P} &= m(v - v') = 1.415 \text{ lbsec} \end{aligned}$$

## Problem 2



$$mg \cos \alpha - N = m\ddot{y}_c = 0 \quad \textcircled{1}$$

$$N = mg \cos \alpha$$

$$-mg \sin \alpha - \mu mg \cos \alpha = m\ddot{x}_c \quad \textcircled{2}$$

$$(\mu mg \cos \alpha) r = I_c \ddot{\theta} \quad \textcircled{3}$$

$$\ddot{x}_c = -g(\sin \alpha + \mu \cos \alpha)$$

$$\dot{x}_c = -gt(\sin \alpha + \mu \cos \alpha) + v_0 \quad \textcircled{4}$$

$$x_c = -gt^2 \frac{1}{2} (\sin \alpha + \mu \cos \alpha) + v_0 t \quad \textcircled{5}$$

$$\ddot{\theta} = \frac{(\mu mg \cos \alpha) r}{\frac{3}{5} m r^2} = \frac{5 \mu g \cos \alpha}{2 r}$$

$$\dot{\theta} = \frac{5}{2} \frac{\mu g \cos \alpha}{r} t + 0 \quad (6)$$

$$\theta = \left( \frac{5}{2} \frac{\mu g \cos \alpha}{r} \right) \frac{t^2}{2} \quad (7)$$

at pure roll  $\dot{x}_c = r \dot{\theta}$

$$\therefore -g(\sin \alpha + \mu \cos \alpha) t^* + v_0 = \frac{5}{2} (\mu g \cos \alpha) t^*$$

$$t^* = \frac{v_0}{g(\sin \alpha + \mu \frac{7}{2} \cos \alpha)}$$

$$x^* = -\frac{g}{2} (\sin \alpha + \mu \cos \alpha) \left[ \frac{v_0}{g(\sin \alpha + \frac{7}{2} \mu \cos \alpha)} \right]^2 + v_0 \left[ \frac{v_0}{g(\sin \alpha + \mu \frac{7}{2} \cos \alpha)} \right]$$

$$= \frac{v_0^2}{2g} \left[ \frac{\sin \alpha + 6\mu \cos \alpha}{(\sin \alpha + \frac{7}{2} \mu \cos \alpha)^2} \right]$$

$$2v_0^2 \left[ (\sin \alpha + \mu \frac{7}{2} \cos \alpha) - v_0^2 \left[ \sin \alpha + \mu \cos \alpha \right] \right]$$

$$v_0^2 \left[ \sin \alpha + 6\mu \cos \alpha \right] \quad \checkmark$$

1. A motorist enters a curve of 500-ft. radius at a speed of 45 mph. As he applies his brakes, he decreases his speed at a constant rate of 5 ft/sec<sup>2</sup>. Determine the magnitude of the total acceleration of the automobile when its speed is 40 mph.
2. A particle moves in a plane with constant speed. Prove that its acceleration is perpendicular to its velocity.
3. A particle moves in an elliptical path with constant speed. At what points is the magnitude of the acceleration (1) a maximum, (2) a minimum? If the axes of the elliptical path are 4 and 2 ft. respectively, and if the speed of the particle is 8 ft/sec, determine the magnitudes of these accelerations.
4. A particle moves along a curve

$$y = c \sin px$$

where  $c$  and  $p$  are constants. The component of velocity in the  $x$ -direction is a constant ( $u$ ). Find the acceleration and describe the hodograph.

5. Starting from

$$x = r \cos \theta$$

$$y = r \sin \theta$$

calculate  $\ddot{x}$  and  $\ddot{y}$ . Hence, by resolving the acceleration vector along and perpendicular to the radius vector, establish the acceleration components for plane polar coordinate system derived in class.

6. A motorboat experiences a resistance proportional to the square of the speed. The engine is switched off when the speed is 50 ft/sec. When the boat has moved through a distance of 60 feet, its speed has been reduced to 20 ft/sec. Find (to the nearest foot) the total distance traversed when the speed has been reduced to 10 ft/sec.
7. The two-dimensional motion of a particle is defined by the relations

$$r = k(1 + \cos \frac{\pi t}{2})$$

$$\theta = \frac{\pi t}{2}$$

Determine the velocity and acceleration of the particle when (a)  $t = 1$  and (b)  $t = 2$ .

Page 10

10-10-1944

1. The first part of the report deals with the general situation of the country. It is a very interesting and informative account of the country and its people. The author has done a great deal of research and has written a very well informed and interesting account of the country.

2. The second part of the report deals with the political situation. It is a very interesting and informative account of the political situation and the various parties and movements. The author has done a great deal of research and has written a very well informed and interesting account of the political situation.

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5. The fifth part of the report deals with the cultural situation. It is a very interesting and informative account of the cultural situation and the various cultural movements and movements. The author has done a great deal of research and has written a very well informed and interesting account of the cultural situation.

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7. The seventh part of the report deals with the foreign relations situation. It is a very interesting and informative account of the foreign relations situation and the various foreign relations movements and movements. The author has done a great deal of research and has written a very well informed and interesting account of the foreign relations situation.

8. The eighth part of the report deals with the future of the country. It is a very interesting and informative account of the future of the country and the various future movements and movements. The author has done a great deal of research and has written a very well informed and interesting account of the future of the country.

9. The ninth part of the report deals with the conclusion. It is a very interesting and informative account of the conclusion and the various conclusion movements and movements. The author has done a great deal of research and has written a very well informed and interesting account of the conclusion.

10. The tenth part of the report deals with the appendix. It is a very interesting and informative account of the appendix and the various appendix movements and movements. The author has done a great deal of research and has written a very well informed and interesting account of the appendix.

11. The eleventh part of the report deals with the bibliography. It is a very interesting and informative account of the bibliography and the various bibliography movements and movements. The author has done a great deal of research and has written a very well informed and interesting account of the bibliography.

12. The twelfth part of the report deals with the index. It is a very interesting and informative account of the index and the various index movements and movements. The author has done a great deal of research and has written a very well informed and interesting account of the index.

13. The thirteenth part of the report deals with the conclusion. It is a very interesting and informative account of the conclusion and the various conclusion movements and movements. The author has done a great deal of research and has written a very well informed and interesting account of the conclusion.

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15. The fifteenth part of the report deals with the bibliography. It is a very interesting and informative account of the bibliography and the various bibliography movements and movements. The author has done a great deal of research and has written a very well informed and interesting account of the bibliography.

8. A particle moves along the hyperbolic spiral  $r\theta = b$ . (a) Determine the magnitude of the velocity of the particle in terms of  $b$ ,  $\theta$ , and  $d\theta/dt$ .  
(b) Knowing that  $d\theta/dt$  is constant and denoting this by  $\omega$ , determine the magnitude of the acceleration in terms of  $b$ ,  $\theta$ , and  $\omega$ .
9. If  $V = x^2 + y^2 + z^2 + xy + x$ , at what points in space is the vector  $\text{grad } V$  parallel to the  $z$ -axis?
10. A scalar field is given over a plane by

$$V = \frac{x^2 + y^2}{2x}$$

What are the level curves? (Curves of constant  $V$ ). Show that, at the point with polar coordinates  $(r, \theta)$ ,  $\text{grad } V$  is inclined to the  $x$ -axis at an angle  $2\theta$  and its magnitude is  $(\sec^2 \theta)/2$ .

[illegible]

the 1990s, the number of people in the world who are illiterate has increased from 1.2 billion to 1.5 billion. The number of illiterate people in the world is projected to reach 1.7 billion by the year 2015. The number of illiterate people in the world is projected to reach 1.7 billion by the year 2015.

1. The first of these is the fact that the majority of the population of the United States is now living in urban areas. This is a result of the process of urbanization, which has been going on since the beginning of the 20th century. The process of urbanization is the movement of people from rural areas to urban areas. This movement is caused by a number of factors, including the search for better living conditions, the desire for education, and the need for employment. The result of this process is that the majority of the population now lives in cities and towns. This has a number of implications for the future of the United States. For example, it means that the majority of the population will be living in areas where there are a high concentration of people. This can lead to a number of problems, including overcrowding, pollution, and a lack of resources. It also means that the majority of the population will be living in areas where there are a high concentration of people who are not employed. This can lead to a number of problems, including poverty, crime, and social unrest. Therefore, it is important to consider the implications of the process of urbanization for the future of the United States.

...the ... of ...



H.W. #1

AE 211

Dr. Nardo

1.  $a_T = -5 \text{ ft/sec}^2$

$$a_N = \frac{v^2}{\rho}$$

$$\rho = 500 \text{ ft} \quad v = 40 \text{ mph} = 58.7 \text{ ft/sec}$$

$$a_N = \frac{(58.7)^2}{500} = 6.88 \text{ ft/sec}^2$$

$$a = \sqrt{(6.88)^2 + (-5)^2} = \sqrt{25 + 47.4} = 8.51 \text{ ft/sec}^2$$

2.

Given  $|\vec{v}| = c$

Prove:  $\vec{a} \perp \vec{v}$

$$\vec{v} = v \vec{e}_T, \quad \vec{a} = \dot{v} \vec{e}_T + \frac{v^2}{\rho} \vec{e}_N$$

then

$$\vec{v} \cdot \vec{a} = v \dot{v} = 0 \quad (\text{since } v = c, \frac{dv}{dt} = 0)$$

this gives two cases,

1.  $\vec{v}, \vec{a} = 0$

2.  $\vec{v} \perp \vec{a}$

in first case  $\vec{v} \neq 0$  since  $v$  is finite;  $\vec{a} \neq 0$  but  $\vec{a} = a_N = \frac{v^2}{\rho} \neq 0$   
this leaves case 2.

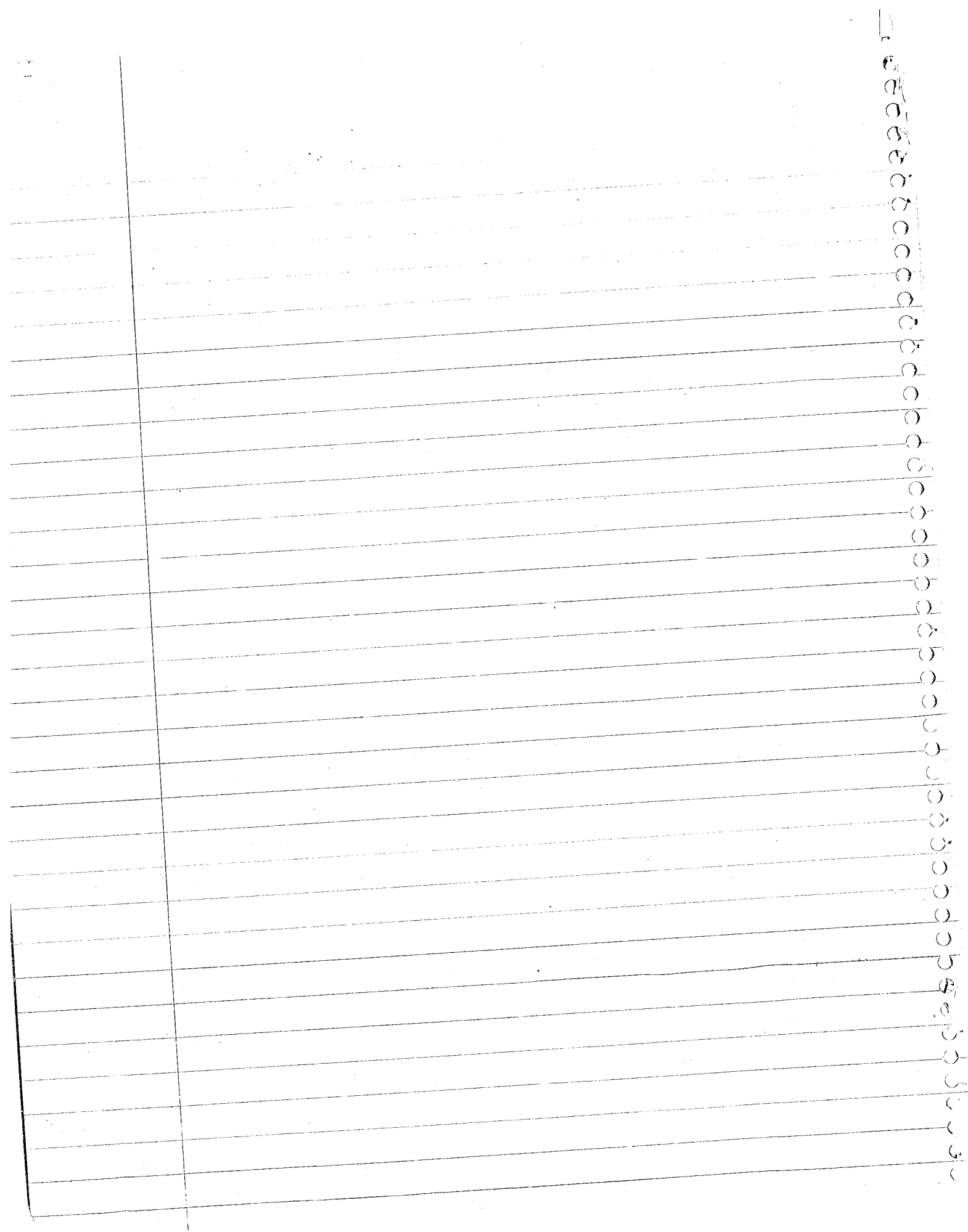
(The case where  $\rho = \infty$  is not considered.)

Therefore  $\vec{a} \perp \vec{v}$ .

QED

Excellent

10



Cesar Levy

1.  $x = r \cos \theta$

$$\dot{x} = \dot{r} \cos \theta - r \dot{\theta} \sin \theta$$

$$\ddot{x} = (\ddot{r} - r \dot{\theta}^2) \cos \theta - (2\dot{r} \dot{\theta} + r \ddot{\theta}) \sin \theta$$

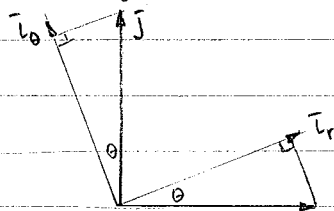
$$y = r \sin \theta$$

$$\dot{y} = \dot{r} \sin \theta + r \dot{\theta} \cos \theta$$

$$\ddot{y} = (\ddot{r} - r \dot{\theta}^2) \sin \theta + (2\dot{r} \dot{\theta} + r \ddot{\theta}) \cos \theta$$

$$\vec{r} = r \cos \theta \vec{i} + r \sin \theta \vec{j}$$

$$\vec{a} = \ddot{x} \vec{i} + \ddot{y} \vec{j}$$



$$\vec{i}_r = \vec{i} \cos \theta + \vec{j} \sin \theta$$

$$\vec{i}_\theta = \vec{j} \cos \theta - \vec{i} \sin \theta$$

$$\vec{i} = \vec{i}_r \cos \theta - \vec{i}_\theta \sin \theta$$

$$\vec{j} = \vec{i}_r \sin \theta + \vec{i}_\theta \cos \theta$$

$$\begin{aligned}
 \vec{a} &= \ddot{x} [\vec{i}_r \cos \theta - \vec{i}_\theta \sin \theta] + \ddot{y} [\vec{i}_r \sin \theta + \vec{i}_\theta \cos \theta] \\
 &= \vec{i}_r [\ddot{r} - r \dot{\theta}^2] \cos^2 \theta - \vec{i}_r [2\dot{r} \dot{\theta} + r \ddot{\theta}] \cos \theta \sin \theta \\
 &\quad + \vec{i}_\theta [\ddot{r} - r \dot{\theta}^2] \sin \theta \cos \theta + \vec{i}_\theta [2\dot{r} \dot{\theta} + r \ddot{\theta}] \sin^2 \theta \\
 &\quad + \vec{i}_r [\ddot{r} - r \dot{\theta}^2] \sin^2 \theta + \vec{i}_r [2\dot{r} \dot{\theta} + r \ddot{\theta}] \sin \theta \cos \theta \\
 &\quad + \vec{i}_\theta [\ddot{r} - r \dot{\theta}^2] \sin \theta \cos \theta + \vec{i}_\theta [2\dot{r} \dot{\theta} + r \ddot{\theta}] \cos^2 \theta
 \end{aligned}$$

$$\vec{a} = \vec{i}_r [\ddot{r} - r \dot{\theta}^2] + \vec{i}_\theta [2\dot{r} \dot{\theta} + r \ddot{\theta}]$$

(10)



$$\sum F_x = m\ddot{x} + kV^2 = 0$$

$$\ddot{x} = -\frac{kV^2}{m}$$

@  $t=0$   $V_0 = 50$   $s_0 = 0$

$t = t^*$   $V = 20$   $s = 60$

$$a = V \frac{dV}{ds} = -\frac{kV^2}{m}; \quad -\frac{dV}{V} = \frac{k}{m} ds$$

$$\ln \left[ \frac{V_0}{V} \right] = \frac{k}{m} [s - s_0]; \quad \ln \left[ \frac{50}{V} \right] = \frac{k}{m} s$$

@  $t = t^*$

$$\ln \left[ \frac{5}{2} \right] = \frac{k}{m} 60 \quad \frac{k}{m} = \frac{1}{60} \ln \left[ \frac{5}{2} \right] \quad \checkmark$$

@  $V = 10$  ft/sec

$$\ln \left[ \frac{50}{10} \right] = \frac{1}{60} \ln \left[ \frac{5}{2} \right] s$$

10

$$s = 60 \frac{\ln(5)}{\ln(5/2)} \approx 105 \text{ ft} \quad \checkmark$$

3.  $r = k(1 + \cos \frac{\pi t}{2})$   $\theta = \frac{\pi t}{2}$

$$\vec{v} = \dot{r} \vec{e}_r + r \dot{\theta} \vec{e}_\theta = \frac{k\pi}{2} \left[ \left(1 + \cos \frac{\pi t}{2}\right) \vec{e}_\theta - \sin \frac{\pi t}{2} \vec{e}_r \right]$$

@  $t=1$

$$\vec{v} = \frac{k\pi}{2} [\vec{e}_\theta - \vec{e}_r] \quad \checkmark$$

@  $t=2$

$$\vec{v} = 0 \quad \checkmark$$

$$\vec{a} = (\ddot{r} - r\dot{\theta}^2) \vec{e}_r + (2\dot{r}\dot{\theta} + r\ddot{\theta}) \vec{e}_\theta$$

$$= -\frac{k\pi^2}{4} \left[ \left(1 + 2\cos \frac{\pi t}{2}\right) \vec{e}_r + 2\sin \frac{\pi t}{2} \vec{e}_\theta \right]$$

@  $t=1$

$$\vec{a} = -\frac{k\pi^2}{4} [\vec{e}_r + 2\vec{e}_\theta] \quad \checkmark$$

10

@  $t=2$

$$\vec{a} = \frac{k\pi^2}{4} \vec{e}_r \quad \checkmark$$

9.  $\nabla V = (2x+y+1)\vec{i} + (2y+x)\vec{j} + 2z\vec{k}$

if  $\nabla V = \epsilon \vec{k}$  then  $\nabla V = 2z\vec{k}$  only where  $\epsilon = 2k$

$\therefore 2x+y+1=0$  &  $2y+x=0$  simultaneously.

from these two equations:  $x = -2/3$   $y = 1/3$   $-\infty \leq z \leq \infty$

(10)

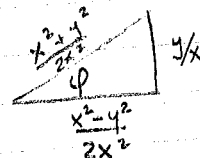
10a.  $V = \frac{x^2+y^2}{2x} = C$

$x^2+y^2 = 2xC \rightarrow (x-C)^2 + y^2 = C^2$  or a circle having a radius of  $C$  and having origin at  $(C,0)$ .

10b.  $\nabla V = \left\{ \frac{2x[2x] - 2[x^2+y^2]}{4x^2} \right\} \vec{i} + \left\{ \frac{2x[2y]}{4x^2} \right\} \vec{j}$

$= \frac{x^2-y^2}{2x^2} \vec{i} + \frac{y}{x} \vec{j}$

$|\nabla V| = \sqrt{\left(\frac{x^2-y^2}{2x^2}\right)^2 + \left(\frac{y}{x}\right)^2} = \frac{x^2+y^2}{2x^2}$



but  $x = r \cos \theta$   $y = r \sin \theta$

$\therefore |\nabla V| = r^2 / [2r^2 \cos^2 \theta] = \sec^2 \theta / 2$

(10)

$\cos \phi = \frac{x^2-y^2}{2x^2} / \frac{x^2+y^2}{2x^2} = r^2 \cos 2\theta / r^2 = \cos 2\theta$

$\therefore \phi = 2\theta$

3.3.

$F = ma_x = ct \Rightarrow mv = \frac{ct^2}{2} + \mathcal{C}_1$  at  $t=0$   $v=0$   $\therefore \mathcal{C}_1 = 0$

$mx = \frac{ct^3}{6} + \mathcal{C}_2$  at  $t=0$   $v=0$   $x=0$   $\therefore \mathcal{C}_2 = 0$

$\therefore x = \frac{ct^3}{6m}$  for  $0 \leq t \leq t_0$

in region where  $t_0 \leq t \leq 2t_0$

$F = 2ct_0 - ct = ma_x$

$$mv = 2ct_0 t - \frac{ct^2}{2} + C_3$$

$$mv_0 = \frac{ct_0^2}{2} = 2ct_0^2 - \frac{ct_0^2}{2} + C_3 \quad \text{at } t=t_0 \quad v=v_0$$

$$C_3 = -ct_0^2$$

$$mv = 2ct_0 t - \frac{ct^2}{2} - ct_0^2$$

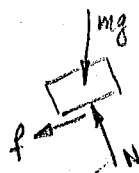
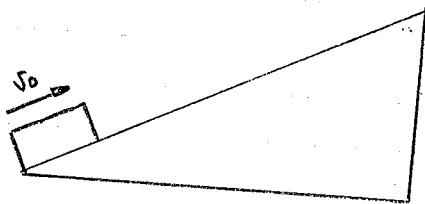
$$mx = ct_0 t^2 - \frac{ct^3}{6} - ct_0^2 t + C_4 \quad \text{at } t=t_0 \quad x=x_0$$

$$mx_0 = \frac{ct_0^3}{6} = ct_0^3 - \frac{ct_0^3}{6} - ct_0^3 + C_4 \quad \therefore C_4 = \frac{ct_0^3}{3}$$

$$mx = ct_0 t^2 - \frac{ct^3}{6} - ct_0^2 t + \frac{ct_0^3}{3}$$

$$\Delta x = \frac{1}{m} \left[ \left( ct_0 t^2 - \frac{ct^3}{6} - ct_0^2 t + \frac{ct_0^3}{3} \right) \Big|_{t_0}^{2t_0} + \left( \frac{ct^3}{6} \right) \Big|_0^{t_0} \right] = \frac{ct_0^3}{m}$$

3.5.



$$-mg \cos \theta + N = ma_y = 0$$

$$N = mg \cos \theta$$

$$F_x = ma_x = -mg \sin \theta - \mu N$$

$$a_x = -g \sin \theta - \mu g \cos \theta$$

$$v = -gt \sin \theta - \mu g t \cos \theta + C_1 \quad \text{at } t=0 \quad v=v_0 \quad \therefore C_1 = v_0$$

$$\therefore v_{up} = -gt \sin \theta - \mu g t \cos \theta + v_0$$

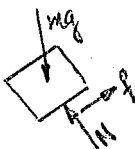
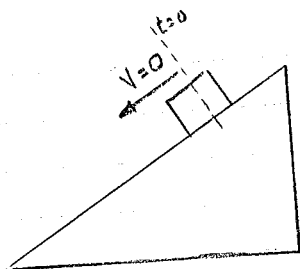
$$x_{up} = -g \frac{t^2}{2} \sin \theta - \mu g \frac{t^2}{2} \cos \theta + v_0 t + C_2; \quad t=0 \quad x=0 \quad \therefore C_2 = 0$$

$$\therefore x_{up} = -g \frac{t^2}{2} \sin \theta - \mu g \frac{t^2}{2} \cos \theta + v_0 t$$

$$\text{at } s=s_0 \quad v=0 \quad \therefore t_{up}^* = \frac{v_0}{g[\sin \theta + \mu \cos \theta]}$$

$$\text{the distance traveled in } t_{up}^* = \frac{v_0^2}{2g[\sin \theta + \mu \cos \theta]}$$

C. Levy  
A5211



$$\begin{aligned} F_y = ma_y &= -mg \cos \theta + N = 0 \\ N &= mg \cos \theta \\ F_x = ma_x &= mg \sin \theta - \mu N \end{aligned}$$

$$a_x = g \sin \theta - \mu g \cos \theta$$

$$v = gt \sin \theta - \mu g t \cos \theta + v_0 \quad \text{at } t=0 \quad v=0 \quad v_0=0$$

$$\therefore v = gt \sin \theta - \mu g t \cos \theta$$

$$x = \frac{gt^2}{2} \sin \theta - \mu \frac{gt^2}{2} \cos \theta + x^0 \quad \text{at } t=0 \quad v=0 \quad x^0=0$$

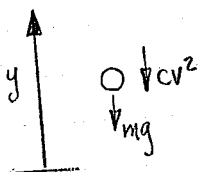
$$\therefore x = \frac{gt^2}{2} \sin \theta - \mu \frac{gt^2}{2} \cos \theta$$

$$\text{at } t = t_{\text{down}}^* \quad x = \frac{v_0^2}{2g[\sin \theta + \mu \cos \theta]} = \frac{g}{2} t_{\text{down}}^{*2} \sin \theta - \mu \frac{g}{2} t_{\text{down}}^{*2} \cos \theta$$

$$t_{\text{down}}^* = \sqrt{\frac{v_0^2}{g^2 [\sin \theta + \mu \cos \theta] [\sin \theta - \mu \cos \theta]}} = \frac{v_0}{g} \sqrt{\frac{1}{\sin^2 \theta - \mu^2 \cos^2 \theta}}$$

$$t_{\text{tot}} = t_{\text{up}}^* + t_{\text{down}}^* = \frac{v_0}{g} \left[ (\sin \theta + \mu \cos \theta)^{-1} + (\sin^2 \theta - \mu^2 \cos^2 \theta)^{-1/2} \right]$$

3.12



$$m\ddot{y} = -mg - cv^2 = -c \left( \frac{mg}{c} + v^2 \right) = m v \frac{dv}{dy}$$

$$dy = -\frac{m}{c} \left( \frac{v dv}{v_t^2 + v^2} \right)$$

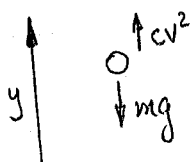
using the cond.  $v = v_0$  @  $y = 0$

$$y = \frac{m}{2c} \ln \left( \frac{v_t^2 + v_0^2}{v_t^2 + v^2} \right)$$

we get

when  $v=0$ :

$$y^* = \frac{m}{2c} \ln \left( \frac{v_t^2 + v_0^2}{v_t^2} \right)$$



$$m v \frac{dv}{dy} = cv^2 - mg$$

$$\frac{m}{c} \frac{v dv}{v^2 - v_t^2} = dy \Rightarrow \frac{m}{2c} \ln(v^2 - v_t^2) = y - y_2$$

when  $v=0$   $y=y^*$  which leads to

$$y = \frac{m}{2c} \ln \left[ \frac{(v^2 - v_t^2)(v_t^2 + v_0^2)}{-v_t^4} \right] \checkmark$$

when  $y=0$

$$\text{either } \frac{m}{2c} = 0 \text{ or } \left[ \frac{(v^2 - v_t^2)(v_t^2 + v_0^2)}{-v_t^4} \right] = 1$$

if  $\frac{m}{2c} = 0$  we have a trivial solution

$\therefore$

$$\left[ \frac{(v^2 - v_t^2)(v_t^2 + v_0^2)}{-v_t^4} \right] = 1$$

$$v^2 - v_t^2 = \frac{-v_t^4}{v_t^2 + v_0^2}$$

$$v^2 = \frac{-v_t^4}{v_t^2 + v_0^2} + v_t^2$$

$$= \frac{-v_t^4}{v_t^2 + v_0^2} + \frac{v_t^2(v_t^2 + v_0^2)}{v_t^2 + v_0^2}$$

$$= \frac{v_t^2 v_0^2}{v_t^2 + v_0^2}$$

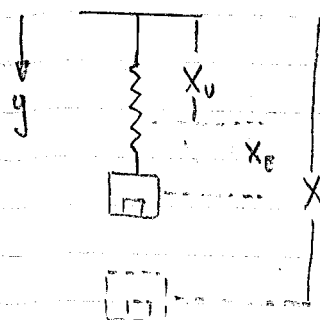
finally:

$$v = \frac{v_t v_0}{(v_t^2 + v_0^2)^{1/2}}$$

QED



3.20

C. Henry  
AE 211

$$(M+m)g - k(X-X_0) = F$$

$$\text{let } y_r = X - X_0 - X_E$$

$$(M+m)g = +k(X_E)$$

$$X_E = \frac{(M+m)g}{k}$$

$$\text{then } y_r = X - X_0 - \frac{(M+m)g}{k}$$

$$\therefore -ky_r = (m+M)\ddot{y}_r$$

from this we get

$$y_r = a \sin \sqrt{\frac{k}{M+m}} t + b \cos \sqrt{\frac{k}{M+m}} t$$

$$\text{at } y_r = d, t = 0 \quad v = 0$$

$$\dot{y}_r = a\omega \cos \omega t - b\omega \sin \omega t \quad \text{where } \omega = \sqrt{\frac{k}{M+m}}$$

$$\therefore 0 = a\omega \quad \therefore a = 0 \Rightarrow \dot{y}_r = -b\omega \sin \omega t$$

$$\text{and } y_r = b \cos \omega t \Rightarrow y_r = d \cos \omega t \quad \checkmark$$

$$\text{at } y_r = -d \quad \dot{y}_r = 0 \quad t = \frac{\pi}{\omega}$$



$$mg - F_R = m\ddot{y}_r = -\cancel{k y_r} \quad \text{sub for } \ddot{y}_r$$

$$\therefore F_R = mg + k y_r \Rightarrow mg - F_R = -\omega^2 d m \cos \omega t$$

$$F_R = mg + k d \cos \sqrt{\frac{k}{M+m}} t \quad F_R = m \left[ g - \frac{k}{M+m} d \cos \omega t \right]$$

$$F_R = 0 \quad d \min = d \text{crit} = \frac{g(M+m)}{k}$$

$$\text{at } y_r = -d \quad F_R = 0$$

$$0 = mg + k d \cos \sqrt{\frac{k}{M+m}} \left( \pi \sqrt{\frac{M+m}{k}} \right) = mg - kd$$

$$\boxed{d = mg/k}$$

8

$$X = X_0 + \frac{mg}{k} + \frac{(m+M)g}{k} = X_0 + \frac{(2m+M)g}{k}$$

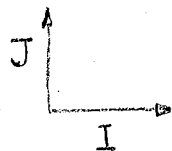
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5.1

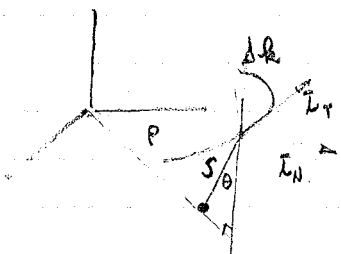


$ma_0 \vec{i} = S \sin \theta \vec{i} + S \cos \theta \vec{j} - mg \vec{j}$   
since the total force on the body is equal to the acceleration of the system  $\times$  mass.

from this

$$\begin{aligned} S \sin \theta &= ma_0 \\ S \cos \theta &= mg \end{aligned}$$

$$\left. \begin{aligned} S \sin \theta &= ma_0 \\ S \cos \theta &= mg \end{aligned} \right\} \Rightarrow S = m(a_0^2 + g^2)^{1/2} \quad \tan \theta = \frac{a_0}{g}$$



$\vec{r} = \frac{v_0^2}{\rho} \vec{i}_N$  the only acceleration due to the turning about the center of the circle

$$m\vec{r} = \vec{S} - mg\vec{k} = +S \sin \theta \vec{i}_N + S \cos \theta \vec{k} - mg\vec{k}$$

$$\begin{aligned} \text{and } \frac{mv_0^2}{\rho} &= S \sin \theta \\ mg &= S \cos \theta \end{aligned}$$

$$\left. \begin{aligned} \frac{mv_0^2}{\rho} &= S \sin \theta \\ mg &= S \cos \theta \end{aligned} \right\} \Rightarrow S = m(g^2 + \frac{v_0^4}{\rho^2})^{1/2}; \tan \theta = \frac{v_0^2}{\rho g}$$

5.5

$$b\vec{i}_r = \vec{r}$$

$$\vec{\omega} = \frac{v_0}{b} \vec{k}$$

$$\frac{d\vec{r}}{dt} = \dot{r} \vec{i}_r + r\dot{\theta} \vec{i}_\theta \quad \frac{d^2\vec{r}}{dt^2} = (\ddot{r} - r\dot{\theta}^2) \vec{i}_r + (2\dot{r}\dot{\theta} + r\ddot{\theta}) \vec{i}_\theta$$

from  $\frac{d^2\vec{r}}{dt^2}$  we get  $-b\omega^2 \vec{i}_r$  from  $\frac{d\vec{r}}{dt}$  we get  $b\omega \vec{i}_\theta$

$\vec{\omega} \times \vec{r}$  gives  $v \vec{i}_\theta$ ;  $\vec{a} \times (\vec{\omega} \times \vec{r})$  gives  $-\frac{v^2}{b} \vec{i}_r$ ;  $2\vec{\omega} \times \frac{d\vec{r}}{dt}$  gives  $-2\omega v \vec{i}_r$

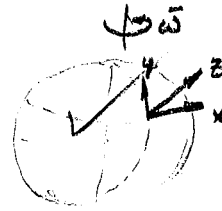
$$\therefore \vec{a} = -\vec{i}_r \left[ b\omega^2 + 2\omega v + \frac{v^2}{b} \right] \quad \text{and} \quad \vec{F} = m\vec{a}$$

if  $v = b\omega$   $\vec{a} = -\vec{i}_r [b\omega^2 + 2\omega^2 b + b\omega^2] = -\vec{i}_r [4\omega^2 b]$   
if  $v = -b\omega$   $\vec{a} = -\vec{i}_r [b\omega^2 - 2\omega^2 b + b\omega^2] = \vec{0}$

(10)

5.7.

$$\vec{a}_{\text{cor}} = -2\vec{\omega} \times \vec{r} = -2 \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ 0 & \omega \sin \lambda & \omega \cos \lambda \\ 0 & 350 \text{ mph} & 0 \end{vmatrix}$$



$$= -2 \left( -\hat{i} \left[ 350 \times \frac{88 \text{ fps}}{60 \text{ mph}} \right] \omega \sin \lambda \right) = \hat{i} \left\{ 1027 \times \frac{\sqrt{2}}{2} (7.3 \times 10^{-5}) \right\}$$

$$\vec{F} = m a \vec{i} = \hat{i} \left\{ \frac{4000}{32.2} (1.027) (.707) (7.3) \right\} = 6.57 \text{ lb east.}$$

10

4.1

$$\vec{F} = cyz\vec{i} + czx\vec{j} + cxy\vec{k}$$

$$\nabla \times \vec{F} = \begin{vmatrix} \vec{i} & \vec{j} & \vec{k} \\ \partial/\partial x & \partial/\partial y & \partial/\partial z \\ cyz & czx & cxy \end{vmatrix}$$

$$= \vec{i}[cx - cx] + \vec{j}[cy - cy] + \vec{k}[cz - cz] = \vec{0}$$

Conservative

$$\vec{F} = cyz\vec{i} + cxy\vec{j} + czx\vec{k}$$

$$\nabla \times \vec{F} = \begin{vmatrix} \vec{i} & \vec{j} & \vec{k} \\ \partial/\partial x & \partial/\partial y & \partial/\partial z \\ cyz & cxy & czx \end{vmatrix}$$

$$= \vec{i}[0 - 0] + \vec{j}[cy - cz] + \vec{k}[cy - cz] \neq \vec{0}$$

non-conservative

$$\vec{F} = cy/z\vec{i} + cx/z\vec{j} + \frac{cxy}{z^2}\vec{k}$$

$$\nabla \times \vec{F} = \begin{vmatrix} \vec{i} & \vec{j} & \vec{k} \\ \partial/\partial x & \partial/\partial y & \partial/\partial z \\ cy/z & cx/z & -\frac{cxy}{z^2} \end{vmatrix}$$

$$= \vec{i}\left[-\frac{cx}{z^2} - \left[-\frac{cx}{z^2}\right]\right] + \vec{j}\left[-\frac{cy}{z^2} - \left[-\frac{cy}{z^2}\right]\right] + \vec{k}\left[\frac{c}{z} - \frac{c}{z}\right] = \vec{0}$$

Conservative

4.3

Given:

$$V = ax + by^2 + cz^3, \quad \text{particle m mass, at } (x, y, z) = (0, 0, 0) \quad v = v_0$$

Find:

$v$  when  $(x, y, z) = (1, 1, 1)$  if it passes through it.

$$\vec{F} = -\nabla V = -a\vec{i} - 2by\vec{j} - 3cz^2\vec{k}$$

to pass through  $(1, 1, 1) \quad \vec{F} \neq \vec{F}(t) \quad \text{or} \quad \vec{F} = \vec{F}(x, y, z) \quad \text{or} \quad \nabla \times \vec{F} = \vec{0}$

$$\nabla \times \vec{F} = \begin{vmatrix} \vec{i} & \vec{j} & \vec{k} \\ \partial/\partial x & \partial/\partial y & \partial/\partial z \\ -a & -2by & -3cz^2 \end{vmatrix} = \vec{0}$$

$\therefore \vec{F}$  is conservative

$$\therefore \vec{F} = \vec{F}(x, y, z)$$

we can then use  $T + V = E \Rightarrow \frac{1}{2}mv_0^2 = \frac{1}{2}mv_*^2 + (a + b + c)$

or

$$v_* = \sqrt{v_0^2 - \frac{2(a+b+c)}{m}}$$

4.5

$$\vec{F}_1 = y\vec{i} + x\vec{j} ; \quad \vec{F}_2 = y\vec{i} - x\vec{j}$$

$$\nabla \times \vec{F}_1 = \begin{vmatrix} \vec{i} & \vec{j} & \vec{k} \\ \partial/\partial x & \partial/\partial y & \partial/\partial z \\ y & x & 0 \end{vmatrix} = \vec{k}(1-1) = \vec{0} \quad \text{Conservative}$$

$$\nabla \times \vec{F}_2 = \begin{vmatrix} \vec{i} & \vec{j} & \vec{k} \\ \partial/\partial x & \partial/\partial y & \partial/\partial z \\ y & -x & 0 \end{vmatrix} = \vec{k}(-1-1) = -2\vec{k} \neq \vec{0} \quad \text{non conservative,}$$

$$\textcircled{a} \quad \int \vec{F}_1 \cdot d\vec{r} = \int (F_x dx + F_y dy) = \int (y dx + x dy)$$

$$\text{if } x=y$$

$$\int_0^1 x dx + \int_0^1 y dy = 1 \quad \checkmark$$

$$\text{if } x=c=0 \quad \text{to } (0,1)$$

$$\text{then } y=c=1 \quad \text{to } (1,1)$$

$$\int_0^1 dx = 1 \quad (\text{the first integral from } 0,0 \text{ to } 0,1 \text{ is } 0)$$

$$\textcircled{b} \quad \int \vec{F}_2 \cdot d\vec{r} = \int (y dx - x dy)$$

$$\text{if } x=y$$

$$\int_0^1 x dx - \int_0^1 y dy = 0$$

$$\text{if } x=c=0 \quad (0,0) \text{ to } (0,1)$$

$$y=c=1 \quad (0,1) \text{ to } (1,1)$$

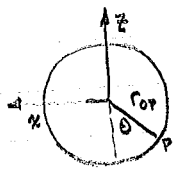
$$\int_0^1 dx = 1$$

$$\text{as you can see } \int \vec{F}_1 \cdot d\vec{r} = 1 \quad \text{both ways}$$

$$\text{but } \int \vec{F}_2 \cdot d\vec{r} \text{ is not.}$$

(10)

4.9.



$$\vec{r}_{Op} = -b \sin \theta \vec{i} - b \cos \theta \vec{j}$$

$$\vec{v}_{rel} = -V_0 \cos \theta \vec{i} + V_0 \sin \theta \vec{j}$$

$$b \frac{d\theta}{dt} = b\omega = V_0$$

$$\vec{v} = V_0(1 - \cos \theta) \vec{i} + \vec{j} V_0 \sin \theta$$

$$v^2 = 2V_0^2(1 - \cos \theta)$$

$v$  at any pt  $p$  with respect to the ground

for this velocity and taking datum line at center of wheel:

$$z = -b \cos \theta$$

$$\therefore mV_0^2(1 - \cos \theta) - mgb \cos \theta = \text{Constant.}$$

at highest point in the trajectory:

$$\vec{v} = V_0(1 - \cos \theta) \vec{i} \quad \text{only} \quad \text{and} \quad z = z_{rel}^* \quad z_{rel}^* = \text{relative height wrt datum line}$$

thus,

$$mV_0^2(1 - \cos \theta) - mgb \cos \theta = \frac{mV_0^2}{2}(1 - \cos \theta)^2 + mgz_{rel}^* \quad (1)$$

$$\text{take } \frac{dz_{rel}^*}{d\theta} = 0 = V_0^2 \sin \theta + gb \sin \theta = V_0^2 (\sin \theta - \sin \theta \cos \theta)$$

$$gb \sin \theta = -V_0^2 \sin \theta \cos \theta$$

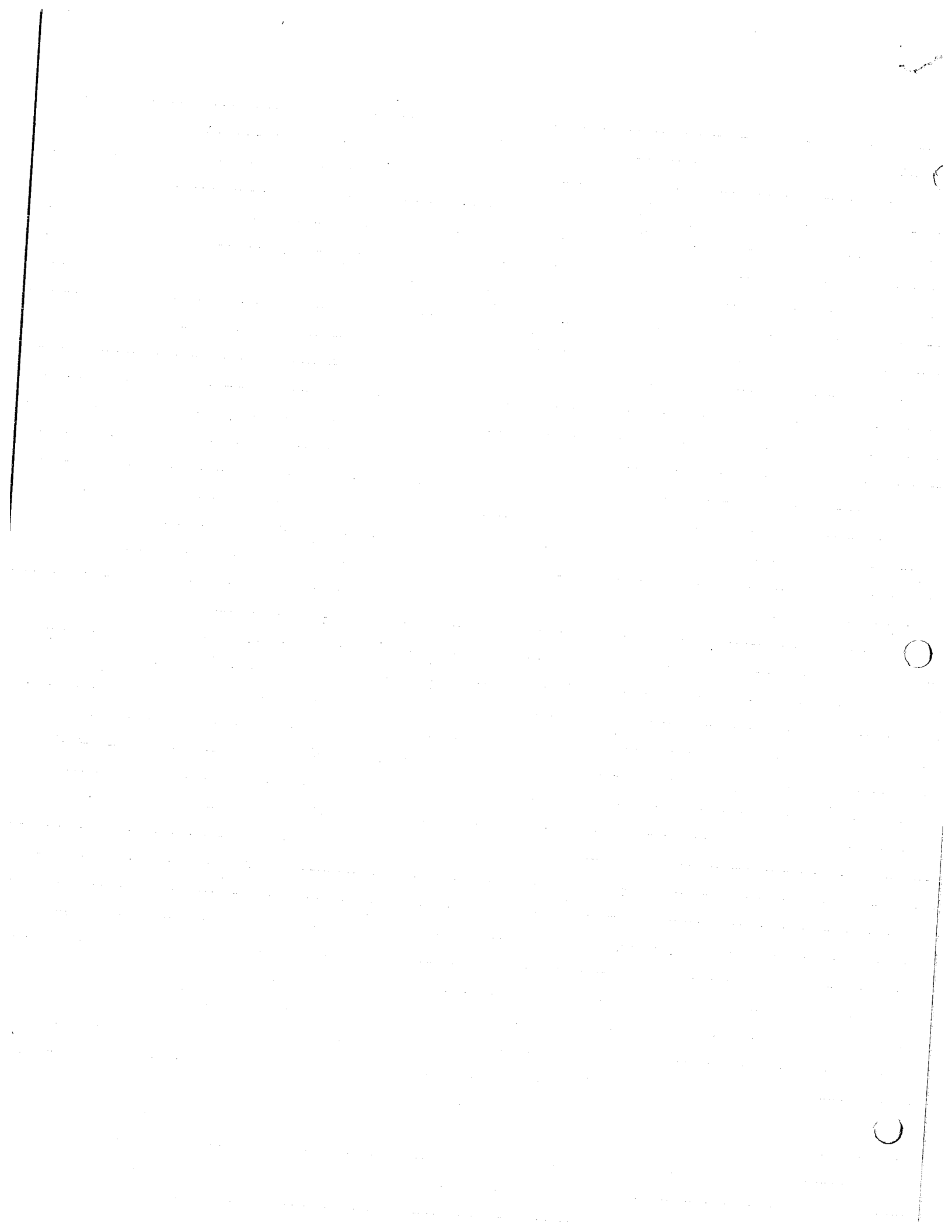
$$\cos \theta = -\frac{gb}{V_0^2}$$

Substitute the following into the equat (1) we finally get:

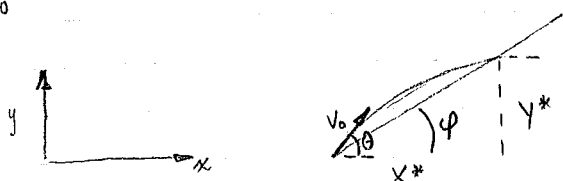
$$\therefore z_{rel}^* = \frac{V_0^2}{2g} + \frac{gb^2}{2V_0^2}; \quad z = z_{rel}^* + b$$

$$z = b + \frac{V_0^2}{2g} + \frac{gb^2}{2V_0^2}$$

10







$$x = v_0 \cos \theta t \quad y = v_0 \sin \theta t - \frac{1}{2} g t^2$$

$$\text{at } t = t^* \quad x = x^* \quad y = y^* \quad R = \sqrt{x^{*2} + y^{*2}}$$

$$\tan \varphi = \frac{y^*}{x^*} \quad x^* = v_0 \cos \theta t^*; \quad y^* = v_0 \sin \theta t^* - \frac{1}{2} g t^{*2}$$

$$y^* = x^* \tan \varphi = v_0 \cos \theta \tan \varphi t^* = v_0 \sin \theta t^* - \frac{1}{2} g t^{*2}$$

$$\text{or } t^* = \frac{2v_0}{g} (\sin \theta - \cos \theta \tan \varphi)$$

$$x^* = v_0 \cos \theta \left[ \frac{2v_0}{g} (\sin \theta - \cos \theta \tan \varphi) \right]$$

$$y^* = v_0 \sin \theta \left[ \frac{2v_0}{g} (\sin \theta - \cos \theta \tan \varphi) \right] - \frac{g}{2} \left[ \frac{2v_0}{g} (\sin \theta - \cos \theta \tan \varphi) \right]^2$$

$$y^* = \frac{2v_0^2}{g} [\sin \theta \cos \theta \tan \varphi - \cos^2 \theta \tan^2 \varphi]$$

$$\begin{aligned} R^2 = x^{*2} + y^{*2} &= \frac{4v_0^4}{g^2} \cos^2 \theta [\sin^2 \theta - \sin 2\theta \tan \varphi + \tan^2 \varphi + \cos^2 \theta \tan^4 \varphi - \sin 2\theta \tan^3 \varphi] \\ &= \frac{4v_0^4}{g^2} \frac{\cos^2 \theta}{\cos^4 \varphi} [\sin^2 \theta \cos^4 \varphi - \sin 2\theta \sin \varphi \cos \varphi + \sin^2 \varphi \cos^2 \varphi + \cos^2 \theta \sin^4 \varphi] \\ &= \frac{4v_0^4}{g^2} \frac{\cos^2 \theta}{\cos^4 \varphi} [\sin^4 \varphi - \sin^4 \varphi \sin^2 \theta + \sin^2 \varphi \cos^2 \varphi + \sin^2 \theta \cos^4 \varphi - \sin 2\theta \sin \varphi \cos \varphi] \\ &= \frac{4v_0^4}{g^2} \frac{\cos^2 \theta}{\cos^4 \varphi} [\sin^2 \varphi \cos^2 \theta + \sin^2 \theta \cos^2 \varphi - 2 \sin \theta \cos \theta \sin \varphi \cos \varphi] \end{aligned}$$

$$R = \frac{2v_0^2}{g} \frac{\cos \theta}{\cos^2 \varphi} [\sin(\theta - \varphi)]$$

QED.

10

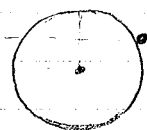
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4.17



$$\frac{1}{2} m v^2 + m g z = E$$

$$\text{when } z = b/2 \quad v = 0 \Rightarrow m g b/2 = \frac{1}{2} m v^2 + m g z$$

$$\text{or } v^2 = g(b - 2z) \quad (1)$$

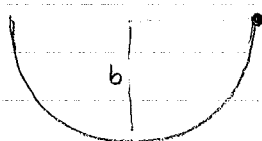
$$\text{but } m g \cos \theta = \frac{m v^2}{b} \quad \text{but } \cos \theta = \frac{z}{b} \quad (2)$$

$$\therefore (1) \text{ into } (2) \text{ gives } g \frac{z}{b} = g(b - 2z) \cdot \frac{1}{b}$$

$$\text{or } z = b - 2z \Rightarrow z = b/3 \quad \checkmark$$

10

4.19



$$E = \frac{1}{2} m v^2 + m g z \quad \checkmark$$

$$\text{when } v = 0 \quad z = b$$

$$E = m g b$$

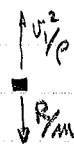
$$\text{when } z = 0 \quad v = v_1$$

$$\therefore m g b = \frac{1}{2} m v_1^2$$

$$v_1 = \sqrt{2 g b}$$

$$-\frac{m v_1^2}{b} = +m g + R$$

$$R = -\frac{1}{3} m g$$



10

4.21

$$T_{\text{ELEM}} = 2\pi \sqrt{\frac{L}{g}}$$

$$T_{\text{NEW}} = 2\pi \sqrt{\frac{L}{g}} \left( 1 + \frac{\theta_0^2}{16} + \dots \right) = T_{\text{ELEM}} \left( 1 + \frac{\theta_0^2}{16} + \dots \right) \quad \checkmark$$

$$\text{if } \theta_0 = 30^\circ = \frac{\pi}{6} \text{ rad.}$$

$$1 + \frac{\theta_0^2}{16} = 1 + \frac{\pi^2}{36 \cdot 16} = 1.01715$$

Error incurred is 1.715% ;  $T_{\text{ELEM}}$  is too small by 1.715%

10



Cesar Henry  
AE 211

1.  $r_L = 29960$  miles  $r_S = 43600$  miles

$$\frac{V_L^2}{2} - \frac{\mu}{r_L} = \frac{V_S^2}{2} - \frac{\mu}{r_S} ; r_L V_L = r_S V_S$$

$$\frac{1}{2} \left( \frac{r_S V_S}{r_L} \right)^2 - \frac{V_S^2}{2} = \mu \left[ \frac{1}{r_L} - \frac{1}{r_S} \right]$$

$$V_S = \sqrt{\frac{2\mu \left[ \frac{1}{r_L} - \frac{1}{r_S} \right]}{\left[ \left( \frac{r_S}{r_L} \right)^2 - 1 \right]}} ; \frac{r_S}{r_L} = .1455$$

a)  $V_S = 32650$  ft/sec

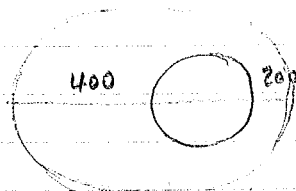
b)  $V_L = \frac{r_S V_S}{r_L} = .1455 (32650) = 4750$  ft/sec

2.

$$V_{e0} = V_e \sqrt{\frac{R}{r_0}}$$

$$V_{e0} = \sqrt{2} V_{e0}$$

$$\therefore V_{e0} = V_e \sqrt{\frac{R}{2r_0}} = 36700 \sqrt{\frac{3960}{8720}} = .674 (36700) = 24700 \text{ ft/sec}$$



$$a = 4260 \text{ miles}$$

$$V = \sqrt{\mu \left[ \frac{2}{r_0} - \frac{1}{a} \right]} \text{ where } r_0 = 4360 \text{ miles}$$

$$V = \sqrt{(1.408 \times 10^6) \left[ \frac{2}{4360 \times 5280} - \frac{1}{4260 \times 5280} \right]}$$

$$V = 24400 \text{ ft/sec}$$

$$\epsilon = \frac{24700 - 24400}{24700} \times 100 = 1.215 \%$$

3.  $h = r_0 v_0 \sin \phi_0$  ✓ where  $r_0 = 5460 \text{ miles}$ ,  $v_0 = 26700 \text{ ft/sec}$ ,  $\phi_0 = 76^\circ$

$$h = 7.47 \times 10^{11} \text{ ft}^2/\text{sec}$$

$$E = \frac{v_0^2}{2} - \frac{\mu}{r_0} = \frac{(26700)^2}{2} - \frac{1.408 \times 10^{16}}{5460 \times 5280} = -1.315 \times 10^8$$

$$e = \sqrt{1 + \frac{2 E h^2}{\mu^2}} = .511 \quad \checkmark$$

at  $\theta = 0$   $\cos \theta_0 = \frac{1}{e} \left[ \frac{h^2}{r \mu} - 1 \right]$

$$\cos \theta_0 = .73 \quad \theta_0 = 43.0^\circ$$

$$u = \frac{\mu}{h^2} [1 + e \cos(\theta - \theta_0)] \quad \checkmark \quad \theta - \theta_0 = 0, 180^\circ$$

$$\therefore \frac{1}{r_{\text{LARGE}}} = \frac{\mu}{h^2} [1 - e] \quad \checkmark \quad r_{\text{LARGE}} = 15350 \text{ miles} \quad h_t = 11390 \text{ miles}$$

$$\therefore \frac{1}{r_{\text{SMALL}}} = \frac{\mu}{h^2} [1 + e] \quad \checkmark \quad r_{\text{SMALL}} = 4980 \text{ miles} \quad h_t = 1020 \text{ miles}$$

(10)

1.

$$\bar{r} = \frac{\sum (i+j) + (j+k) + k}{3} = \frac{i}{3} + \frac{2j}{3} + \frac{2k}{3}$$

$$\bar{v} = \frac{\sum (2i) + j + (i+j+k)}{3} = i + \frac{2j}{3} + \frac{k}{3}$$

$$\bar{p} = \sum m_i \bar{v}_i = 3i + 2j + k$$

10

2.

$$v_0 = v_B - v_g$$

$$-v_g = v_0 - v_B$$

$$m v_B = -M v_g$$

$$-M v_g = m v_0 - m v_B$$

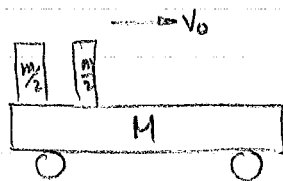
$$m v_B + M v_B = m v_0$$

$$v_B = \frac{v_0}{(1 + \frac{m}{M})}$$

10







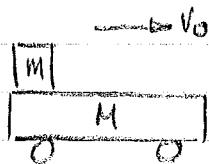
$$(M+m)v_0 = (M+m/2)(v_0 + \Delta v_1) + m/2(v_0 + \Delta v_1 - u)$$

$$\Delta v_1 = \frac{mu}{2(M+m)}$$

$$(M+m/2)(v_0 + \Delta v_1) = M(v_0 + \Delta v_1 + \Delta v_2) + m/2(v_0 + \Delta v_1 + \Delta v_2 - u)$$

$$\Delta v_2 = \frac{mu}{2(M+m/2)}$$

$$\Delta v_T = \Delta v_1 + \Delta v_2 = \frac{mu}{2M+2m} + \frac{mu}{2M+m}$$



$$(M+m)v_0 = M(v_0 + \Delta v) + m(v_0 + \Delta v - u)$$

$$\Delta v = \frac{mu}{M+m}$$

Assume

$$\Delta v \geq \Delta v_T$$

$$\frac{2mu}{2m+2M} \geq \frac{mu}{2M+2m} + \frac{mu}{2M+m}$$

$$\frac{mu}{2m+2M} > \frac{mu}{2M+m}$$

but this is not true since  $2M+m \leq 2m+2M$

$$\therefore \Delta v_T \geq \Delta v$$

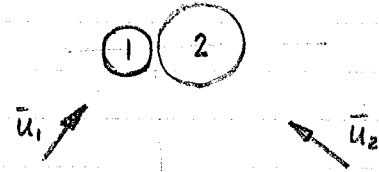
10



1.  $e = .5$   $m_1 = 1$   $m_2 = 10$

$\vec{u}_1 = 10\vec{i} + 10\vec{j}$   $\vec{u}_2 = -20\vec{i} + 15\vec{j}$

In y direction, it was proven that  
 $u_{1y} = u'_{1y} = 10$   
 and  $u_{2y} = u'_{2y} = 15$



since  $e = \frac{u_{2x} - u'_{1x}}{u_{1x} - u_{2x}} = .5$  we obtain  $u_{2x} - u'_{1x} = 15$

solving for  $u'_{1x}$  we obtain  $u'_{1x} = u_{2x} - 15$

Substituting into the equation obtained from entire system in x direction  
 $m_1 u_{1x} + m_2 u_{2x} = m_1 u'_{1x} + m_2 u'_{2x}$  we obtain

$m_1 u_{1x} + m_2 u_{2x} = m_1 (u_{2x} - 15) + m_2 u'_{2x}$  ; solving for  $u'_{2x}$

$$\frac{m_1 u_{1x} + m_2 u_{2x} + m_1 \cdot 15}{m_1 + m_2} = \frac{1(10) + 10(-20) + 15}{11} = \frac{-175}{11} = -15.91$$

since  $\hat{P}$  is the impulsive force for particle 2, we can write  
 $m_2 u_{2x} + \hat{P} = m_2 u'_{2x}$  ; solving for  $\hat{P}$  we obtain

$$\hat{P} = m_2 (u'_{2x} - u_{2x}) = 10 (-15.91 + 20) = 40.9$$

since we can also write an equation for  $u'_{1x}$  as a function of  $m_1, u_{1x}, \hat{P}$

$$u'_{1x} = u_{1x} - \frac{\hat{P}}{m_1} = 10 - 40.9 = -30.9$$

$\therefore$

$$\vec{u}'_1 = -30.9\vec{i} + 10\vec{j} \quad \vec{u}'_2 = -15.91\vec{i} + 15\vec{j}$$

2.  $T = \frac{1}{2} m_1 (u_c + u_1)^2 + \frac{1}{2} m_2 (u_c + u_2)^2$

$T' = \frac{1}{2} m_1 (u_c + u'_1)^2 + \frac{1}{2} m_2 (u_c + u'_2)^2$

$$T - T' = \frac{1}{2} m_1 (2u_c u_1 + u_1^2 - 2u_c u'_1 - u_1'^2) + \frac{1}{2} m_2 (2u_c u_2 + u_2^2 - 2u_c u'_2 - u_2'^2)$$

$$T - T' = \frac{1}{2} m_1 v_1^2 + \frac{1}{2} m_2 v_2^2 + \hat{Q}$$

from momentum  $m_1 u_1 + m_2 u_2 = (m_1 + m_2) v_c$  (3)  
 $m_1 u_1' + m_2 u_2' = (m_1 + m_2) v_c$  (4)

where  $u_1 = v_1 + v_c$   $u_2 = v_2 + v_c$   $u_1' = v_1' + v_c$   $u_2' = v_2' + v_c$

$\hat{Q}$  can be evaluated as  $-\frac{1}{2} m_1 v_1'^2 - \frac{1}{2} m_2 v_2'^2$

$$\therefore T - T' = \frac{1}{2} m_1 (v_1^2 - v_1'^2) + \frac{1}{2} m_2 (v_2^2 - v_2'^2) \quad (5)$$

from eq (3) and (4)

$$m_1 v_1 = -m_2 v_2 \quad (6)$$

$$m_1 v_1' = -m_2 v_2' \quad (6)$$

from these we can get the following

$$\frac{v_1}{v_1'} = \frac{v_2}{v_2'} \quad (7) \Rightarrow v_1 = \frac{v_1'}{v_2'} v_2$$

putting them into the equation for coefficient of Restitution

$$e = \frac{v_1' - v_2'}{v_2 - v_1} \quad (8) = \frac{v_1' - v_2'}{\frac{v_2}{v_2'} (v_2' - v_1')} = -\frac{v_2'}{v_2}$$

$$\therefore e = -\frac{v_2'}{v_2} \rightarrow \boxed{-\frac{1}{e} = \frac{v_2}{v_2'} = \frac{v_1}{v_1'}} \quad \checkmark$$

$\therefore -v_2 e = v_2'$  &  $-v_1 e = v_1'$  squaring & putting into (5) gives

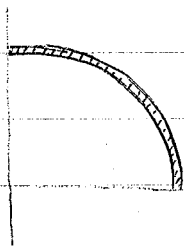
$$T - T' = \frac{1}{2} m_1 v_1^2 (1 - e^2) + \frac{1}{2} m_2 v_2^2 (1 - e^2)$$

Q.E.D.

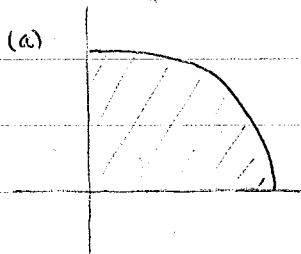
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8.1

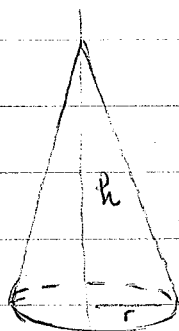
(b)



(a)



(c)



for (a)

$$\bar{x} = \frac{\int p x ds}{\int p ds} \quad \checkmark \quad \text{since } x = r \cos \theta \text{ and } ds = r dr d\theta$$

and  $p = \text{constant}$

$$\bar{x} = \frac{\int \int r^2 \cos \theta dr d\theta}{\int \int r dr d\theta} = \frac{\int_0^a r^2 dr \int_0^{\pi/2} \cos \theta d\theta}{\int_0^a r dr \int_0^{\pi/2} d\theta} = \frac{a^3/3}{\frac{\pi a^2}{4}}$$

$$\bar{x} = \frac{4a}{3\pi} \quad \checkmark$$

since  $y = r \sin \theta$  &  $ds = r dr d\theta$

$$\bar{y} = \frac{\int p y ds}{\int p ds} = \frac{\int_0^a r^2 dr \int_0^{\pi/2} \sin \theta d\theta}{\int_0^a r dr \int_0^{\pi/2} \frac{\pi a}{4} d\theta} = \frac{a^3/3}{\frac{\pi a^2}{4}}$$

$$\bar{y} = \frac{4a}{3\pi} \quad \checkmark$$

(b)  $\bar{x} = \frac{\int x p dl}{\int p dl}$  ✓ since  $p = \text{constant}$  and  $dl = a d\theta$

$$\bar{x} = \frac{\int_0^{\pi/2} a^2 \cos \theta d\theta}{\int_0^{\pi/2} a d\theta} = \frac{a^2 \cdot 1}{\frac{a\pi}{2}} = \frac{2a}{\pi} \checkmark$$

$$\bar{y} = \frac{\int_0^{\pi/2} a^2 \sin \theta d\theta}{\int_0^{\pi/2} a d\theta} = \frac{\int p y dl}{\int p dl} \quad (10)$$

$$= \frac{-a^2 \cos \theta \Big|_0^{\pi/2}}{a\theta \Big|_0^{\pi/2}} = \frac{a^2}{\frac{a\pi}{2}} = \frac{2a}{\pi} \checkmark$$

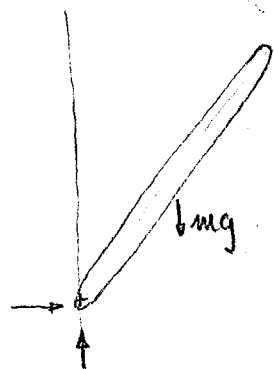
(c)  $\bar{x} = \frac{\int p x dV}{\int p dV}$   $dV = \pi r^2 dx$   $r = a \left[ -\frac{x}{h} + 1 \right]$  ✓  
 $p = \text{const.}$

$$\bar{x} = \frac{a^2 \pi \int \left[ \frac{x}{h} - 1 \right]^2 x dx}{a^2 \pi \int \left[ \frac{x}{h} - 1 \right]^2 dx} = \frac{\frac{x^4}{4h^2} - \frac{2x^3}{3h} + \frac{x^2}{2} \Big|_0^h}{\frac{x^3}{3h^2} - \frac{x^2}{h} + x \Big|_0^h} = \frac{\frac{h^2}{12}}{\frac{h}{3}} = \frac{h}{4}$$

$$\bar{x} = h/4 \checkmark$$

(10)

1.

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$$f = m\ddot{x}_{cm}$$

$$N - mg = m\ddot{y}_{cm}$$

$$I_0 \ddot{\theta} = mg \frac{l}{2} \sin \theta$$

$$mg \frac{l}{2} = \frac{1}{2} I_0 \dot{\theta}^2 + mg \frac{l}{2} \cos \theta \Rightarrow \dot{\theta}^2 = \frac{mgl(1 - \cos \theta)}{I_0} = \frac{3g}{l}(1 - \cos \theta)$$

$$\text{since } y_{cm} = \frac{l}{2} \cos \theta \quad ; \quad \dot{y}_{cm} = \frac{l}{2} (-\sin \theta \dot{\theta})$$

$$x_{cm} = \frac{l}{2} \sin \theta \quad \dot{x}_{cm} = \frac{l}{2} (\cos \theta \dot{\theta})$$

$$\text{this leads to } \ddot{y}_{cm} = \frac{l}{2} (-\sin \theta \ddot{\theta} - \cos \theta \dot{\theta}^2)$$

$$\ddot{x}_{cm} = \frac{l}{2} [\cos \theta \ddot{\theta} - \dot{\theta}^2 \sin \theta]$$

thus

$$\ddot{y}_{cm} = -\frac{l}{2} \left[ \sin \theta \frac{3mgl \sin \theta}{2ml^2} + 2 \cos \theta \frac{3g}{2l} (1 - \cos \theta) \right]$$

$$= -\frac{3}{4} [g \sin^2 \theta - g(2 \cos^2 \theta - 2 \cos \theta)] = +\frac{3}{4} g [(3 \cos^2 \theta - 1) - 2 \cos \theta]$$

$$N = mg + m\ddot{y}_{cm} = \frac{1}{4} mg (3 \cos \theta - 1)^2$$

$$f = m \frac{l}{2} \left[ \cos \theta \cdot \frac{3mgl \sin \theta}{2ml^2} - \frac{2 \cdot 3g}{2l} (1 - \cos \theta) \sin \theta \right]$$

$$= \frac{3}{4} mg \sin \theta [\cos \theta - 2 + 2 \cos \theta] = \frac{3}{4} mg \sin \theta [3 \cos \theta - 2]$$

for slipping  $f = \mu N$   $\therefore$ 

$$\frac{3}{4} mg \sin \theta [3 \cos \theta - 2] = \mu \frac{1}{4} mg (3 \cos \theta - 1)^2$$

$$3 \sin \theta [3 \cos \theta - 2] = \mu (3 \cos \theta - 1)^2$$

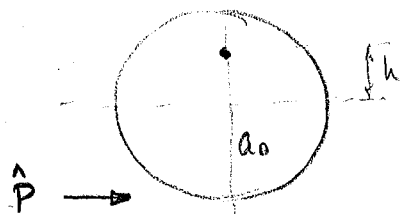
$$\mu = \frac{3 \sin \theta [3 \cos \theta - 2]}{(3 \cos \theta - 1)^2}$$

for slipping to left since denom.  $> 0$   
and since  $0 \leq \theta \leq \frac{\pi}{2}$

$$3 \cos \theta - 2 > 0 \quad \text{or} \quad \theta > \arccos \frac{2}{3}$$

(10)

2.



$$0 + \hat{P} = m v_c = m \omega h$$

$$I_o \omega = \hat{P} (a_0 + h)$$

center of percussion

$$I_o = \frac{m a_0^2}{2} + m h^2 \quad \therefore$$

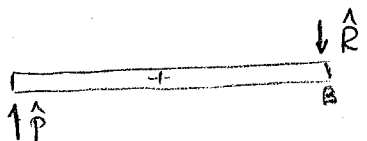
$$m \left( \frac{a_0^2}{2} + h^2 \right) \omega = \hat{P} (a_0 + h) = m \omega h (a_0 + h)$$

$$\frac{a_0^2}{2} = a_0 h$$

$$h = \frac{a_0}{2}$$

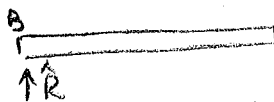
(10)

3.



$$(\hat{P} + \hat{R}) \frac{l}{2} = I_c \dot{\theta}_1$$

$$\hat{P} - \hat{R} = m v_{c1}$$



$$\frac{l}{2} \hat{R} = I_c \dot{\theta}_2$$

$$\hat{R} = m v_{c2}$$

$$v_B = v_{c1} - \frac{l}{2} \dot{\theta}_1 = v_{c2} + \frac{l}{2} \dot{\theta}_2$$

$$\hat{P} = m(v_1 + v_2)$$

$$\hat{P} = \frac{2 I_c}{l} (\dot{\theta}_1 - \dot{\theta}_2) = \frac{m l}{6} (\dot{\theta}_1 - \dot{\theta}_2)$$

(9)

$$v_{c2} + v_{c1} = 2 v_{c2} + \frac{l}{2} (\dot{\theta}_2 + \dot{\theta}_1) = \frac{2 m l^2}{12 l m} \dot{\theta}_2 + \frac{l}{2} (\dot{\theta}_2 + \dot{\theta}_1)$$

$$= \frac{5}{6} l \dot{\theta}_2 + \frac{l}{2} \dot{\theta}_1$$

$$\hat{P} = \frac{m l}{6} [5 \dot{\theta}_2 + 3 \dot{\theta}_1]$$

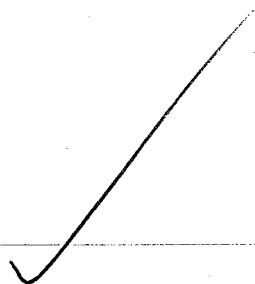
$$\hat{P} = \frac{m l}{6} (\dot{\theta}_1 - \dot{\theta}_2)$$

$$\Rightarrow \dot{\theta}_1 = \frac{3}{4} \frac{\hat{P}}{m l} \quad \dot{\theta}_2 = -\frac{3}{2} \frac{\hat{P}}{m l}$$

$$v_2 = \frac{l}{6} \dot{\theta}_2 = -\frac{\hat{P}}{4 m} \quad v_1 = \frac{5}{4} \frac{\hat{P}}{m}$$

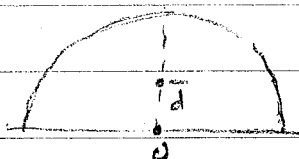
$$v_B = v_{c2} + \frac{l}{2} \dot{\theta}_2 = -\frac{\hat{P}}{4 m} - \frac{3 \hat{P}}{4 m} = -\frac{\hat{P}}{m}$$





Aravind  
AE 211

8.13.



$$d = \frac{\rho \int_0^a r^2 dr \int_0^\pi \sin \theta d\theta}{\rho \int_0^a r dr \int_0^\pi d\theta} = \frac{4a}{3\pi}$$

$$I_{cm} = I_o - Ad^2$$

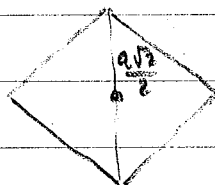
$$\rho Ad^2 = \rho \pi \frac{a^2}{2} \cdot \frac{16a^2}{9\pi^2} = \frac{\rho 16a^4}{18\pi} = \frac{\rho 8a^4}{9\pi}$$

$$I_o = \rho \int r^2 \cdot r dr d\theta = \rho \cdot \frac{\pi a^4}{4}$$

$$I_{cm} = \rho \frac{\pi a^2}{2} \left[ \frac{a^2}{2} - \frac{16a^2}{9\pi^2} \right] = m a^2 \left[ \frac{1}{2} - \left( \frac{4}{3\pi} \right)^2 \right]$$

where  $m = \rho A$

8.15a



$$-mg \frac{a\sqrt{2}}{2} \sin \theta = m k^2 \ddot{\theta} \Rightarrow$$

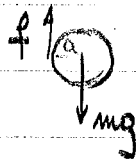
$$T = 2\pi \sqrt{\frac{2k^2}{ga\sqrt{2}}}$$

$$k^2 = k_{cm}^2 + l^2 = \frac{a^2}{6} + \frac{a^2}{2} = \frac{2a^2}{3}$$

$$T = 2\pi \sqrt{\frac{2a}{3g}} \sqrt{2}$$

$$\frac{a\sqrt{2}}{2} \cdot l = k_{cm}^2 = \frac{a^2}{6} \quad l = \frac{a\sqrt{2}}{6}$$

8.17



$$mg - f = m \ddot{y}_c$$

$$f \cdot a = I_c \ddot{\theta} = \frac{2}{5} m a^2 \ddot{\theta}$$

$$f = \frac{2}{5} a m \ddot{\theta}$$

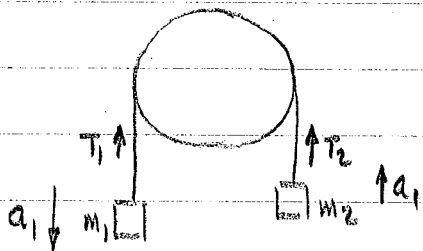
$$mg - \frac{2}{5} a \ddot{\theta} = m \ddot{y}_c$$

$$\ddot{y}_c = a \ddot{\theta}$$

$$mg - \frac{2}{5} m \ddot{y}_c = m \ddot{y}_c$$

$$\ddot{y}_c = \frac{5}{7} g$$

8.19



$$m_1 g - T_1 = m_1 a_1$$

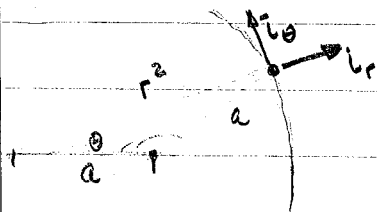
$$T_2 - m_2 g = m_2 a_1$$

$$(T_1 - T_2) a = I \ddot{\theta} = I a_1 / a$$

$$T_2 - T_1 = (m_1 + m_2) a_1 = g(m_1 - m_2)$$

$$- \frac{I}{a^2} a_1 - (m_1 + m_2) a_1 = -g(m_1 - m_2)$$

$$a_1 = g(m_1 - m_2) / (m_1 + m_2 + I/a^2)$$



$$\vec{v} = \dot{r} \hat{r} + r \dot{\theta} \hat{\theta}$$

$$\vec{a} = (\ddot{r} - r \dot{\theta}^2) \hat{r} + (r \ddot{\theta} + 2 \dot{r} \dot{\theta}) \hat{\theta}$$

$$\dot{\theta} = c$$

And you would have had much easier time.

$$r^2 = 2a^2 + 2a^2 \cos(2\theta) = 2a^2 [1 + \cos 2\theta] = 4a^2 \cos^2 \theta$$

$$2r \dot{r} = -2a^2 \sin 2\theta (2\dot{\theta}) = -4a^2 \dot{\theta} \sin 2\theta$$

$$r \dot{r} = -2a^2 \dot{\theta} \sin 2\theta$$

$$\dot{r} = -\frac{2a^2 \dot{\theta} \sin 2\theta}{r}, \quad \ddot{r} = -\frac{2a^2 \ddot{\theta} \sin 2\theta}{r} - \frac{2a^2 \dot{\theta}^2 \cos 2\theta}{r}$$

$$\text{since } \dot{\theta} = c, \quad \ddot{\theta} = 0 \quad \therefore$$

$$\vec{a} = (\ddot{r} - r \dot{\theta}^2) \hat{r} + (2 \dot{r} \dot{\theta}) \hat{\theta}$$

$$\text{since } r \dot{r} = -2a^2 \dot{\theta} \sin 2\theta$$

$$\dot{r} \dot{r} + r \ddot{r} = -4a^2 \dot{\theta}^2 \cos 2\theta$$

$$\ddot{r} = -\frac{4a^2 \dot{\theta}^2 \cos 2\theta}{r} - \dot{r}^2 = -\left[ \frac{4a^2 \dot{\theta}^2 \cos 2\theta}{r} + \frac{4a^4 \dot{\theta}^2 \sin^2 2\theta}{r^3} \right]$$

$$\vec{a} = \left( -\left[ \frac{4a^2 \dot{\theta}^2 \cos 2\theta}{r} + \frac{4a^4 \dot{\theta}^2 \sin^2 2\theta}{r^3} \right] + \frac{2a^2 \dot{\theta} \sin 2\theta}{r} \dot{\theta}^2 \right) \hat{r} - 2 \left( \frac{a^2 \dot{\theta}^2 \sin 2\theta}{r} \right) \hat{\theta}$$

$$a = |\vec{a}| = 1$$

$$a_r = -\left[ \frac{4a^2 \dot{\theta}^2 \cos 2\theta}{r} + \frac{4a^4 \dot{\theta}^2 \sin^2 2\theta}{r^3} + \frac{2a^2 \dot{\theta}^2 \sin 2\theta}{r} \right]$$

Good try

$$\ddot{r} = -\frac{4a^2 \dot{\theta}^2}{r} \left[ \cos 2\theta + \frac{a^2 \sin^2 2\theta}{r^2} \right] = -\frac{4a^2 \dot{\theta}^2}{r^3} \left[ 2a^2 \cos 2\theta + a^2 + a^2 \cos^2 2\theta \right]$$

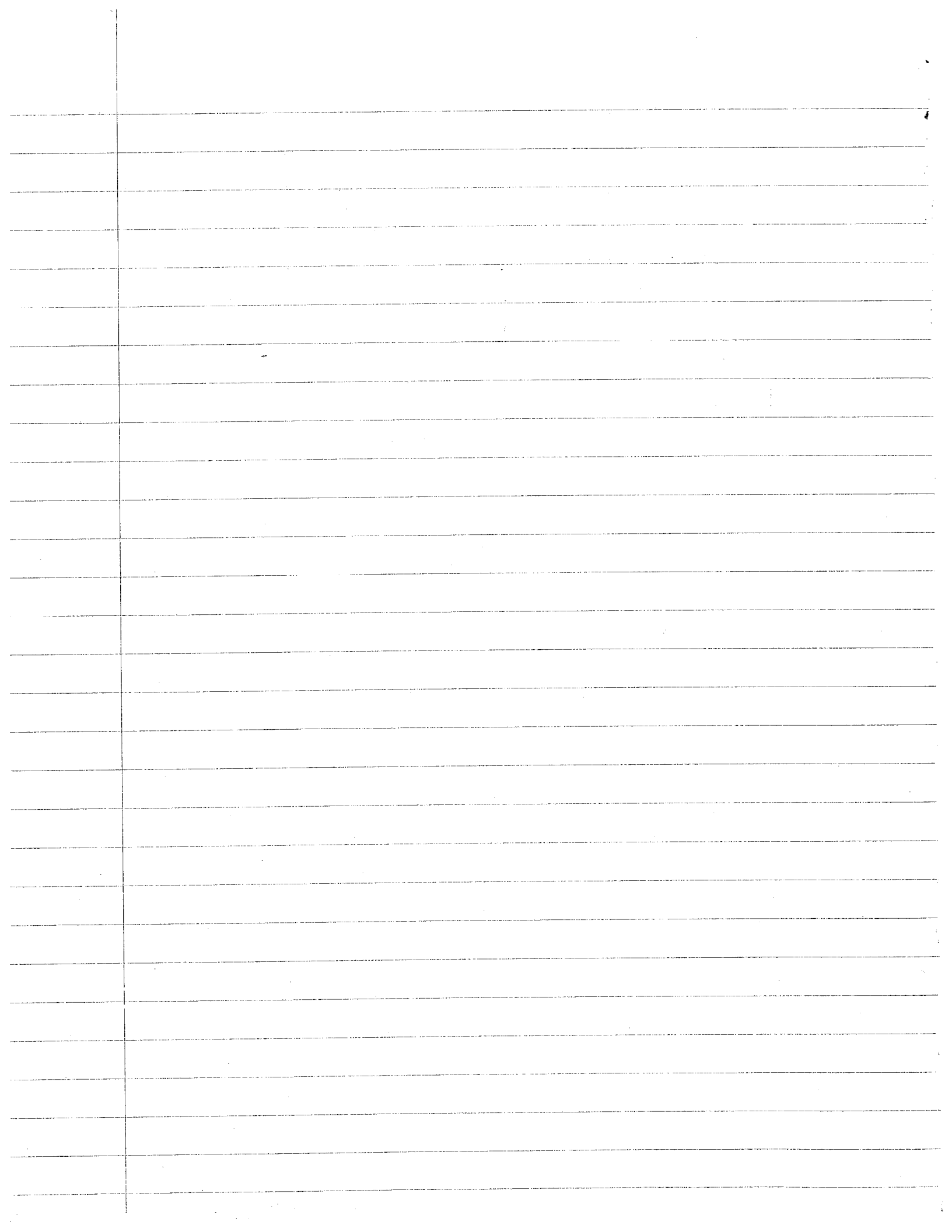
$$r \dot{\theta}^2 = \frac{r^2 \dot{\theta}^2}{r} = \frac{2a^2 \dot{\theta}^2 + 2a^2 \dot{\theta}^2 \cos 2\theta}{r}$$

$$\dot{r} \dot{\theta} = -\frac{2a^2 \dot{\theta}^2 \sin 2\theta}{r}$$

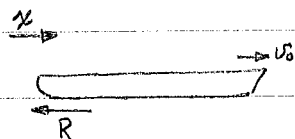
$$\ddot{r} = -\frac{4a^2 \dot{\theta}^2}{r} \frac{[1 + \cos 2\theta]}{2}$$

$$\ddot{r} = -\frac{2a^2 \dot{\theta}^2}{r} [1 + \cos 2\theta]$$

(25)



II



$$\sum F_x = m\ddot{x}$$

$$-mcv = m\ddot{x}$$

$$-mcv = m v \frac{dv}{dx}$$

$$-c dt = dv$$

$$-c \int_0^t dt = \int_{v_0}^v dv$$

$$-ct = -v_0 + v$$

$$v = v_0 - ct \quad \leftarrow (1)$$

$$\text{when } v=0 \quad t = t^*$$

$$\therefore \boxed{t^* = \frac{v_0}{c}} \quad !!$$

(1)  $\frac{ds}{dt} = v_0 - ct$  *should be  $x$  or  $r$*   $\rightarrow$  obtain  $-ct = \ln(v_0 - ct) + C$  etc  $\downarrow$

$$\int_0^s ds = \int_0^{t^*} (v_0 - ct) dt$$

$$s = v_0 t - \frac{ct^2}{2}$$

$$\text{when } t = t^* = \frac{v_0}{c}$$

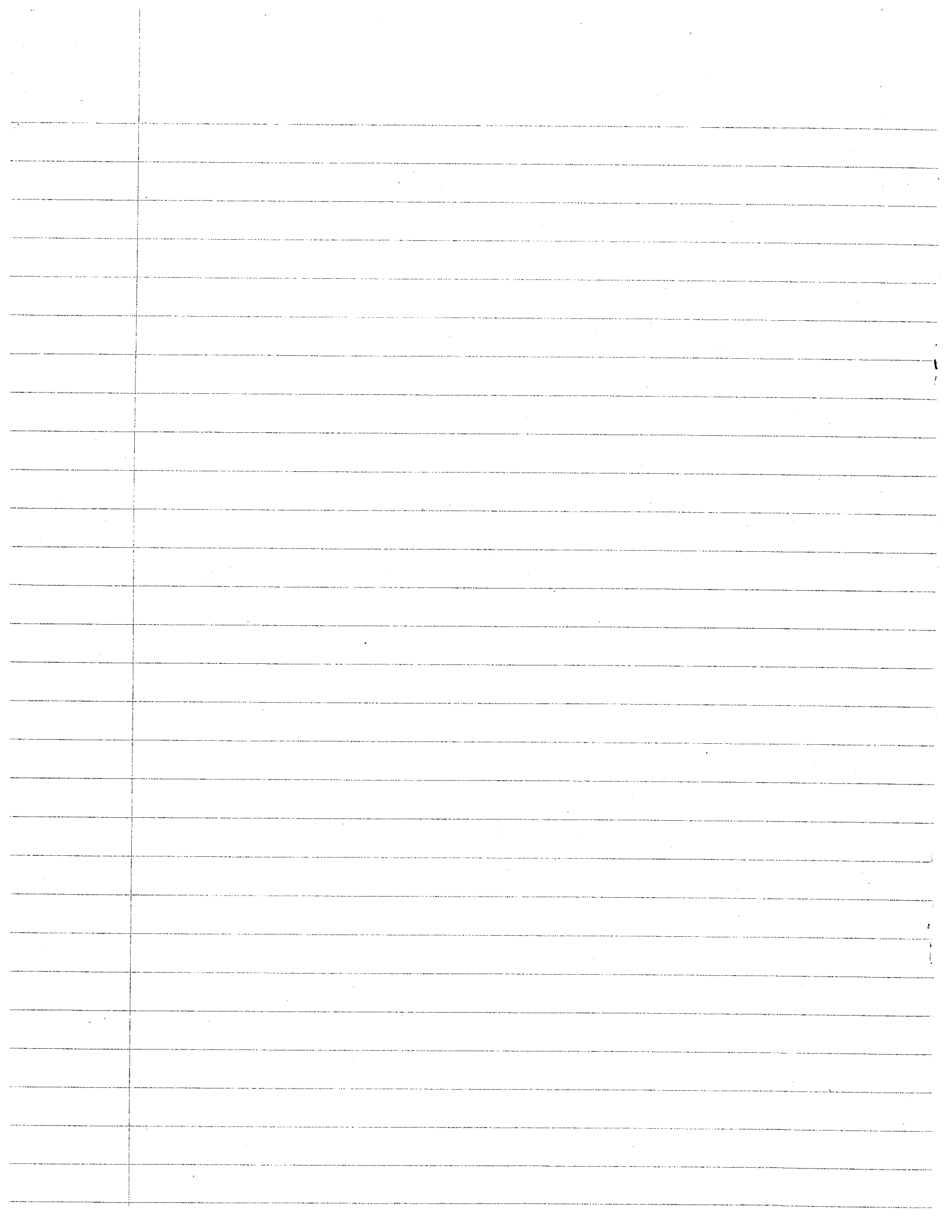
$$s = s^*$$

$$s^* = v_0 t^* - \frac{ct^{*2}}{2} = \frac{v_0^2}{c} - \frac{c v_0^2}{2 c^2} = \frac{v_0^2}{2c}$$

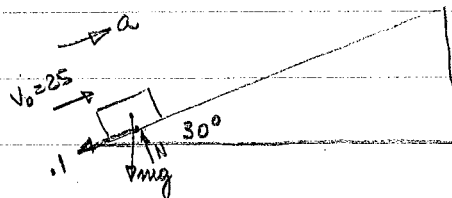
$$\boxed{s^* = \frac{v_0^2}{2c}}$$

BS

~90%



III



$$\int_1^2 \vec{F} \cdot d\vec{r} = T_2 - T_1$$

$$\vec{F} = (-\mu N - mg \sin \theta) \hat{i}$$

$$d\vec{r} = dx \hat{i}$$

$$\int \vec{F} \cdot d\vec{r} = - \int_0^x (\mu N + mg \sin \theta) dx = T_2 - T_1$$

$$F_y = N - mg \cos \theta = 0$$

$$N = mg \cos \theta$$

$$+ \cancel{\mu mg \cos \theta} + mg \sin 30^\circ x = + \frac{\mu v_0^2}{2}$$

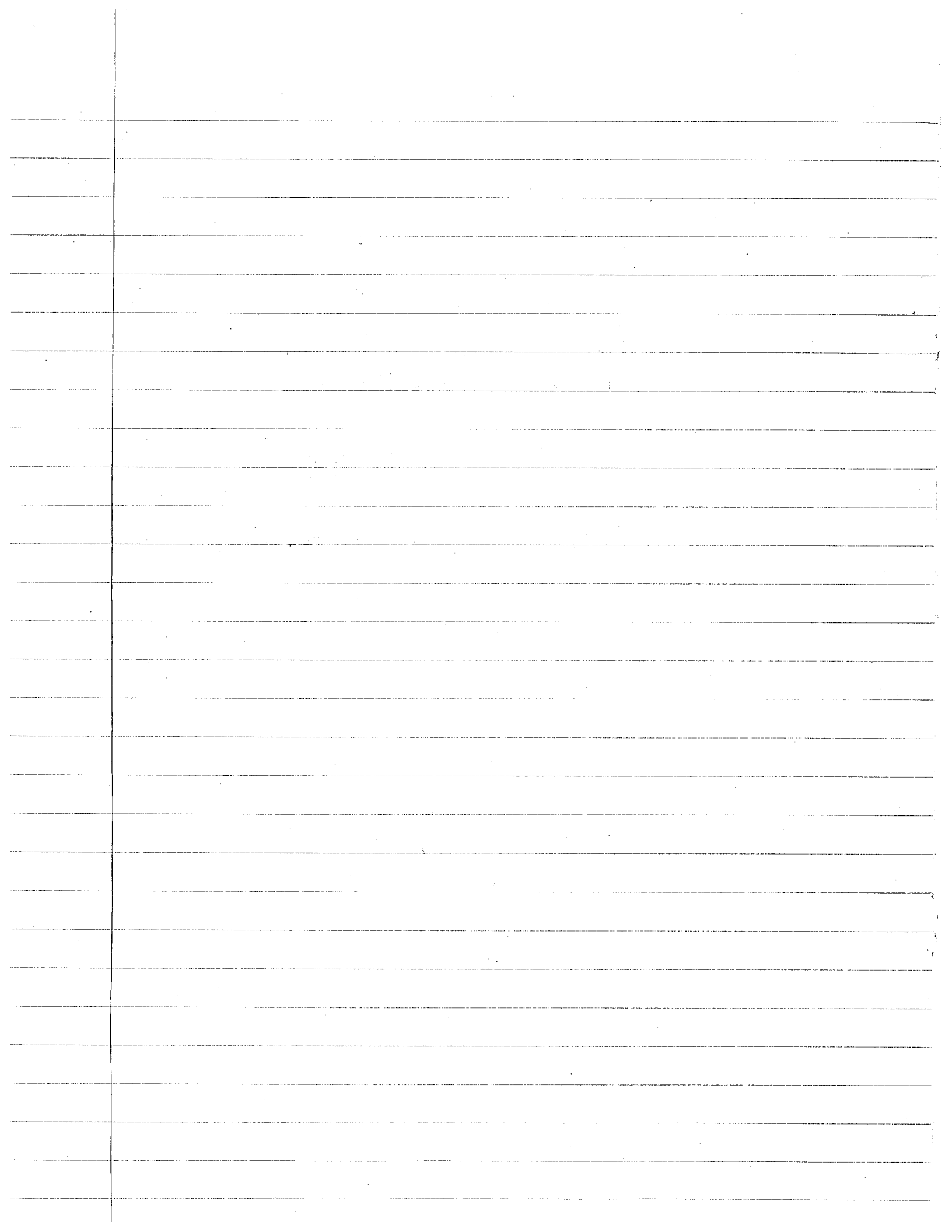
$$x = \frac{v_0^2}{2[\mu g + g/2]} = \frac{v_0^2}{g[2\mu + 1]}$$

$$- (\mu mg \cos \theta + mg \sin \theta) x = - \frac{\mu v_0^2}{2}$$

$$x = \frac{v_0^2}{2g[\mu \cos \theta + \sin \theta]} = \frac{625}{2(32)[.0866 + .5]}$$

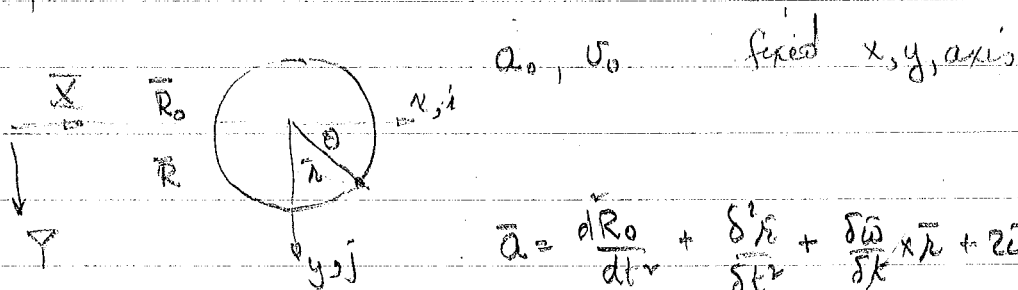
$$x = \frac{625}{64[.5866]} \approx 16.5 \text{ ft}$$

30





Problem semi:



$$\vec{a} = \frac{d\vec{R}_0}{dt} + \frac{\delta^2 r}{\delta t^2} + \frac{\delta \vec{\omega}}{\delta t} \times \vec{r} + 2\vec{\omega} \times \frac{\delta \vec{r}}{\delta t} + \vec{\omega} \times (\vec{\omega} \times \vec{r})$$

$$\vec{\omega} = 0$$

$$\vec{r} = r \cos \theta \hat{i} + r \sin \theta \hat{j}$$

$$\frac{\delta \vec{r}}{\delta t} = -r \sin \theta \dot{\theta} \hat{i} + r \cos \theta \dot{\theta} \hat{j}$$

$$\frac{\delta^2 \vec{r}}{\delta t^2} = r \left[ -[\ddot{\theta} \sin \theta + \dot{\theta}^2 \cos \theta] \hat{i} + [\ddot{\theta} \cos \theta - \dot{\theta}^2 \sin \theta] \hat{j} \right]$$

$$r \ddot{\theta} = \ddot{x} \quad \vec{a} = a_0 \hat{i} - \left[ a_0 \sin \theta + \frac{v_0^2}{r} \cos \theta \right] \hat{i} + \left[ a_0 \cos \theta - \frac{v_0^2}{r} \sin \theta \right] \hat{j}$$

$$r \dot{\theta} = \dot{x} = v_0$$

$$r \ddot{\theta} = \ddot{x} = a_0$$

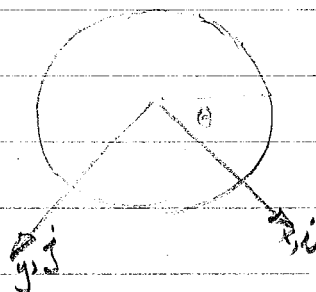
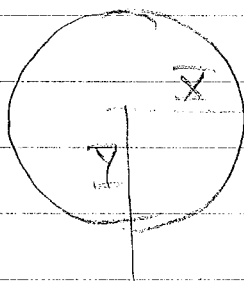
$$a^2 = \left[ a_0 (1 - \sin \theta) - \frac{v_0^2}{r} \cos \theta \right]^2 + \left[ a_0 \cos \theta - \frac{v_0^2}{r} \sin \theta \right]^2$$

$$2a \frac{da}{d\theta} = 2 \left[ a_0 (1 - \sin \theta) - \frac{v_0^2}{r} \cos \theta \right] \left[ -a_0 \cos \theta + \frac{v_0^2}{r} \sin \theta \right]$$

$$+ 2 \left[ a_0 \cos \theta - \frac{v_0^2}{r} \sin \theta \right] \left[ -a_0 \sin \theta - \frac{v_0^2}{r} \cos \theta \right] = 0$$

if  $x, y$  imbedded in wheels.

the  $\vec{\omega}$  is the rotation of relative frame seen from fixed syst.



$$v_0 \rightarrow \quad a_0 \rightarrow$$

$$\frac{d^2 \bar{R}_0}{dt^2} = \bar{a}_0$$

$$\bar{r} = r \bar{i}$$

$$\frac{\delta \bar{r}}{\delta t} = 0$$

$$\frac{\delta^2 r}{\delta t^2} = 0$$

$$\bar{a} = \frac{d^2 \bar{R}_0}{dt^2} + \frac{\delta \bar{\omega}}{\delta t} \times \bar{r} + \bar{\omega} \times (\bar{\omega} \times \bar{r})$$

$$\bar{\omega} = \frac{v_0}{r} \bar{k}$$

$$\frac{\delta \bar{\omega}}{\delta t} = \frac{a_0}{r} \bar{k} \quad \text{since} \quad r \ddot{\theta} = r \frac{\delta \omega}{\delta t} = a_0$$

$$\bar{a} = a_0 \bar{i} + \frac{a_0}{r} \bar{k} \times r \bar{i} + \frac{v_0}{r} \bar{k} \times \left( \frac{v_0}{r} \bar{k} \times r \bar{i} \right)$$

$$= a_0 \bar{i} + a_0 \bar{j} = \frac{v_0}{r} \bar{i}$$

$$\bar{i} = I \cos \theta + J \sin \theta$$

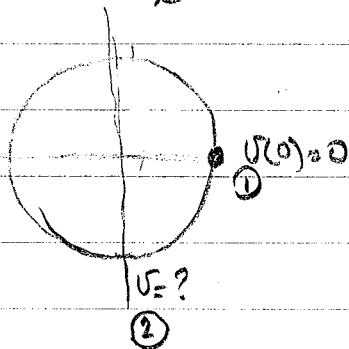
$$I = \bar{i} \cos \theta - \sin \theta \bar{j}$$

$$\bar{j} = J \cos \theta - I \sin \theta$$

$$J = \bar{i} \sin \theta + \bar{j} \cos \theta$$

$$\bar{a} = a_0 \cos \theta \bar{i} - a_0 \sin \theta \bar{j} - \frac{v_0}{r} \bar{i} + a_0 \bar{j}$$

$$= \left( a_0 \cos \theta - \frac{v_0}{r} \right) \bar{i} + a_0 (1 - \sin \theta) \bar{j}$$



$$T + V = E$$

$$T + V_1 = T_2 + V_2$$

$$0 = \frac{1}{2} m v_2^2 - mgr$$

$$v_2 = \sqrt{2gr}$$

3.  $h = 340$  miles  $r_1 = 3960 + 340 = 4300$  miles

$v_1 = 27000$  ft/sec

$$v_1^2 = \mu \left( \frac{2}{r_1} - \frac{1}{a} \right)$$

$$\frac{1}{a} = \frac{2}{r_1 + r_2}$$

$$v_1^2 = \mu \left( \frac{2(r_1 + r_2) - 2r_1}{r_1(r_1 + r_2)} \right) = \mu \left[ \frac{2r_2}{r_1(r_1 + r_2)} \right]$$

$$v_1^2 r_1 (r_1 + r_2) = 2\mu r_2$$

$$v_1^2 r_1^2 + v_1^2 r_1 r_2 = 2\mu r_2$$

$$v_1^2 r_1^2 = r_2 (2\mu - v_1^2 r_1)$$

$\sqrt{235 \times 10^8}$

$\sqrt{1\mu}$

$340 \times 10^3$

$$r_2 = \frac{v_1^2 r_1^2}{2\mu - v_1^2 r_1}$$

$\frac{ft^3}{sec^2} \quad \frac{ft^3}{sec^2}$   
 $3. \times 10^4 \times 5280 \quad 9 \times 10^8 \quad 4 \times 10^3 \cdot 5 \times 10^3 \quad (20 \times 10^3)^2 \quad 4 \times 10^{14} \cdot 9 \times 10^8 = 36 \times 10^{22}$

$$r_2 = \frac{(27000)^2 (4300 \times 5280)^2}{2.82 \times 10^{16} - (27000)^2 (4300 \times 5280)} = \frac{37.6 \times 10^{22}}{1.165 \times 10^{16}}$$

$30 \times 10^7$

$32.3 \times 10^6$  ft  $\frac{9 \times 10^8 (20 \times 10^3)^2}{18 \times 10^6}$   $\frac{22.7 \times 10^6}{5.2 \times 10^3}$   
 $4 \times 10^3$

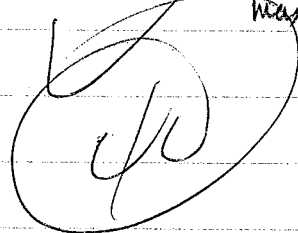
$r_2 = 22.7 \times 10^6$  ft = ~~4300 miles~~ 6120 miles

~~$h = 340$  miles~~

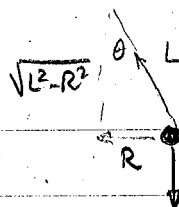
$h = 2160$  miles

~~max height~~

max height



1.



$$S \cos \theta = mg$$

$$S \sin \theta = \frac{mv^2}{R}$$

$$\cos \theta = \frac{\sqrt{L^2 - R^2}}{L}$$

$$\tan \theta = \frac{R}{\sqrt{L^2 - R^2}}$$

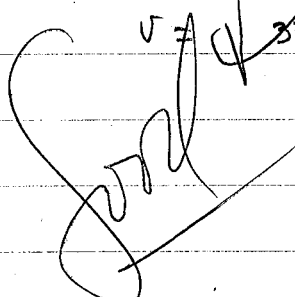
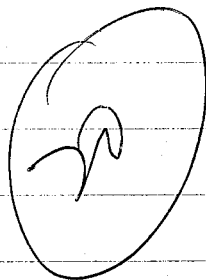
$$\sin \theta = \frac{R}{L}$$

$$\frac{g R^2}{\sqrt{L^2 - R^2}} = v^2$$

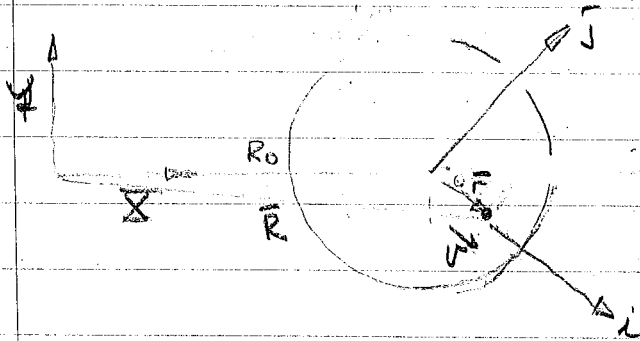
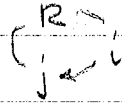
$$v^2 = \frac{(32.2)(4)}{\sqrt{16 - 4}} = \frac{32.2(4)}{2\sqrt{3}} = \frac{(32.2)(2)}{1.732}$$

$$\frac{64.4}{1.732} = v^2$$

$$v = \sqrt{37.2} = 6.1 \text{ ft/sec}$$



2.



$$\vec{r} = r \sin \theta \vec{j}$$

$$\omega = V/R$$

$\frac{dR_0}{dt} = 0$  since the wheel is not moving in translation with respect to fixed axes.  $\therefore \frac{d^2 R_0}{dt^2} = 0$

$$\vec{r} = (r \cos \theta \vec{i} - r \sin \theta \vec{j}) \quad \vec{r} = r \vec{i}$$

$$\frac{\delta \vec{r}}{\delta t} = V \vec{i}$$

$$\frac{\delta^2 \vec{r}}{\delta t^2} = 0$$

$$\frac{\delta \vec{r}}{\delta t} \cdot \frac{\delta \theta}{\delta t} = 0$$

if wheel has radius  $r$ .

$$\vec{\omega} = \omega \vec{k} \text{ since it is const angular velocity } \frac{\delta \vec{\omega}}{\delta t} = 0$$

$$\vec{a} = 0 + 0 + 0 + 2\omega \vec{k} \times V \vec{i} + \omega \vec{k} \times (\omega \vec{k} \times r \vec{i})$$

$$\vec{a} = 2\omega V \vec{j} + \omega \vec{k} \times \omega r \vec{j} = 2\omega V \vec{j} - \omega^2 r \vec{i}$$

$$\vec{a} = 2\omega V \vec{j} - \omega^2 r \vec{i}$$

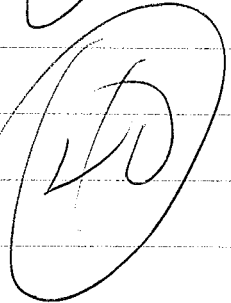
$$\text{if } \omega = v/b$$

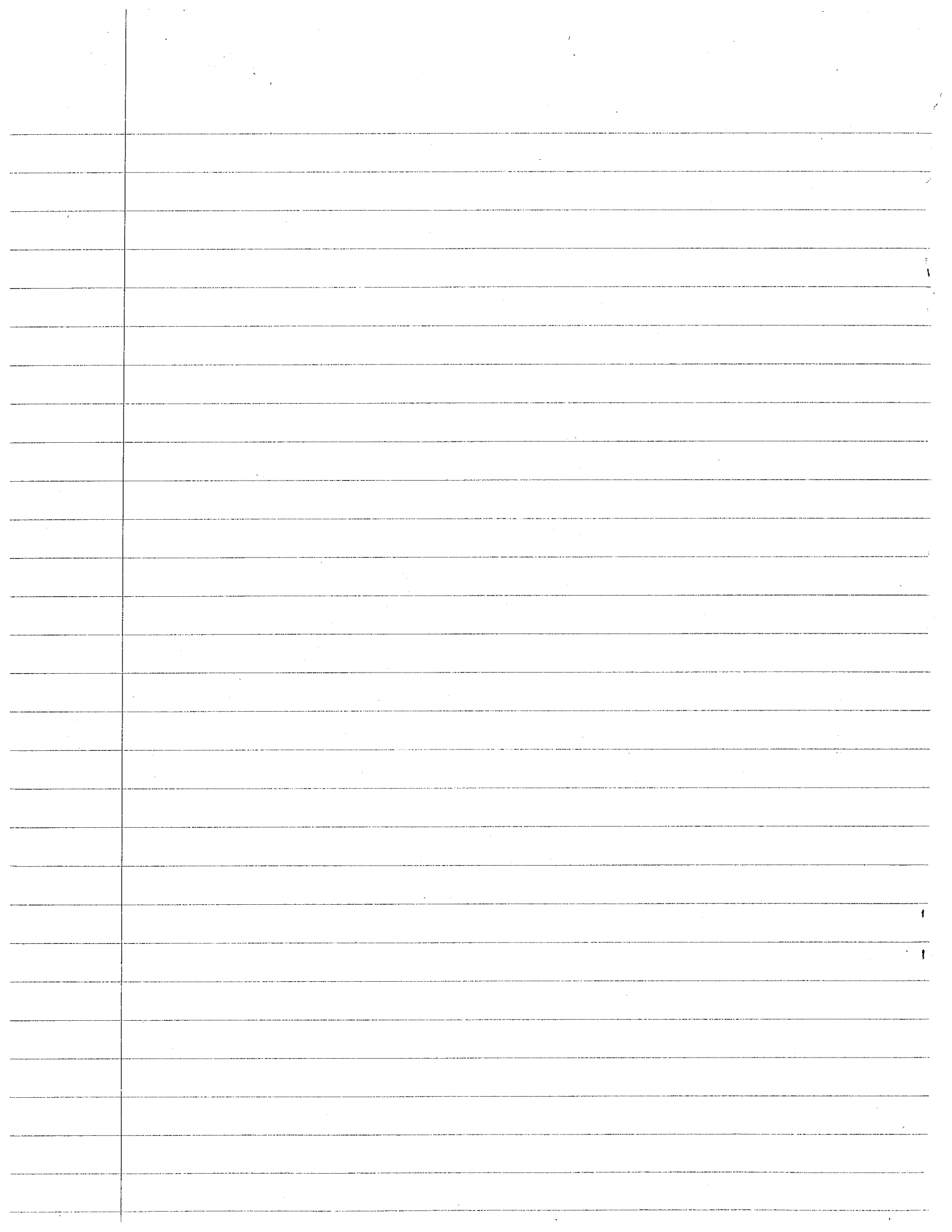
where  $v$  = bug's velocity

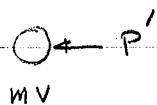
$$\frac{v^2}{b^2} r$$

$$\text{is } r = b$$

$$\frac{v^2}{b}$$



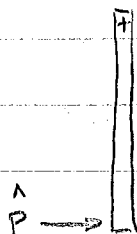




$$mv - \hat{P} = mv'$$

$$v' = v - \frac{\hat{P}}{m}$$

$$v_{cm}, v', \hat{P}, \omega$$



$$-\hat{R} + \hat{P} = Mv_{cm}$$

$$\hat{P}l = I_o \omega$$

$$I_o = \frac{Ml^2}{3} = \frac{.5(9)}{3} = 1.5$$

$$\omega = \hat{P} \cdot \frac{3}{2} \cdot \frac{1}{l} = 2 \frac{\hat{P}}{l}$$

$$e = .5 = \frac{v_{cm} + \omega l/2 - v'}{v - 0} = \frac{v_{cm} + 1.5\omega - v'}{v}$$

$$.5v = v_{cm} + 1.5\omega - v' = \frac{\hat{P}}{.5} + \frac{1.5 \hat{P} \cdot 3}{1.5} - v + \frac{\hat{P}}{m}$$

$$.5v = \frac{\hat{P}}{M} + 1.5 \frac{\hat{P}l}{I_o} - v + \frac{\hat{P}}{m}$$

$$1.5v = \frac{\hat{P}}{.5} + 3 \cdot \frac{1.5}{1.5} \hat{P} + \frac{\hat{P}}{.01} = 2\hat{P} + 3\hat{P} + 100\hat{P} = 105\hat{P}$$

$$\hat{P} = \frac{1.5}{105} v = \frac{150}{105} = 1.43 \text{ lb-sec}$$

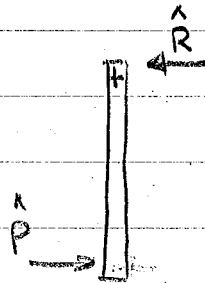
$$v_{cm} = \frac{.5}{1.43} = .35 \text{ ft/sec}$$

$$\textcircled{2} \quad \omega = \frac{\hat{P}l}{I_o} = \frac{1.43(3)}{1.5} = 2.86 \text{ rad/sec}$$

$$\textcircled{1} \quad v' = 100 - \frac{1.43}{.01} = 100 - 143 = -43 \text{ ft/sec}$$

$$e = .5 = \frac{v_{cm} + \omega l/2 - v'}{v} = .5v = v_{cm} + 1.5\omega - v' = 3\hat{P}$$

$$m\vec{v} - \hat{P} = m\vec{v}'$$



$$v', \hat{P}, v_{cm}, \hat{R}, \omega$$

$$\hat{P} - \hat{R} = Mv_{cm}$$

$$\hat{P}l = I_o \omega$$

$$e = .5 = \frac{v_{cm} + \frac{1}{2}\omega - v'}{v - 0}$$

$$1 - \hat{P} = .01v'$$

$$v_{cm} = \frac{1}{2}\omega$$

$$\omega = \frac{3\hat{P}}{1.5}$$

$$e = .5$$

$$.5v = \frac{(\omega - v')}{2} \Rightarrow .5v = 3(2\hat{P}) + 100\hat{P} - v$$

$$v' = v - \frac{\hat{P}}{m}$$

$$\frac{1.5v}{106} = \hat{P}$$

$$\hat{P} = 1.415 \text{ lb-sec}$$

$$\omega = 2\hat{P} = 2.83 \text{ rad/sec}$$

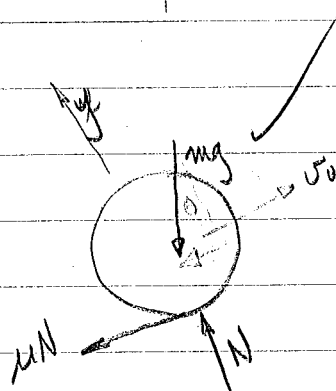
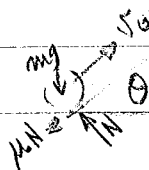
$$v_{cm} = 1.5(2.83) = 4.24 \text{ ft/sec}$$

$$\hat{R} = \hat{P} - Mv_{cm} = 1.415 - 2.12 = -.705 \text{ lb/sec} \checkmark$$

$$v' = 100 - 141.5 = -41.5 \text{ ft/sec} \checkmark$$

Solved





$$N - mg \cos \theta = m \ddot{y}_{cm} = 0$$

$$N = mg \cos \theta$$

$$-\mu N = m \ddot{x}_{cm} = -\mu mg \cos \theta = m \ddot{x}_{cm}$$

I forgot a  
 $-mg \sin \theta$   
 in here

$$-\mu g \cos \theta t = v_{cm} - v_0$$

should be

$$-\mu mg \cos \theta - mg \sin \theta = m \ddot{x}_{cm}$$

$$v_{cm} = -\mu g \cos \theta t + v_0 \quad \dot{x}_{cm} = -\mu g (\cos \theta + \sin \theta) t + v_0$$

$$a) \quad x_{cm} = -\mu g \cos \theta \frac{t^2}{2} + v_0 t$$

$$\mu N a = I_{cm} \dot{\omega} \quad \checkmark$$

$$b) \quad \text{when pure rolling} \quad v_{cm} = a \omega \quad \checkmark$$

$$t^* = \frac{a \omega - v_0}{-\mu g \cos \theta} = \frac{v_0 - a \omega}{\mu g \cos \theta}$$

$$x^* = -\frac{\mu g \cos \theta}{2} \left[ \frac{v_0 - a \omega}{\mu g \cos \theta} \right]^2 + v_0 \left[ \frac{v_0 - a \omega}{\mu g \cos \theta} \right]$$

$$\mu N a = I_{cm} \ddot{\theta}$$

$$\mu m g \cos \theta a = I_{cm} \ddot{\theta}$$

Integrate to  
obtain  $\dot{\theta}$  or  $\omega$

$$\ddot{\theta} = \frac{g \sin \theta}{R}$$

JK

It just took  
longer to roll  
w/ that  $\mu$  (negligible)  
component of  $F_x$

(K)