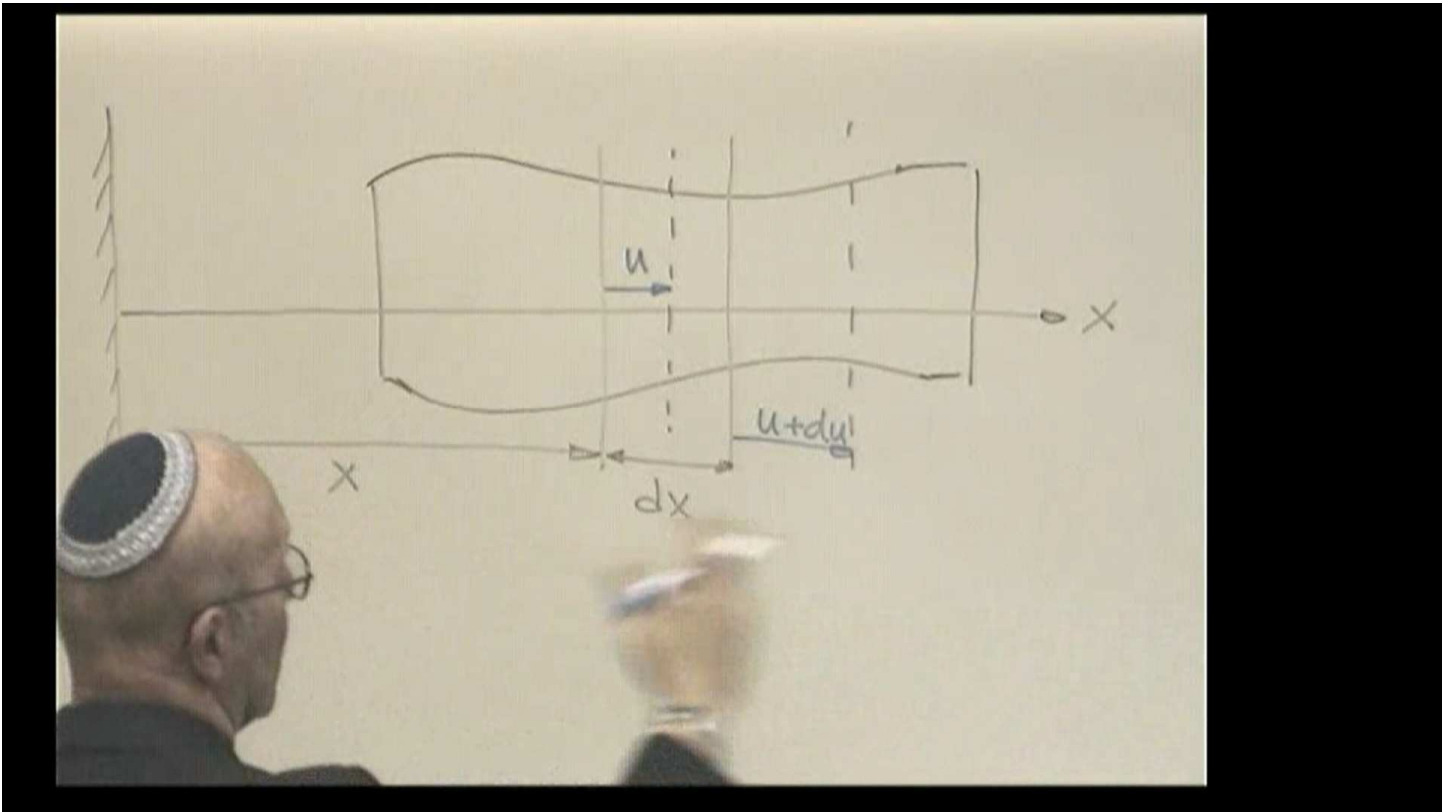


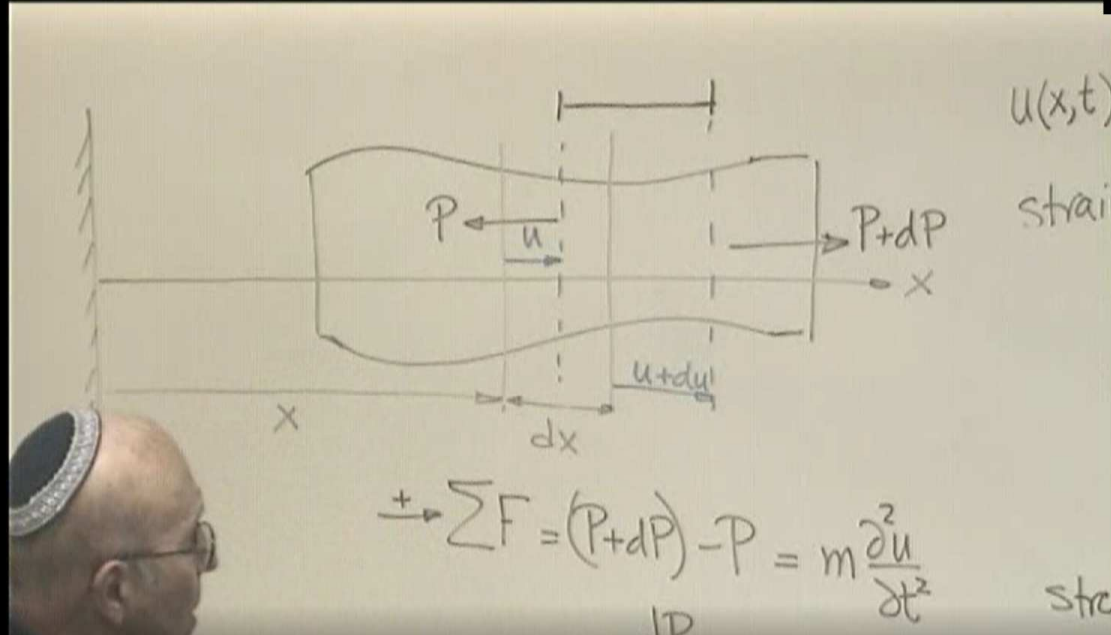
The derivation of the wave equation. Let  $u(x,t)$  represent the displacement of a cross-section of the bar at  $x$



$$\begin{aligned} \text{strain } \epsilon &= \frac{\text{new length} - \text{old length}}{\text{old length}} \\ &= \frac{[(x+dx+u+du) - (x+u)] - dx}{dx} \\ &= \frac{dx+du-dx}{dx} = \frac{du}{dx} \Rightarrow \frac{\partial u}{\partial x} \\ \text{stress } \sigma &= E\epsilon = E \frac{\partial u}{\partial x} \\ \text{force } \sigma \cdot A \end{aligned}$$

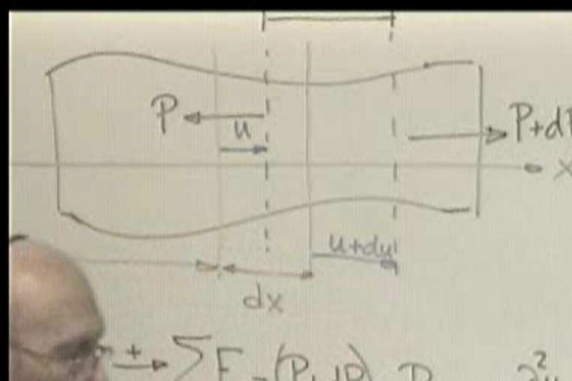
Force at any cross-section is  $\sigma \cdot A$  ( $A$  the cross-sectional area) =  $P$ . In 1-D we assume stress is the average across the cross-section.

Now application of the  $\sum F = \text{mass} \times \text{acceleration}$  gives



$u(x,t)$   
 strain  
 $x$   
 $P$   
 $u$   
 $P+dP$   
 $x$   
 $u+du$   
 $dx$   
 $\sum F = (P+dP) - P = m \frac{\partial^2 u}{\partial t^2}$   
 $\frac{dP}{dx} dx$   
 stress  
 for

Since  $P$  depends on stress and stress depends on variation of  $u$  with respect to  $x$ , then  $P$  is a function of  $x$



$u(x,t)$   
 strain  $\epsilon = \frac{\text{new length} - \text{old length}}{\text{old length}}$   
 $= \frac{[(x+dx+u+du) - (x+u)]}{dx}$   
 $= \frac{dx+du}{dx}$   
 $\sum F = (P+dP) - P = m \frac{\partial^2 u}{\partial t^2}$   
 $\frac{dP}{dx} dx$   
 stress  $\sigma = E \epsilon = E \frac{\partial u}{\partial x}$   
 force  $\sigma \cdot A$   
 $\frac{d}{dx}(\sigma A) dx = \frac{d}{dx} \left( E \frac{\partial u}{\partial x} A \right) dx =$

strain  $\epsilon = \frac{\text{old length}}{\text{new length}} = \frac{[(x+dx+u+du) - (x+u)]}{dx}$

$$= \frac{dx+du-dx}{dx} = \frac{du}{dx}$$

stress  $\sigma = E\epsilon = E \frac{du}{dx}$

force  $\sigma \cdot A$

$$(P+dP) - P = m \frac{\partial^2 u}{\partial t^2}$$

$$\frac{dP}{dx} dx = \frac{\partial}{\partial x} (E \frac{\partial u}{\partial x} A) dx = \rho A dx \frac{\partial^2 u}{\partial t^2}$$

In the case where the extensional stiffness  $EA$  is a constant, each can change at every cross-section but their product is constant, then

$$\frac{\partial}{\partial x} (EA \frac{\partial u}{\partial x}) = \rho A \frac{\partial^2 u}{\partial t^2}$$

IF  $EA = \text{const}$

$$EA \frac{\partial^2 u}{\partial x^2} = \rho A \frac{\partial^2 u}{\partial t^2}$$

$$\frac{\partial^2 u}{\partial x^2} = \frac{1}{c^2} \frac{\partial^2 u}{\partial t^2} \quad c = \sqrt{E/\rho}$$

Here  $c$  is the bar speed.  $\rho$  is the density, in this case mass/unit length.  $E$  has units of load/unit area.

IF  $EA = \text{const}$

$$EA \frac{\partial^2 u}{\partial x^2} = \rho A \frac{\partial^2 u}{\partial t^2}$$

$$\frac{\partial^2 u}{\partial x^2} = \frac{1}{c^2} \frac{\partial^2 u}{\partial t^2} \quad c = \sqrt{E/\rho}$$

$$u_{xx} - \frac{1}{c^2} u_{tt} = 0$$

$t \leftrightarrow y$   
 $x \leftrightarrow x$

$$Au_{xx} + Bu_{xy} + Cu_{yy} + \dots = 0 \quad A=1 \quad B=0 \quad C = -\frac{1}{c^2}$$

To characterize this equation to what we have learned previously

$$\frac{dy}{dx} = \frac{B \pm \sqrt{B^2 - 4AC}}{2A}$$

$$\frac{dt}{dx} = \pm \frac{\frac{2}{c}}{2} = \pm \frac{1}{c}$$

$$t - \frac{1}{c}x = \xi$$

$$t + \frac{1}{c}x = \eta$$

Now let us look at the 1-D heat equation and characterize it using the information we have previously learned

1-D Heat Eqn

$$\frac{\partial^2 T}{\partial x^2} = \alpha \frac{\partial T}{\partial t} \quad \alpha = \frac{\rho c v}{k}$$

$$0 = B^2 - 4AC \quad A=1 \quad B=0 \quad C=0$$

$$\frac{dt}{dx} = \frac{B \pm \sqrt{B^2 - 4AC}}{2A} = 0$$

Since  $dt/dx=0$ , then  $t=\text{constant}$ , let's call it  $\xi$  and the other characteristic is any line that crosses it like  $\eta=\text{constant}=x$ . Hence, the 1-D Heat equation is an example of a parabolic PDE.

Now look at the steady state 2-D heat equation

2-D STEADY STATE HEAT EQN

$$\frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} = \alpha \frac{\partial T}{\partial t}$$

$= 0$   
S.S.

$$\frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} = 0$$

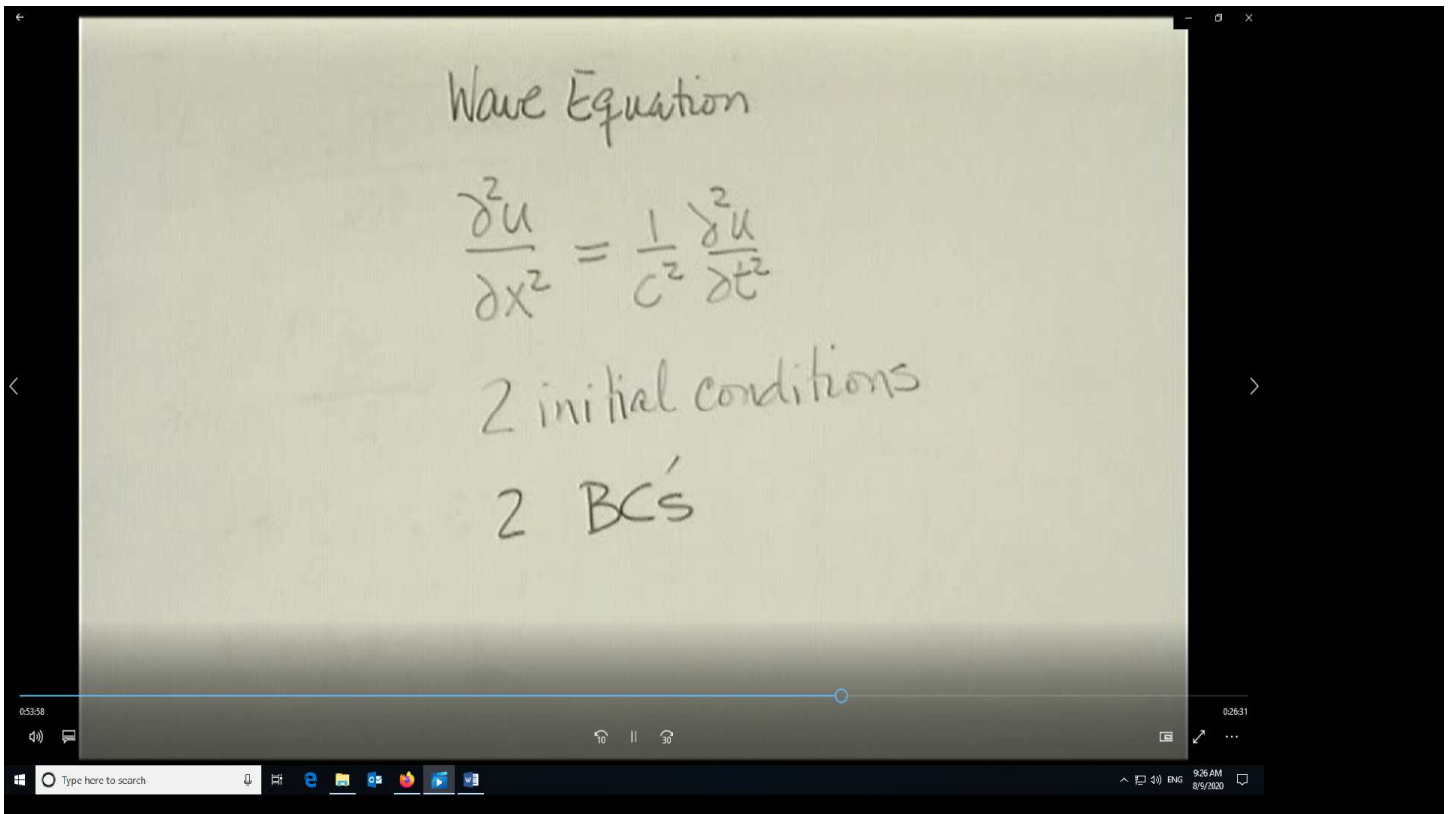
$$Au_{xx} + Bu_{xy} + Cu_{yy} + \dots = 0$$

$T \leftrightarrow u$   
 $x \leftrightarrow x$   
 $y \leftrightarrow y$

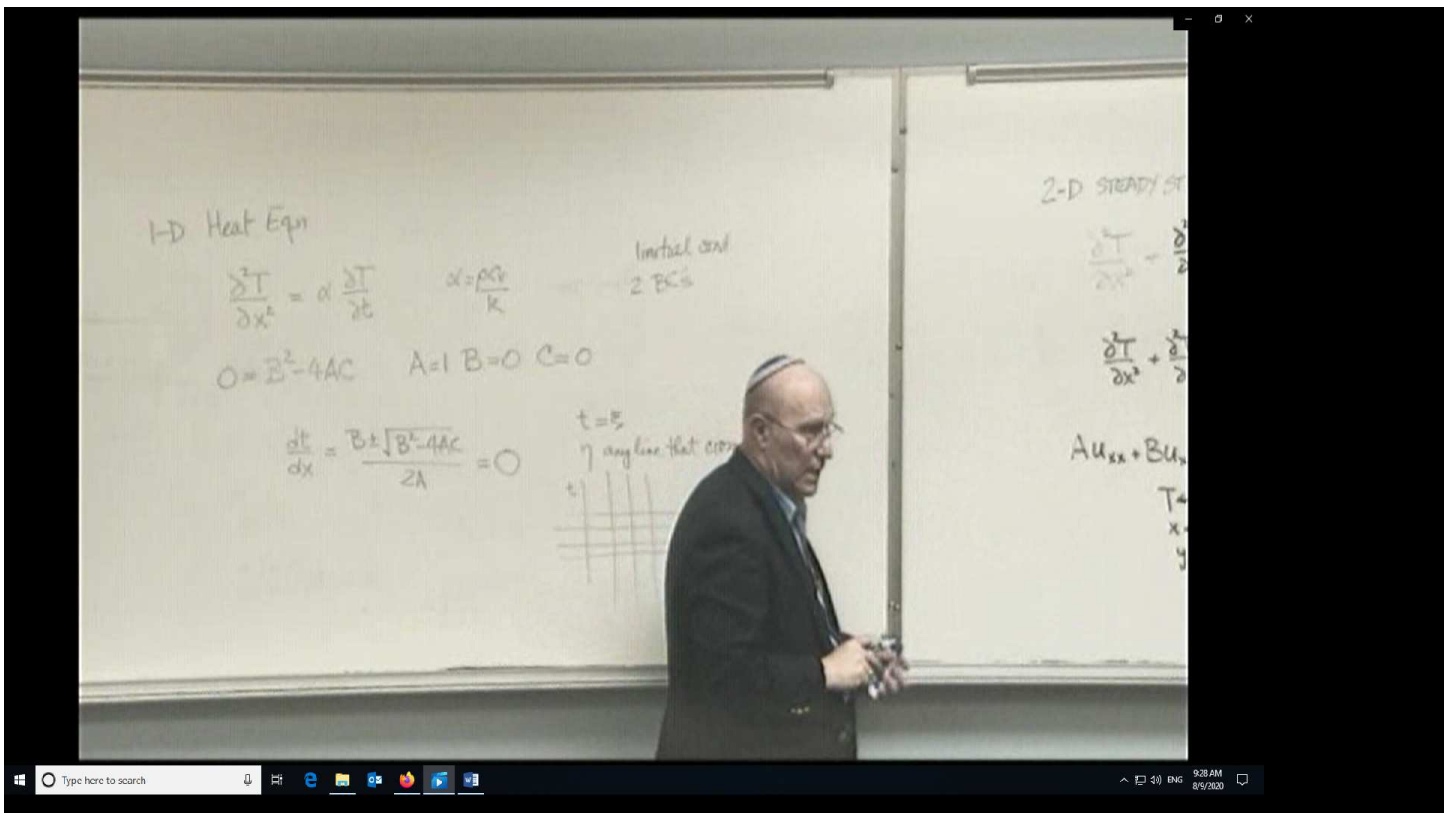
$A=1 \quad B=0 \quad C=1$   
 $B^2 - 4AC = -4 < 0$

Since the discriminant is less than zero, this is an example of an elliptic PDE

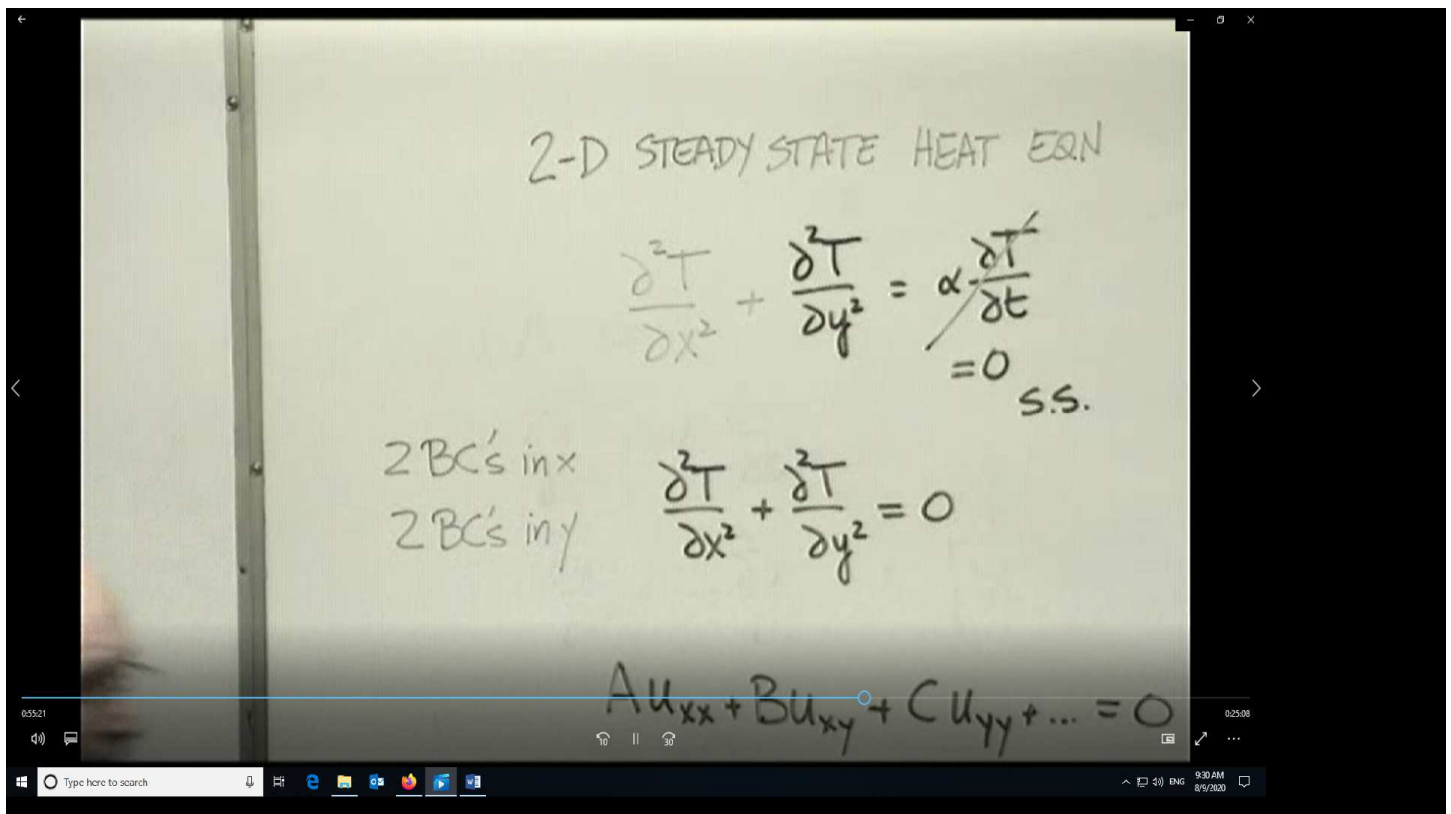




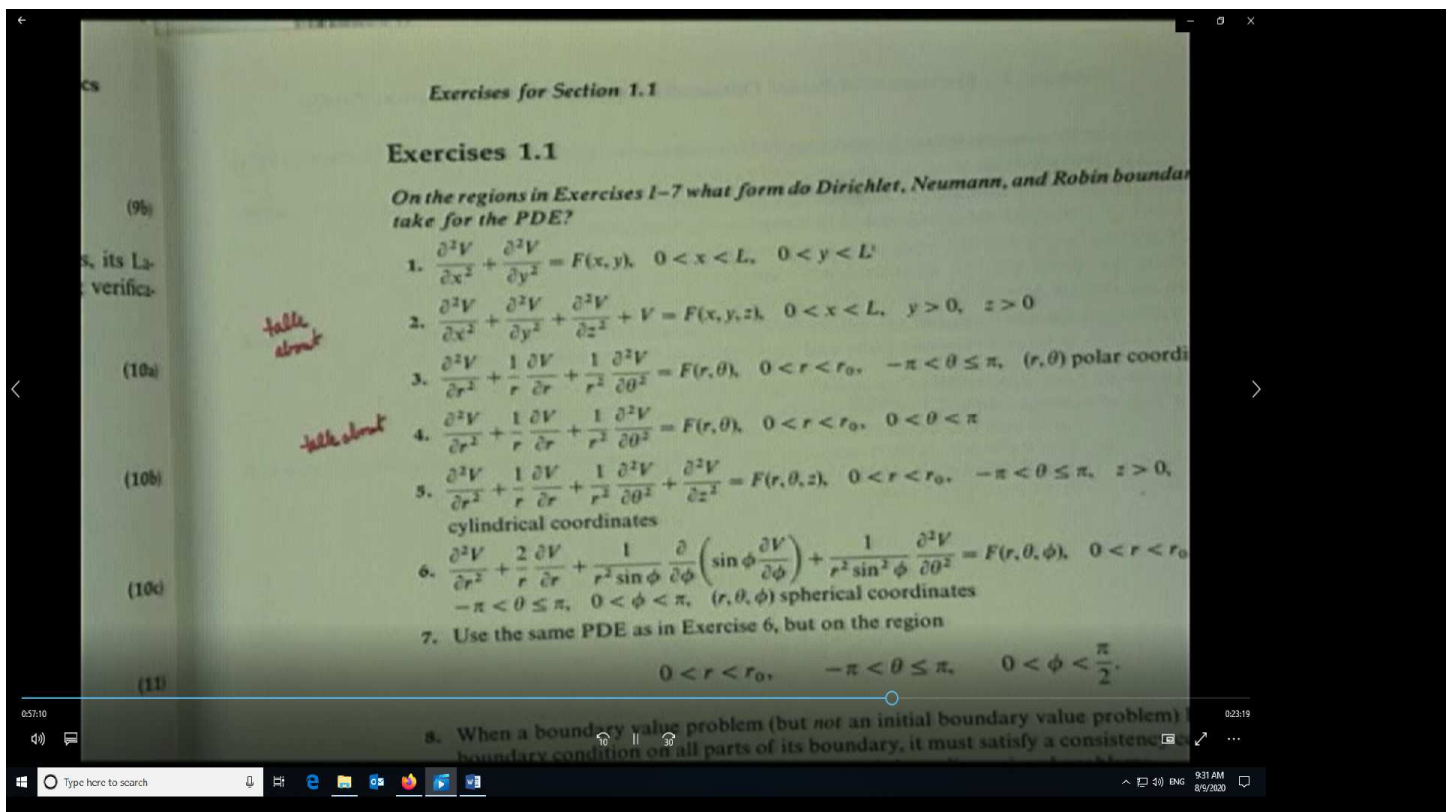
For a well posed wave-equation type problem, these are the basic requirements



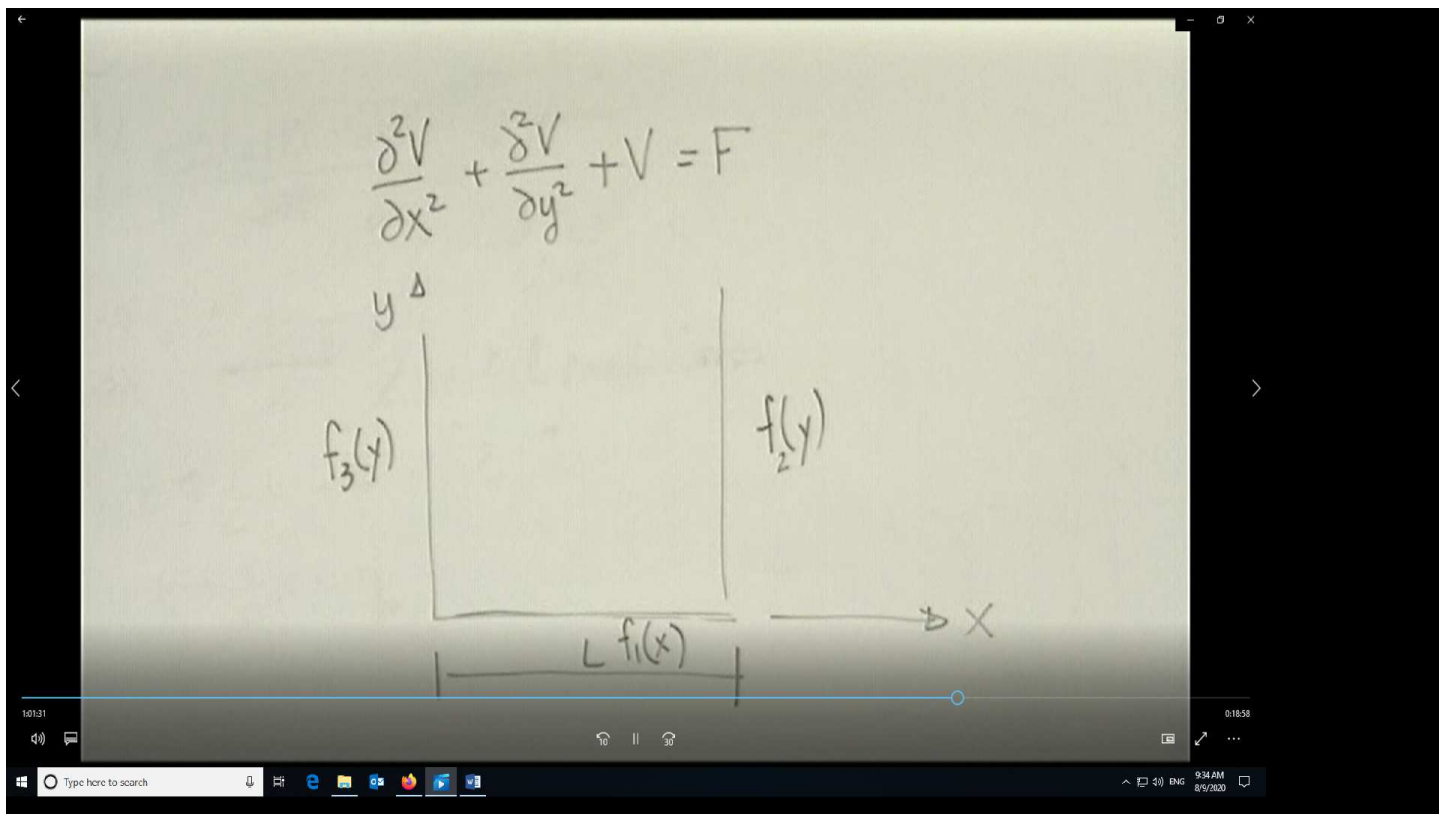
For a well posed parabolic PDE, you need 1 IC and 2 BCs



For elliptic conditions you need 4 BCs, in this case 2 in x and 2 in y

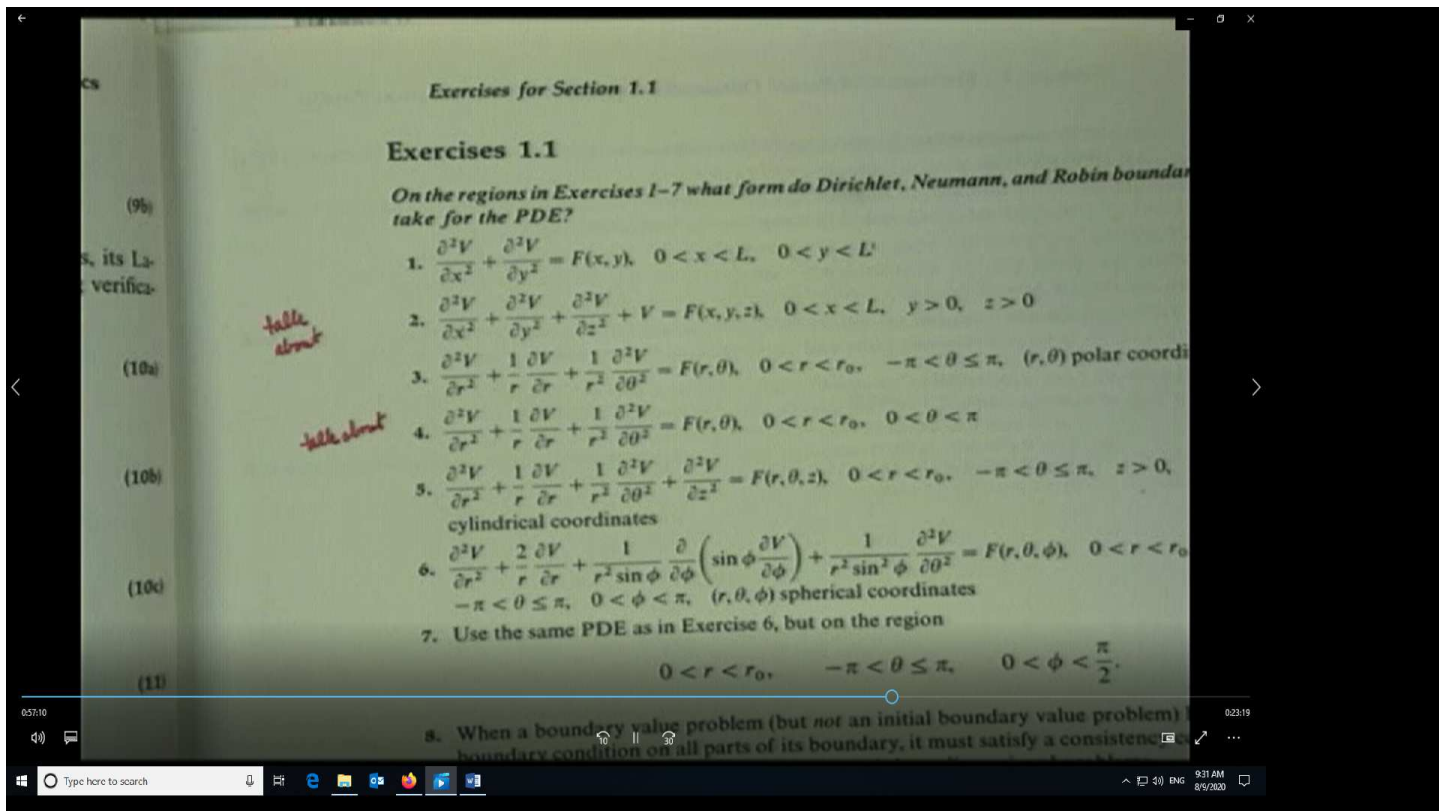


From Trim's book, Section 1.1 Exercise 1.1. Look at the 2-D equivalent of problem 2



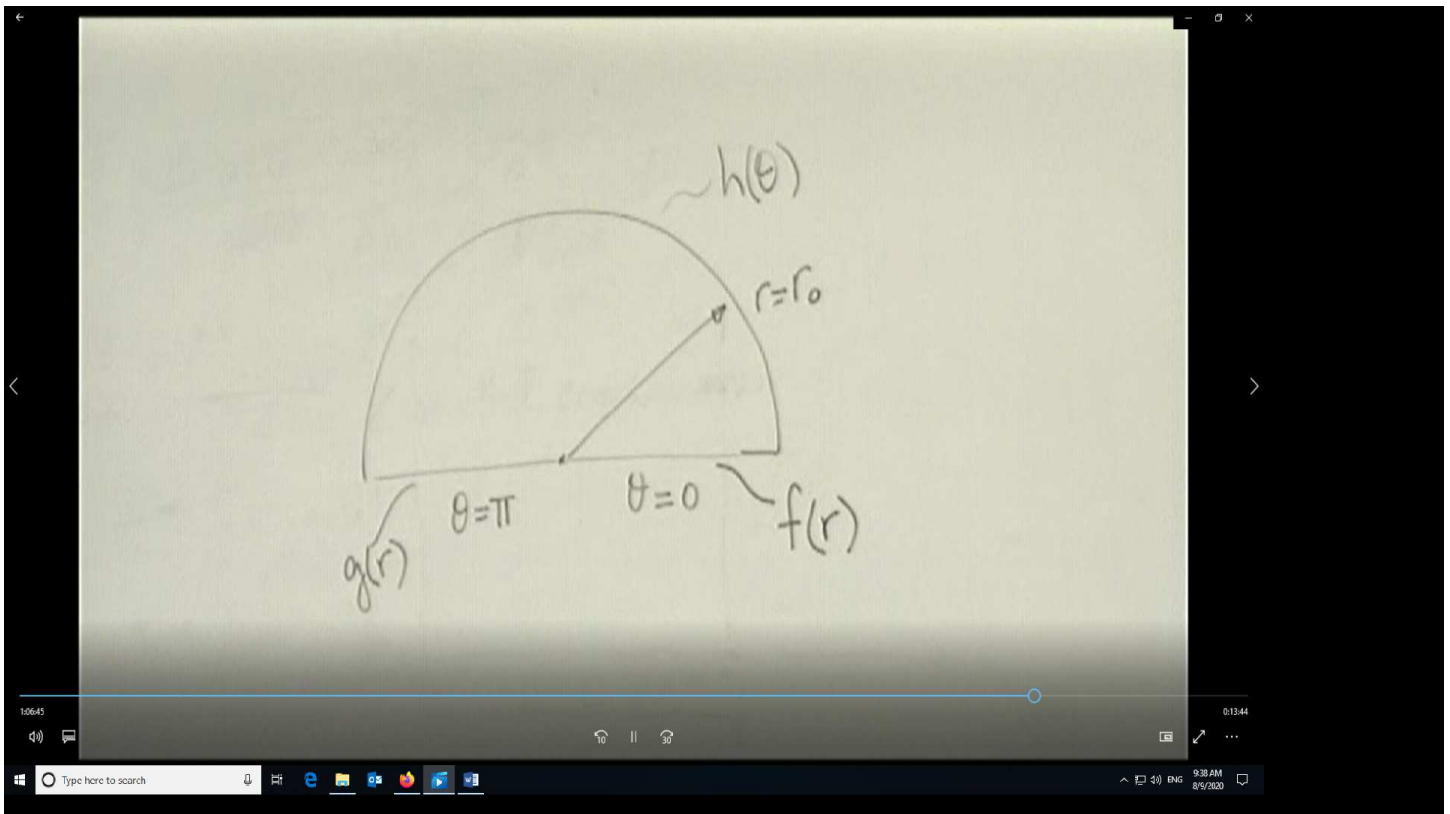
In this semi-infinite problem, at  $y=\infty$  the solution BC is that it must remain bounded. On the  $x=\text{constant}$ , the BCs can at most be functions of  $y$ , since  $x$  is fixed. On the  $y=\text{constant}$  line the BC can be at most a function of  $x$ .

Now looking at problem 4

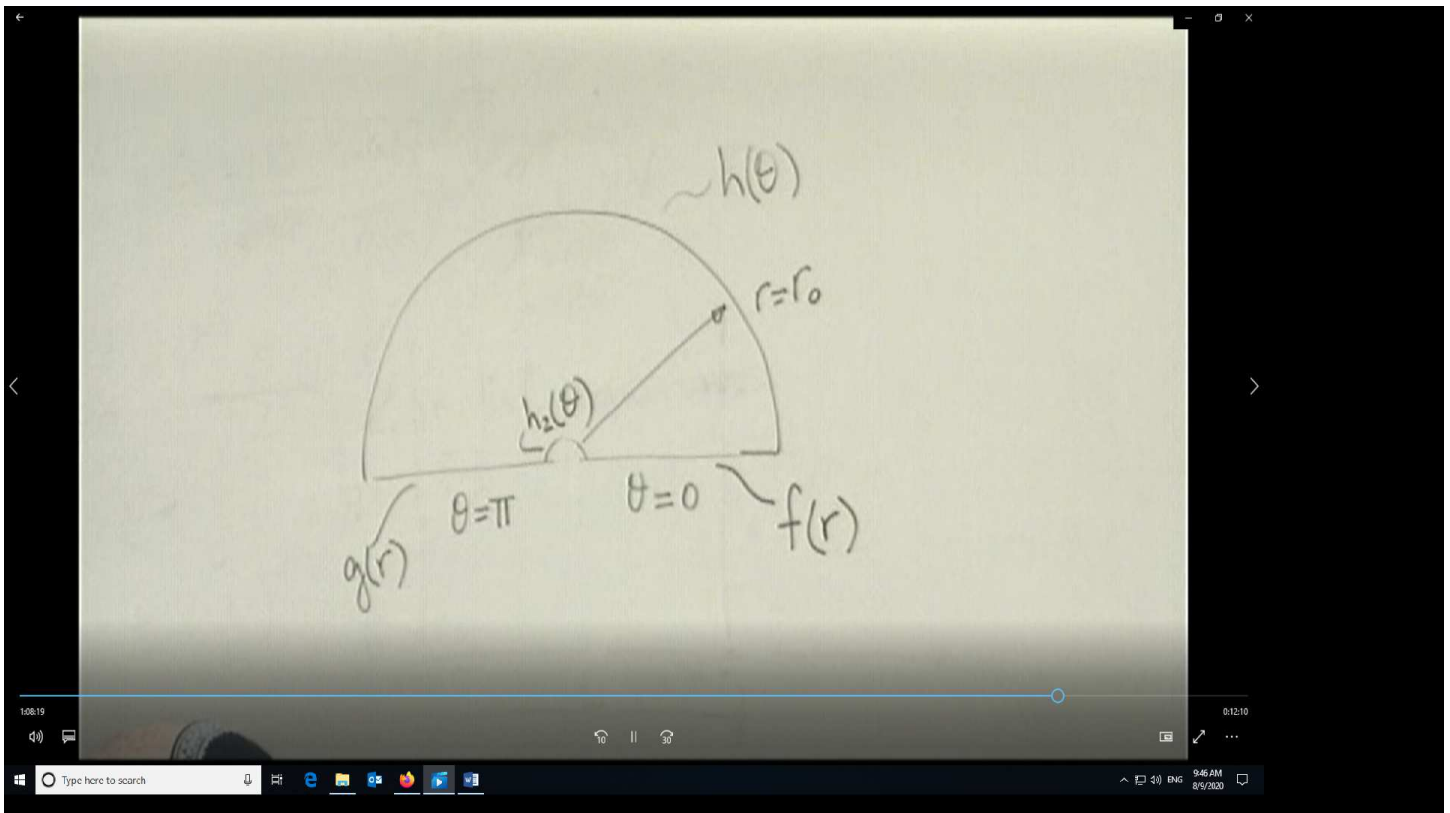


This is a semi circular region. The four boundaries are at  $\theta=0$ ,  $\theta=\pi$ ,  $r=r_0$  and at  $r=0$





$r=0$  is a limiting case of  $r=\epsilon$  where epsilon is a small quantity which is made smaller and smaller until it reaches zero. Namely, the semi-circle is a limiting case of a thick-walled cylinder where the inner radius is made so small as to collapse to a point.



In the above, for  $\theta=\text{constant}$  lines, the BCs can be at most functions of  $r$ ; similarly, on constant  $r$  lines, the BCs can be at most functions of  $\theta$ .

and, if  $V(x, y, z)$  is a function of three variables, as

$$\nabla^2 V = \frac{\partial^2 V}{\partial x^2} + \frac{\partial^2 V}{\partial y^2} + \frac{\partial^2 V}{\partial z^2}. \quad (9b)$$

When a function is expressed in polar, cylindrical, or spherical coordinates, its Laplacian is more complicated to calculate. We list the formulas here, leaving verification to Exercises 9 and 10. In polar coordinates  $(r, \theta)$  (Figure 1.5),

$$\nabla^2 V = \frac{\partial^2 V}{\partial r^2} + \frac{1}{r} \frac{\partial V}{\partial r} + \frac{1}{r^2} \frac{\partial^2 V}{\partial \theta^2}; \quad (10a)$$

in cylindrical coordinates  $(r, \theta, z)$ ,

$$\nabla^2 V = \frac{\partial^2 V}{\partial r^2} + \frac{1}{r} \frac{\partial V}{\partial r} + \frac{1}{r^2} \frac{\partial^2 V}{\partial \theta^2} + \frac{\partial^2 V}{\partial z^2}; \quad (10b)$$

and in spherical coordinates  $(r, \theta, \phi)$  (Figure 1.6),

$$\nabla^2 V = \frac{\partial^2 V}{\partial r^2} + \frac{2}{r} \frac{\partial V}{\partial r} + \frac{1}{r^2 \sin \phi} \frac{\partial}{\partial \phi} \left( \sin \phi \frac{\partial V}{\partial \phi} \right) + \frac{1}{r^2 \sin^2 \phi} \frac{\partial^2 V}{\partial \theta^2}. \quad (10c)$$

The PDE obtained by setting the Laplacian of a function equal to zero,

$$\nabla^2 V = 0, \quad (11)$$

is called *Laplace's equation*.

Here we show the definition of the Laplacian in different coordinate systems, Cartesian, cylindrical and spherical.

Examples of types of BCs: first type of Dirichlet (on  $u$ ), second type or Neumann (on derivative of  $u$ ), third type or mixed/Robin (on combination of  $u$  and its derivative)